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## APPROXIMATE METHOD FOR CALCULATING TRANSONIC FLOW ABOUT LIFTING WING-BODY CONFIGURATIONS: COMPUTER PROGRAM AND USER'S MANUAL

Richard W. Barnwell and Ruby M. Davis  
August 1975

(NASA-TM-X-72758) APPROXIMATE METHOD FOR  
CALCULATING TRANSONIC FLOW ABOUT LIFTING  
WING-BODY CONFIGURATIONS: COMPUTER PROGRAM  
AND USER'S MANUAL (NASA) 135 p HC \$3.75

N75-30099

CSCL 01A G3/02 33056  
SEP 1975  
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NASA STI FACILITY  
INPUT BRANCH  
Unclas

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NATIONAL AERONAUTICS AND SPACE ADMINISTRATION  
LANGLEY RESEARCH CENTER, HAMPTON, VIRGINIA 23665

1. Report No. <b>NASA TM X-72758</b>	2. Government Accession No.	3. Recipient's Catalog No.
4. Title and Subtitle <b>Approximate Method for Calculating Transonic Flow About Wing-Body Configurations: Computer Program and User's Manual</b>	5. Report Date <b>August 1975</b>	6. Performing Organization Code
7. Author(s) <b>Richard W. Barnwell and Ruby M. Davis</b>	8. Performing Organization Report No.	10. Work Unit No. <b>505-06-11-02</b>
9. Performing Organization Name and Address <b>NASA-Langley Research Center Hampton, Virginia 23665</b>	11. Contract or Grant No.	13. Type of Report and Period Covered <b>NASA Technical Memorandum</b>
12. Sponsoring Agency Name and Address <b>National Aeronautics and Space Administration Washington, D. C. 20546</b>	14. Sponsoring Agency Code	
15. Supplementary Notes <b>Special technical information release, not planned for formal NASA publication.</b>		
16. Abstract <b>This paper is a user's manual for a computer program which calculates inviscid flow about lifting configurations in the free-stream Mach-number range from zero to low supersonic. Angles of attack of the order of the configuration thickness-length ratio and less can be calculated. An approximate formulation is used which accounts for shock waves, leading-edge separation and wind-tunnel wall effects.</b>		
17. Key Words (Suggested by Author(s)) (STAR category underlined) <b><u>Aerodynamics</u></b> <b>Transonic Flow</b> <b>Wing-Body Configurations</b> <b>Leading-Edge Separation</b> <b><u>Shock Waves</u></b> <b>Wind-Tunnel Walls</b>		18. Distribution Statement <b>Unclassified - unlimited</b>
19. Security Classif. (of this report) <b>Unclassified</b>	20. Security Classif. (of this page) <b>Unclassified</b>	21. No. of Pages <b>133</b>
		22. Price* <b>\$5.75</b>

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APPROXIMATE METHOD FOR CALCULATING  
TRANSONIC FLOW ABOUT LIFTING WING-BODY  
CONFIGURATIONS: COMPUTER PROGRAM AND  
USER'S MANUAL

Richard W. Barnwell and Ruby M. Davis  
Langley Research Center

SUMMARY

This paper is a user's manual for a computer program which calculates inviscid flow about lifting configurations in the free-stream Mach number range from zero to low supersonic. Angles of attack of the order of the configuration thickness-length ratio and less can be treated. An approximate formulation is used which accounts for shock waves, leading edge separation and wind-tunnel wall effects.

INTRODUCTION

In this paper a listing, user's manual, and sample case for a computer program which calculates inviscid flow about lifting configurations traveling at any Mach number in the range from zero to low supersonic is presented. The angle-of-attack range extends to values of the order of the configuration thickness length ratio. The approximate method which is used is described in reference 1. A preliminary version of the method is described in reference 2. The theory of

references 3 and 4 is used to reduce the nonlinear three-dimensional problem of transonic flow about lifting configurations to two two-variable problems: a linear lift problem and a nonlinear coupled thickness-lift problem.

The linear lift solution is determined first. For free-stream Mach numbers near one this solution is obtained from slender-wing theory. For subsonic and supersonic Mach numbers appreciably different from one the theory of Lawrence and Flax (ref. 5) and a modified version of the quasiconical theory of Carofoli (ref. 6), respectively, are used. It should be noted that the lift solution varies consistently in the transonic range because the theory of Lawrence and Flax and quasiconical theory both reduce to slender wing theory as the free-stream Mach number approaches one.

The nonlinear thickness-lift solution is determined numerically with a two-independent variable method of relaxation algorithm of the type introduced by Murman and Cole (ref. 7). The present method is similar to that of Bailey (ref. 8) for axisymmetric flow except that the shock finite-difference operator of Murman (ref. 9) is employed.

The two-variable formulation of the thickness-lift problem is similar to the axisymmetric formulation, in that the independent variables are the axial and radial coordinates  $x$  and  $r$  as shown in figure 1.

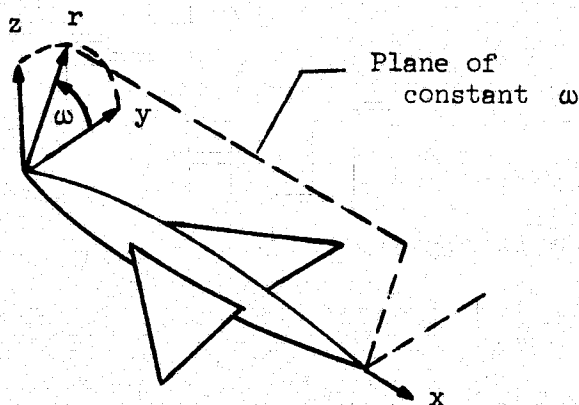


Figure 1.- Coordinate systems.

However, cross-flow effects are not set to zero as in axisymmetric flow but are evaluated with the theory of references 3 and 4. It should be noted that this theory accounts for nonlinear as well as linear phenomena. Solutions are determined in semiplanes of constant polar angle  $\omega$  such as the one shown in figure 1. A separate solution must be obtained in each plane for which results are desired. Note that the angle  $\omega$  is zero in the wing plane and is positive above the wing.

A discussion of the program input and output are given in this paper. In addition, a Fortran IV program listing is given in appendix A, and a sample input and output are given in appendices B and C, respectively. The minimum number of computer storage locations required to execute the program on the CDC 6600 computer is 77,000<sub>8</sub>.

## SYMBOLS

$a, b$	width and spacing of slots in slotted tunnel wall
$f(x)$	dipole strength for linear lift solution
$M_{\infty}$	free-stream Mach number
$r$	radial coordinate
$U_{\infty}$	free stream velocity
$u, v$	perturbation velocity components in axial and radial directions
$x$	axial coordinate
$x_c$	axial position of maximum body diameter
$y$	spanwise coordinate
$z$	vertical coordinate
$\alpha$	angle of attack
$\kappa$	constant of proportionality for slotted-wall boundary condition
$\rho_{\infty}$	free-stream density
$\omega$	polar angle

## DESCRIPTION OF INPUT

The program input consists of 17 fixed-point and 22 floating-point parameters which are input with a namelist statement. These parameters are organized into several groups according to their use.

### Computational Grid

The first 10 parameters determine the grid, which is shown schematically in figure 2. The grid indices in the axial and radial directions are  $J$  and  $K$ , respectively; and the arrays for the axial and radial grid coordinates are  $XW(J)$  and  $RW(K)$ .

The grid in the axial direction is specified by the fixed-point parameters  $J1$ ,  $J2$ ,  $J3$ ,  $J4$  and  $J5$  and the floating-point parameter  $FAC$ . The grid is uniform between  $J1$  and  $J4$ . The body is located between  $J2$  and  $J3$ , and the  $x$  grid is scaled such that

$$XW(J2) = 0,$$

$$XW(J3) = 1.$$

There are expanded grids in the regions  $J=1$  to  $J=J1$  and  $J=J4$  to  $J=5$  such that

$$(XW(J) - XW(J-1))/(XW(J+1) - XW(J)) = FAC$$

in the upstream nonuniform region and

$$(XW(J) - XW(J-1))/(XW(J-1) - XW(J-2)) = FAC$$

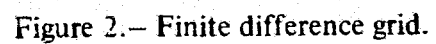


Figure 2.— Finite difference grid.

in the downstream nonuniform region. For supersonic free-stream Mach numbers it is recommended that the grid be uniform everywhere. This is accomplished by setting

$$J1 = 1$$

$$J4 = J5$$

The grid in the radial direction is specified by the fixed-point parameter  $KM$  and the floating-point parameters  $RCOM$ ,  $A$  and  $B$ . The index of the outer boundary is  $KM$ . The radial grid distribution is given by the equation

$$RW(K) = RCOM + ETA / (B - ETA * A)$$

where

$$ETA = K / KM$$

The quantity  $RCOM$  is the radius at which the inner boundary condition is applied, and the parameters  $A$  and  $B$  determine that stretching in the radial direction. If  $A=B$  the radius of the outer boundary  $RW(KM)$  is infinite.

### Outer Boundary Condition

The boundary condition at the outer wall is specified by the fixed-point parameter IWALL and the floating-point parameter P. The values for IWALL are

IWALL =	0, free air
	1, porous wall
	2, slotted wall

If IWALL=0, the parameter P is not used by the program so any value may be input. For a porous wall (IWALL = 1) P is the constant of proportionality in the porous-wall boundary condition

$$v = -Pu$$

where u and v are the perturbation velocity components in the axial and radial directions respectively. For a slotted wall (IWALL = 2) P is the constant of proportionality in the slotted wall boundary condition

$$\frac{\partial v}{\partial x} = -Pu$$

It should be noted that P for slotted walls is the reciprocal of the parameter  $\kappa$  used in references 1 and 2. Baldwin, Turner and Knechtel (ref. 10) derive the approximate form

$$\kappa = -\frac{b}{\pi} \ln \left( \sin \frac{\pi a}{2b} \right)$$

where b and a are the slot width and spacing.



## Basic Parameters

There are five basic floating-point parameters.  $\phi$ MEGAD is the polar angle  $\omega$  shown in figure 1 which defines the plane in which the computation is made, and ALPHAD is the angle of attack. Both  $\phi$ MEGAD and ALPHAD are in degrees. HSPAN is the nondimensional semispan of the wing. The Mach number and ratio of specific heats are specified by the parameters AMINF and GAMMA, respectively.

## Body

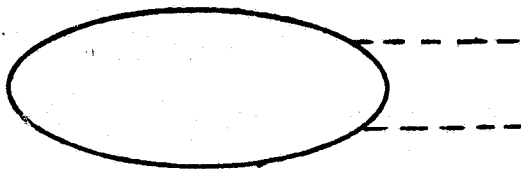
The body shape is specified by two fixed-point parameters and four floating-point parameters. There are 5 body shapes which can be used. The choice of body shape is designated with the parameter IR as shown in figure 3. The maximum body radius is specified by the parameter RMAX.

The parameters RC and RN are used only for the general pointed bodies. If IR is not 1 or 2 any value can be specified for these parameters. The general pointed-body shapes were developed by McDevitt and Taylor (ref. 11). If the point of maximum thickness is ahead of the mid-point the body radius  $R(J)$  is given by the FORTRAN IV equation

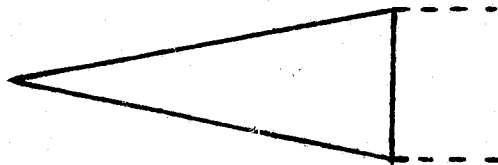
$$R(J) = RC * RMAX * (1. - XW(J) - (1. - XW(J)) ** RN)$$

and if the point of maximum thickness is behind the midpoint the equation for the body radius is

$$R(J) = RC * RMAX * (XW(J) - XW(J) ** RN)$$



ellipse,  $IR = 0$



cone,  $IR = 3$



general pointed body, maximum  
radius ahead of midpoint  
 $IR = 1$



ogive-cylinder-ogive,  
 $IR = 4$



general pointed body, maximum  
radius behind midpoint  
 $IR = 2$

Figure 3.- Body shapes.

Values for RC, RN and IR for several configurations are given in table I. The values in this table were obtained from reference 11. Let the axial

Location of maximum radius, x	IR	RC	RN
.3	1	1.71	6.03
.4	1	2.36	3.39
.5	1 or 2	4.00	2.00
.6	2	2.36	3.39
.7	2	1.71	6.03

Table I. - Parameters for general pointed body.

location of the maximum radius be designated as  $x_c$ . In general  $x_c$ , RC and RN are related as

$$x_c = 1 - \left( \frac{1}{RN} \right)^{\frac{1}{RN-1}}$$

$$RC = \frac{1}{1 - x_c - (1 - x_c)^{RN}}$$

for  $x_c \leq 1/2$  and as

$$x_c = \left( \frac{1}{RN} \right)^{\frac{1}{RN-1}}$$

$$RC = \frac{1}{x_c - x_c^{RN}}$$

for  $x_c \geq 1/2$

The configurations which can be treated can have stings. The radius of the sting is specified by the parameter  $RS$ , and the axial location where the sting starts has the axial index  $JS$ . The sting extends to  $J5$ . If there is to be no sting, let  $RS = 0$ , and  $JS = J3$ .

The lengths of the ogive sections of the ogive-cylinder-ogive are each one quarter of the body length.

### Wing

The wing shape, type of flow at the leading edge and algorithm for solving the linear-lift problem are specified with 6 fixed-point parameters and 4 floating-point parameters. The identities of the parameters  $JW1$ ,  $JW2$ ,  $JW3$  and  $JWD$  are indicated in figure 4 for wings with and without strakes.

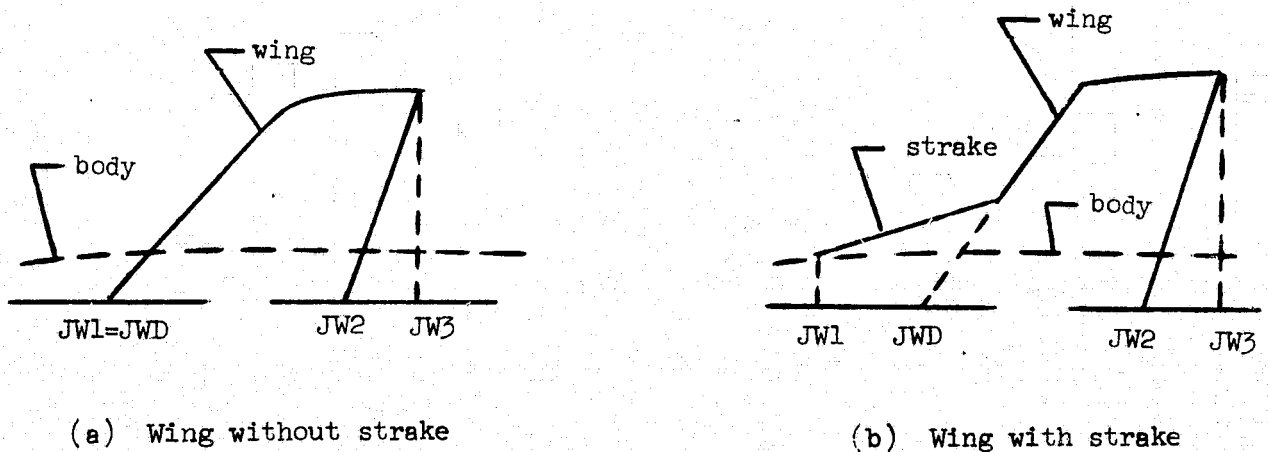


Figure 4.- Fixed-point wing parameters.

The leading and trailing edges of the wing are specified by the arrays  $Y2(J)$  and  $Y1(J)$ , respectively. In this report the trailing edge is a straight line. It may be swept or unswept. An upswept trailing edge is specified by setting  $JW2 = JW3$ . Two types of leading-edge shape are considered. Both types satisfy the condition that the tangent to the wing at the trailing edge is parallel to the free-stream direction so that the slender-wing solution satisfies the Kutta condition automatically.

The first leading-edge shape, which is depicted in figure 5, is a portion of a hyperbola. The foci of the hyperbola lie on the line with the

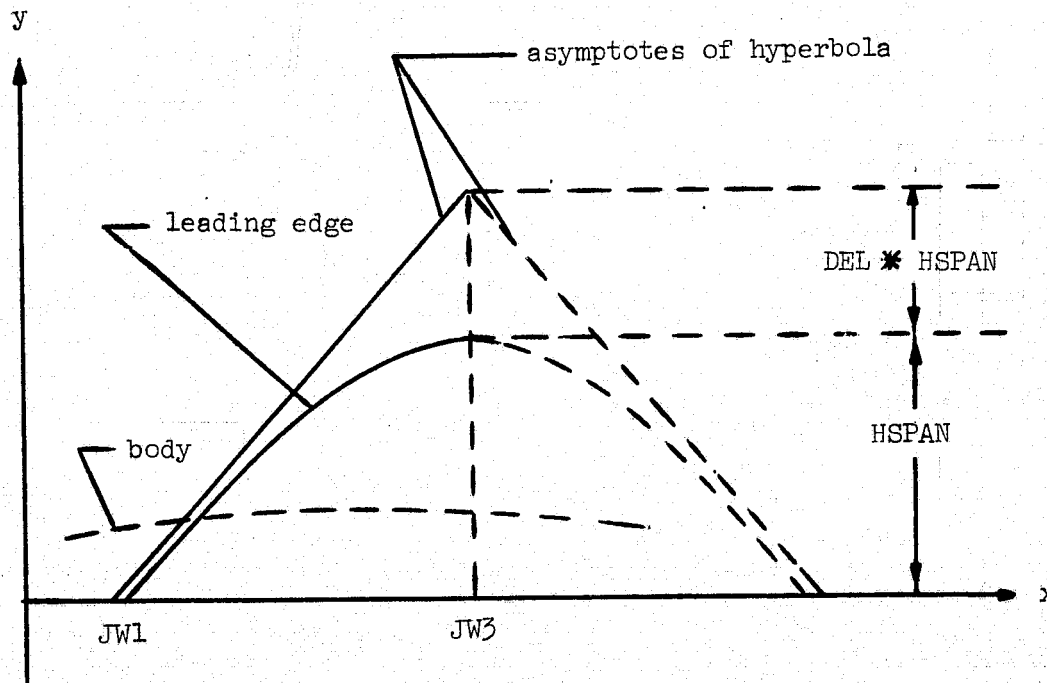


Figure 5.- First leading-edge shape.

index JW3. The wing shape is specified with the parameter IWING. The specification for the first leading-edge shape is  $IWING = 0$ . The only floating-point parameter which must be specified for this leading-edge shape is DEL. This parameter and HSPAN are depicted in figure 5.

The second leading edge shape is depicted in figure 6. This shape is

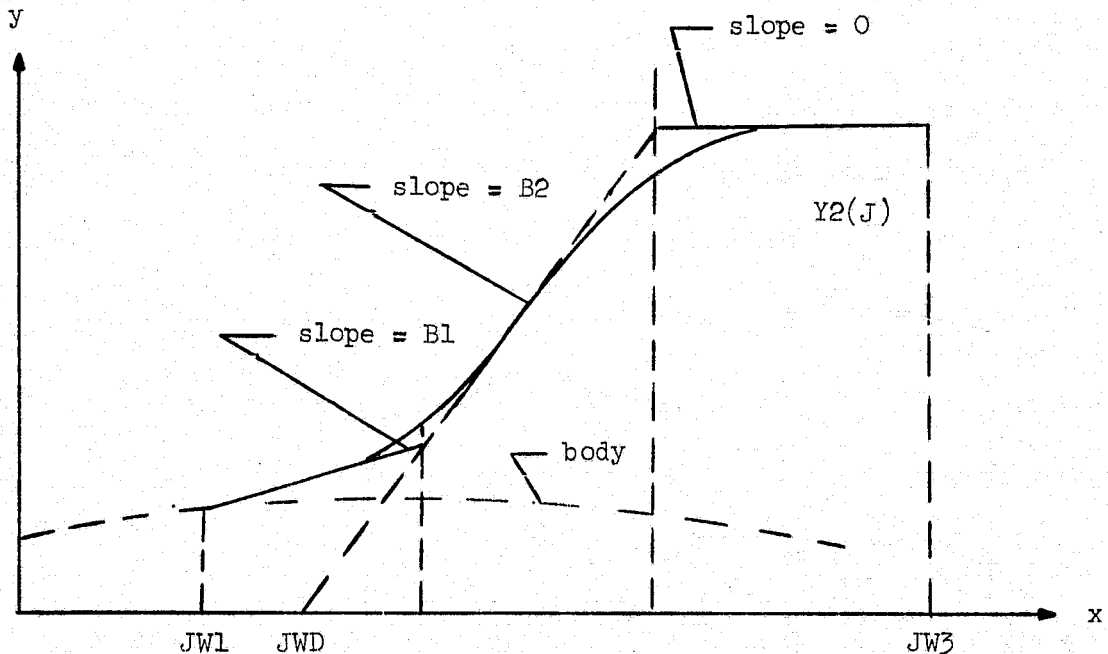


Figure 6.- Second leading-edge shape.

composed of two or three straight-line segments and one or two fillets. The specification for a wing without a strake is  $IWING = 1$  or  $IWING = -1$ . The parameter is positive if the linear lift solution is to be determined with slender wing theory and negative if quasi-conical theory or the theory of Lawrence and Flax is to be used. This wing is composed of two segments with the slopes  $B2$  and  $0$  as indicated in figure 6. The parameter DEL gives

the fractional difference in the local wingspan at the junction point with and without the fillet. The equation for this fractional difference is

$$DEL = (HSPAN - Y2)/HSPAN$$

For a wing without a strake any values will suffice for the parameters  $B1$  and  $DEL1$  since they are not used. The specification for a wing with a strake is  $IWING = 2$  or  $IWING = -2$ . This wing is composed of 3 segments with the slopes  $B1$ ,  $B2$  and  $0$  as shown in figure 6. The definition of the parameter  $DEL$  is the same as for a wing without a strake. The parameter  $DEL1$  has a similar definition. Let the  $y$  coordinate of the intersection point of the first two segments (the segments with the slopes  $B1$  and  $B2$ ) be designated as  $YI$ . The equation for  $DEL1$  is

$$DEL1 = (Y2 - YI)/YI$$

There are three options as to how the flow at the leading edge of the wing behaves. These options are designated with the parameter  $IVOR$ . If the flow is attached the parameter has the value  $IVOR = 0$ , and if the flow is separated at the leading edge the parameter has the value  $IVOR = 1$ . If the wing has a strake, the flow can be separated at the leading edge of the strake and attached on the wing. For this type of flow the parameter has the value  $IVOR = 2$ .

## Computational Parameters

There are two fixed-point and three floating-point parameters which are used to control the computation. As discussed in references 1 and 2, different approximations are used at points inside the wingtip and beyond the wingtip. In order to make the transition the outer region is divided into a thin inner strip and a broad outer strip. There are some differences in the way the problem is formulated in the two strips of the outer region. However, the solution is virtually independent of the relative widths of the two strips. The width of the inner strip is specified by the parameter IDIR. This parameter generally has been given the value 4 by the authors.

The convergence of the program is defined in terms of the maximum change in the velocity potential from one cycle to the next at all the grid points. The computation is terminated when the absolute value of the maximum change from one iteration cycle to the next at any grid location is less than the parameter EPSI. Also, the computation will be terminated if the number of iterations reaches IMAX.

The method of successive line overrelaxation is used in this program. The relaxation factor which is used at points where the flow is subsonic is input with the parameter SUB. This factor can be no larger than 2. At points where the flow is supersonic the relaxation factor is 1 unless the flow at the point immediately upstream is subsonic. If this circumstance pertains, the relaxation factor should be less than one. The value for this factor is input with the parameter SUP. Typically, this factor is given a value slightly less than 1.



## Plotting Parameter

The program output includes two or three figures. The first figure is a view of the configuration in the plane of constant  $\omega$  (see figure 1) and any shock waves or sonic lines which may be present. The second and third figures are plots of pressure distributions. The scale factor for plotting the first figure is input with the parameter SFACTOR. The number which is input is the number of unit lengths per inch which are to be used.

## DESCRIPTION OF PRINTED OUTPUT

The computational program is divided into 3 main parts called Program Start, Program Work, and Program Result. All three parts have output.

### Program Start

The function of Program Start is to establish the basic working constants and arrays used to make the numerical computation. All of these constants and arrays are printed at the end of Program Start. As mentioned previously, the axial and radial grid point locations are given by the arrays XW(J) and RW(K). The shape of the body and the leading and trailing edges of the wing are given by the arrays R(J), Y2(J) and Y1(J), respectively, and the axial derivative of the cross-sectional area is given by the array SPRIME(J). The axial indices of the first columns of grid points downstream of the points where the wing leading and trailing edges emerge from the body are designated as JW10 and JW20. In references 1 and 2, the dipole strength for the linear lift solution is designated by the function  $f(x)$ . In the program the dipole strength and the axial derivative of the dipole strength are given by the arrays FUN3(J) and FUN2(J) respectively.

The Brown and Michael model for leading-edge separation is used. This model represents the vortex system at the leading edge with a vortex core and vorticity feeding sheet. In this program the  $y$  and  $z$  locations of the vortex core are given by the arrays  $YV(JG)$  and  $ZV(JG)$  where the position index  $JG$  is related to the axial index  $J$  by the equation

$$JG = J - JWI\emptyset + 3$$

The vortex-core strength and the axial derivative of the strength are designated as  $GAN$  and  $DGANDX$ , respectively. As noted in the previous section, the flow is separated along the entire length of the leading edge if the separation input parameter is  $IV\emptyset R = 1$ . If the separation input parameter has the value  $IV\emptyset R = 2$  and the wing has a strake ( $IWING = 2$  or  $IWING = -2$ ) the flow is separated at the leading edge only along the strake. Aft of the strake the vortex trails across the wing and the flow is attached at the leading edge of the wing. The last axial station at which the flow at the leading edge is separated is designated by the parameter  $JCHCK$ .

#### Program Work

After each iteration cycle is completed, the largest change in the velocity potential and the grid location where this change is located are printed. The axial and radial indices are designated as  $JMARK$  and  $KMARK$ , respectively, and the change in velocity potential is designated as  $DPHIMX$ . As mentioned previously separate computations are made at points above and beneath the wing if the computational plane is the horizontal plane ( $\omega = 0^\circ$ ). If the position indices are negative the maximum change in velocity potential has occurred beneath the wing.

## Program Result

The computed results are printed in this part of the program. First the shock wave and sonic line locations at each axial station in the region of uniform axial grid ( $J2 \leq J \leq J3$ ) are printed. Provision is made for a total of as many as 6 shock waves and sonic lines at each axial station.

The next quantities to be printed are the pressure coefficients at all the grid points in the region of uniform axial grid. These are printed in rows from  $K=1$  to  $K=KF$  where  $KF = KM$  if a wall is present and  $KI = KM-1$  for free air. In general, the pressure coefficients are calculated with the approximate form of the linear lift potential used in Program Work. The pressure coefficient on both sides of the wing is printed if the flow is calculated on both sides of the wing. In addition, the pressure coefficients at points on the wing are calculated with a more accurate form of the linear lift potential.

The computed values of the potential for the coupled thickness-lift problem are printed next. If the flow beneath the wing is calculated, the potential beneath the wing is printed.

The distribution of the lift along the axis of the configuration is printed. In addition, vortex effects and thickness interaction effects are given. These quantities have been made nondimensional with the product  $\rho_{\infty} U_{\infty}^2$  where  $\rho_{\infty}$  and  $U_{\infty}$  are the free-stream density and speed. The lift, moment, moment arm about the nose and the lift and moment coefficients are also printed.

The pressure coefficient distribution on the body surface is determined and printed. If the configuration is at zero angle of attack so that the flow is axisymmetric only one distribution is given. If the configuration is at

angle of attack and the computational plane is the wing-plane ( $\omega = 0^\circ$ ) the distributions along the intersections of the body surface with the wing plane ( $\omega = 0^\circ$ ) and the vertical plane ( $\omega = +90^\circ, -90^\circ$ ), are given. Two distributions are given along the intersection of the body surface and wing plane, one for the pressure coefficient above the wing and one for the coefficient beneath the wing. The distributions which are obtained for the intersection of the body surface and vertical plane from the horizontal-plane calculation are simply surmised from the horizontal-plane results with the aid of slender-body and slender-wing theory. If the computational plane is the vertical plane ( $\omega = 90^\circ$  or  $\omega = -90^\circ$ ), only the distribution of the pressure coefficient along the intersection of the body surface and the computational plane is printed. When leading-edge vortices and strake-generated vortices are included, the pressure distributions both with and without vortex effects are printed. It should be noted that the body-surface pressure coefficients for lifting configurations are complete only if the computational plane is the horizontal plane ( $\omega = 0^\circ$ ) or the vertical plane ( $\omega = 90^\circ$  or  $\omega = -90^\circ$ ). Lift effects are not included for other values of  $\omega$ .

A number called DRAG is calculated and printed. This number is determined by integrating the surface pressure distribution. The accuracy of the present program is not good enough for this procedure to yield a meaningful value for the drag. It is not unusual for the sign of the number to be negative.

#### DESCRIPTION OF PLOTTED OUTPUT

The output includes either 2 or 3 plots, the first of which shows a view of the configuration and the shock-wave and sonic-line structure in the computational plane, and the second and third of which depict axial pressure-

coefficient distributions. If the configuration is at zero angle of attack only one distribution, the body-surface distribution is plotted. Four distributions are given on two plots if the configuration is lifting and the computational plane is the wing plane ( $\omega = 0^\circ$ ). These distributions are for the pressure coefficient along the intersection of the body surface and the wing plane above and beneath the wing and along the intersection of the body surface and the vertical plane ( $\omega = -90^\circ$ ). If the configuration is lifting and the computational plane is the vertical plane ( $\omega = 90^\circ$  or  $\omega = -90^\circ$ ) the distribution along the intersection of body surface and the side of the vertical plane which is being computed is given.

## ARRAY SIZE

There are eight `COMMON` statements. The first of these is for scalar quantities derived in the program and the last is for the input parameters. These second and third `COMMON` statements are for one-dimensional arrays in the axial direction and are dimensioned 120 in the listing given in appendix A. The fourth statement is for one-dimensional arrays in the radial direction which are dimensioned 100 in appendix A. If the grid size in the axial or radial direction is to exceed 120 or 100, respectively, the dimension of the corresponding arrays must be changed. The fifth and sixth statements are for the one-dimensional arrays in the radial and axial directions respectively, which are used to make computations under the wing of lifting configurations. These arrays are used only if the angle of attack is not zero and the computational plane is the wing plane ( $\omega = 0^\circ$ ). The dimension of the axial arrays must be at least as large as the number  $JW3 - JW10 + 4$  where  $JW3$  and  $JW10$  are the axial indices for the rear-most tip of the wing and the grid point either at or just downstream of the point where the leading edge of the wing intersects the body surface, respectively. It should be noted that  $JW3$  is an input parameter, and  $JW10$  is determined by the program. The dimension of the radial arrays must be at least as large as the index of the smallest value of the array  $RW(K)$  which is larger than the input parameter  $HSPAN$ . The dimensions of these radial and axial arrays in the listing in appendix A are 25 and 50 respectively. The two-dimensional arrays  $PHI(J,K)$  and  $PHIU(JG,K)$  for the general velocity potential and the velocity potential under the wing, respectively, are dimensioned in the seventh `COMMON` block. In the listing given in appendix A the axial and radial dimensions are

109 and 50, respectively, for the former array and 50 and 25, respectively, for the latter array. The seventh ~~COMMON~~, statement also contains the array for the coefficients used in the series solution for the linear lift obtained with Lawrence-Flax theory.

## APPENDIX A

### PROGRAM LISTING

The computational program is listed in this appendix. It is written in the Fortran IV computer language and contains two primary overlays. The numerical computation and the printing is done in the first primary overlay, which contains three secondary overlays. The figures are plotted in the second primary overlay.



	OVERLAY (DICK,0,0)	A	0
	PROGRAM EXEC (INPUT=201,OUTPUT,TAPE5=INPUT,TAPE7,TAPE1)	A	10
C		A	20
C		A	21
C	*****		23
C	*****		25
C	TRANSONIC FLOW ABOUT LIFTING WING-BODY COMBINATIONS	A	30
C		A	40
C	A3746-4	A	50
C		A	60
C		A	70
C	VARIAN PLJT CONTROL CARD SHOULD BE	A	80
C	PLOT.VARIAN( FSH=12.,FSV=11.)	A	90
C		A	100
	COMMON /CALLP/ NREAD,NCASES	A	110
	COMMON /NMLIST/ J1,J2,J3,J4,J5,FAC,KM,RCOM,A,B,IWALL,P,OMEGAD,ALPH	A	120
	1AD,HSPAN,AMINF,GAMMA,IR,RC,RMAX,RN,JS,RS,JW1,JW2,JW3,JWD,IWING,B1,	A	130
	2B2,DEL1,DEL,IVOR,IDIR,EPSI,SUB,SUP,IMAX,SFACTOR	A	140
	NREAD=0	A	150
	READ 30, NCASES,NPLOT	A	160
	DO 20 I=1,NCASES	A	170
	CALL OVERLAY (4HDICK,1,0,6HRECALL)	A	180
	IF (NPLOT.EQ.1) CALL OVERLAY (4HDICK,2,0,6HRECALL)	A	190
20	CONTINUE	A	200
	STOP 0101	A	210
C		A	220
30	FORMAT (10I5)	A	230
	END	A	240-

OVERLAY (DICK,1,0)  
 PRUGRAM ONEO

B 0  
 B 10  
 B 20  
 B 30  
 B 40  
 B 50  
 B 60  
 B 70  
 B 80  
 B 90  
 B 100  
 B 110  
 B 120  
 B 130  
 B 140  
 B 150  
 B 160  
 B 170  
 B 180  
 B 190  
 B 200  
 B 210  
 B 220  
 B 230  
 B 240  
 B 250  
 B 260  
 B 270  
 B 280  
 B 290  
 B 300  
 B 310  
 B 320  
 B 330  
 B 340  
 B 350  
 B 360  
 B 370  
 B 380  
 B 390  
 B 400  
 B 410

COMMON SIGMA,DELTA,I,BETASQ,DXR,DXSQR,GAMP1,GP1DXR,KMM1,KFM1,KF,DE  
 1LETA,PIR,CON4,CON5,H,JT,JI,JF,DPHIMX,DX,JXN,SNO,CS20,SNALP,IJW,JW1  
 20,JW20,JW1X,JW3X,BETA,JW3M1,DLTPH,JCHCK,IW,JW10M2,JW3P1,JW10M1,M,X  
 3WM,XWMSQR,PI,AK2,AX2,AK1,AX1,AX10,CNX,NAMXP1,A1,A2,ZMACH,JMCK  
 COMMON R(120),SPRIME(120),FUN(120),XW(120),Y1(120),Y2(120),FUN1(12  
 10),FUN0(120),IFUN(120),FUN2(120),FUN3(120),FUN4(120),IGUN(120),CP(1  
 2120),FUNX(120),SLAS(120,6),CPO(120),KLOA(120),KUPA(120),FUN5(120),  
 3FUN6(120),FUN7(120),FUNY(120),CP1(120),CP2(120)

COMMON FUN8(120),FUN9(120),FUN10(120),FUN11(120),Y2PRM(120),FUN12(1  
 1120),FUNA(120),FUN8(120)

COMMON CON7(100),CON8(100),CON9(100),CON10(100),CON11(100),CON1(10  
 10),CON2(100),CON3(100),OMEGA(100),ABAR(100),BBAR(100),CBAR(100),DB  
 2AR(100),PHIO(100),RW(100),RWR(100),AXOCR(100),ACHK(100),PHIOLD(100  
 3),BCHK(100)

COMMON PHIUD(25),OMEGAU(25),ACHKU(25),BBARU(25),CBARU(25),DBARU(25  
 1),BCHKU(25),PHIOU(25)

COMMON IFUM(50),VLAM(50),VTAU(50),VLAMP(50),VTAUP(50),YV(50),ZV(50  
 1),FUNAO(50),FUNBO(50),UUOD(50),UU9OD(50)

COMMON PHI(109,50),PHIU(50,25),CDEF(21)

COMMON /NMLIST/ J1,J2,J3,J4,J5,FAC,KM,RCOM,A,B,IWALL,P,OMEGAD,ALPH  
 1AD,HSPAN,AMINF,GAMMA,IR,RC,RMAX,RN,JS,RS,JW1,JW2,JW3,JWD,IWING,B1,  
 2B2,DEL1,DEL,IVOR,IDIR,EPSI,SUB,SUP,IMAX,SFACTOR  
 DIMENSION IDATE(2)

NAMelist /NAME/ J1,J2,J3,J4,J5,FAC,KM,RCOM,A,B,IWALL,P,OMEGAD,ALPH  
 1AD,HSPAN,AMINF,GAMMA,IR,RC,RMAX,RN,JS,RS,JW1,JW2,JW3,JWD,IWING,B1,  
 2B2,DEL1,DEL,IVOR,IDIR,EPSI,SUB,SUP,IMAX,SFACTOR

CALL DAYTIM (IDATE)

PRINT 30, IDATE

PRINT 20

PRINT 30, IDATE

PRINT 10

READ (5,NAME)

REWIND 1

PRINT NAME

PRINT 20

CALL OVERLAY (4HDICK,1,1,6HRECALL)

PRINT 20

CALL OVERLAY (4HDICK,1,2,6HRECALL)  
PRINT 20  
CALL OVERLAY (4HDICK,1,3,6HRECALL)  
RETURN

B 420  
B 430  
B 440  
B 450  
B 460  
B 470  
B 480  
B 490  
B 500  
B 510  
B 520-

C

10 FORMAT (//54H RUBY DAVIS - SUBSONIC-TRANSONIC AERODYNAMICS DIVISIO  
1N/31H FOR DICK BARNWELL A3746 - 4/52H TRANSONIC FLOW ABOUT LIFT  
2ING WING-BODY COMBINATIONS/)  
20 FORMAT (1H1//)  
30 FORMAT (8A10)  
END

OVERLAY (DICK,1,1)	C	0
PROGRAM START	C	10
COMMON SIGMA,DELTA,I,BETASQ,DXR,DXSQR,GAMP1,GP1DXR,KMM1,KFM1,KF,DE	C	20
1 LETA,PIR,CON4,CON5,H,JT,J1,JF,DPHIMX,DX,JXN,SNO,CS20,SNALP,IJW,JW1	C	30
20,JW20,JW1X,JW3X,BETA,JW3M1,DLTPH,JCHCK,IW,JW10M2,JW3P1,JW10M1,M,X	C	40
3WM,XWMSQR,PI,AK2,AX2,AK1,AX1,AX10,CNX,NAMXP1,A1,A2,ZMACH,JMCK	C	50
COMMON R(120),SPRIME(120),FUN(120),XW(120),Y1(120),Y2(120),FUN1(12	C	60
10),FUN0(120),IFUN(120),FUN2(120),FUN3(120),FUN4(120),IGUN(120),CP(	C	70
2120),FUNX(120),SLAS(120,6),CPO(120),KLOA(120),KUPA(120),FUN5(120),	C	80
3FUN6(120),FUN7(120),FUNY(120),CP1(120),CP2(120)	C	90
COMMON FUN8(120),FUN9(120),FUN10(120),FUN11(120),Y2PRM(120),FUN12(	C	100
1120),FUNA(120),FUNB(120)	C	110
COMMON CON7(100),CON8(100),CON9(100),CON10(100),CON11(100),CON1(10	C	120
10),CON2(100),CON3(100),OMEGA(100),ABAR(100),BBAR(100),CBAR(100),DB	C	130
2AR(100),PHIO(100),RW(100),RWR(100),AXOCR(100),ACHK(100),PHIOLD(100	C	140
3),BCHK(100)	C	150
COMMON PHIUD(25),OMEGAU(25),ACHKU(25),BBARU(25),CBARU(25),DBARU(25	C	160
1),BCHKU(25),PHIOU(25)	C	170
COMMON IFUM(50),VLAM(50),VTAU(50),VLAMP(50),VTAUP(50),YV(50),ZV(50	C	180
1),FUNAO(50),FUNBO(50),UUOD(50),UU9OD(50)	C	190
COMMON PHI(109,50),PHIU(50,25),COEF(21)	C	200
COMMON /NMLIST/ J1,J2,J3,J4,J5,FAC,KM,RCOM,A,B,IWALL,P,OMEGAD,ALPH	C	210
1AD,HSPAN,AMINF,GAMMA,IR,RC,RMAX,RN,JS,RS,JW1,JW2,JW3,JWD,IWING,B1,	C	220
2B2,DELI,DEL,IVOR,IDIR,EPSI,SUB,SUP,IMAX,SFACTOR	C	230
	C	240
PART 1 VARIOUS CONSTANTS,AXIAL AND RADIAL GRIDS	C	250
	C	260
RAD=57.29577951308	C	270
SNALP=SIN(ALPHAD/RAD)	C	280
SNO=SIN(OMEGAD/RAD)	C	290
CS20=1.-2.*SNO**2	C	300
IW=0	C	310
IF (ABS(SNO).LT.1.E-06.AND.ABS(SNALP).GT.1.E-06.AND.HSPAN.GT.RMAX)	C	320
1 IW=1	C	330
SIGMA=SNALP**2	C	340
DELTA=RMAX	C	350
I=0	C	360
BETASQ=1.-AMINF**2	C	370
AJ1=J1	C	380
AJ2=J2	C	390
AJ3=J3	C	400
DX=1./(AJ3-AJ2)	C	410

```

DDX=(AJ2-AJ1)*DX
JJF=J4-J1+1
DO 10 JJ=1,JJF
10 XW(J1+JJ-1)=FLOAT(JJ-1)*DX-DDX
IF (J1.EQ.1) GO TO 30
J1M1=J1-1
DO 20 JJ=1,J1M1
JJM1=JJ-1
J=J1-JJ
JP1=J+1
20 XW(J)=XW(JP1)-DX*FAC**JJM1
30 IF (J4.EQ.J5) GO TO 50
J5MJ4=J5-J4
DO 40 JJ=1,J5MJ4
JJM1=JJ-1
J=J4+JJ
JM1=J-1
40 XW(J)=XW(JM1)+DX*FAC**JJM1
50 DXR=1./DX
DXSQR=DXR**2
GAMP1=(GAMMA+1.)*AMINF**2
GP1DXR=GAMP1*DXR
KMM1=KM-1
KF=KMM1
IF (IWALL.NE.0) KF=KM
KFM1=KF-1
AKM=KM
DELETA=1./AKM
DO 60 K=2,KF
AK=K
ETA=AK*DELETA
BMAEK=B-A*ETA
ETAR=1./((ETA+BMAEK*RCOM)
BMAEKR=1./BMAEK
CON1(K)=.5*DELETA*BMAEKR*(B*ETAR-2.*A)
CON=(B*DELETA*BMAEKR)**2
CON2(K)=CON*BMAEKR**2
60 CON3(K)=CON*ETAR**2
CON1(1)=1.
BMADE=B-A*DELETA
BMADER=1./BMADE
TBMADE=2.*B-A*DELETA
TBMADR=1./TBMADE

```

```

C 420
C 430
C 440
C 450
C 460
C 470
C 480
C 490
C 500
C 510
C 520
C 530
C 540
C 550
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C 580
C 590
C 600
C 610
C 620
C 630
C 640
C 650
C 660
C 670
C 680
C 690
C 700
C 710
C 720
C 730
C 740
C 750
C 760
C 770
C 780
C 790
C 800
C 810
C 820
C 830
C 840

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BMTADE=B-2.*A*DELETA	C 850
BMTADR=1./BMTADE	C 860
F1=DELETA+BMADE*RCOM	C 870
F2=3.*DELETA+(2.*B-3.*A*DELETA)*RCOM	C 880
CON=8.*(B*DELETA)**2*BMTADR*TBMADE/F2	C 890
CON2(1)=CON*F1*BMADE**2	C 900
CON3(1)=CON/F1	C 910
PI=3.141592654	C 920
PIR=1./PI	C 930
CON4=PIR*B*DELETA*(2.*B-3.*A*DELETA)/F2*BMTADR*BMADE	C 940
IF (I WALL.NE.0) H=P*B*DELETA/(B-A)**2*(1.+5*B*DELETA/(B-A))	C 950
J1=2	C 960
JF=J5-1	C 970
IF (AMINF.LE.1.) GO TO 70	C 980
J1=3	C 990
70 JT=J1+JF	C1000
DO 90 K=1,KF	C1010
AK=K	C1020
ETA=AK*DELETA	C1030
RW(K)=ETA/(B-A*ETA)+RCOM	C1040
ARG=1.+BETASQ*RW(K)**2	C1050
IF (ARG.LT.0.) GO TO 80	C1060
AXOCR(K)=1./SQRT(ARG)	C1070
80 RWR(K)=SNALP*SNO/RW(K)	C1080
CON10(K)=CON2(K)*SNALP*SNO*RW(K)	C1090
CON11(K)=CON2(K)*RW(K)**2	C1100
CON7(K)=2.*CON3(K)*RWR(K)**2	C1110
CON8(K)=SNALP**2*CON2(K)*RW(K)**2	C1120
CON9(K)=SNALP**2*CON2(K)*RW(K)	C1130
90 ABAR(K)=1.-CON1(K)	C1140
	C1150
PART 2 BODY GEOMETRY	C1160
	C1170
J2M1=J2-1	C1180
DO 100 J=1,J2M1	C1190
R(J)=0.	C1200
100 SPRIME(J)=0.	C1210
COM=RC*RMX	C1220
JSM1=JS-1	C1230
IF (IR.EQ.1) GO TO 120	C1240
IF (IR.EQ.2) GO TO 140	C1250
IF (IR.EQ.3) GO TO 160	C1260
IF (IR.EQ.4) GO TO 180	C1270

DO 110 J=J2,JSM1	C1280
Y=1.-XW(J)	C1290
R(J)=COM*(Y-Y**RN)	C1300
110 SPRIME(J)=2.*PI*COM*(RN*Y**((RN-1.)-1.))*R(J)	C1310
GO TO 220	C1320
120 DO 130 J=J2,JSM1	C1330
R(J)=COM*(XW(J)-XW(J)**RN)	C1340
130 SPRIME(J)=2.*PI*COM*(1.-RN*XW(J)**(RN-1.))*R(J)	C1350
GO TO 220	C1360
140 DO 150 J=J2,JSM1	C1370
Y=1.-2.*XW(J)	C1380
R(J)=RMAX*SQRT(ABS(1.-Y**2))	C1390
150 SPRIME(J)=4.*PI*RMAX**2*Y	C1400
SPRIME(J2)=0.	C1410
GO TO 220	C1420
160 DO 170 J=J2,JSM1	C1430
R(J)=RMAX*XW(J)	C1440
170 SPRIME(J)=2.*PI*RMAX*R(J)	C1450
GO TO 220	C1460
180 DO 210 J=J2,JSM1	C1470
IF (XW(J).GT..25) GO TO 190	C1480
R(J)=8.*RMAX*XW(J)*(1.-2.*XW(J))	C1490
SPRIME(J)=2.*PI*R(J)*8.*RMAX*(1.-4.*XW(J))	C1500
GO TO 210	C1510
190 IF (XW(J).GT..75) GO TO 200	C1520
R(J)=RMAX	C1530
SPRIME(J)=0.	C1540
GO TO 210	C1550
200 R(J)=8.*RMAX*(1.-XW(J))*(2.*XW(J)-1.)	C1560
SPRIME(J)=2.*PI*R(J)*8.*(3.-4.*XW(J))*RMAX	C1570
210 CONTINUE	C1580
220 DO 230 J=J5,J5	C1590
R(J)=RS	C1600
230 SPRIME(J)=0.	C1610
	C1620
C PART 3 WING GEOMETRY	C1630
C	C1640
C	C1650
IF (JW3.GT.JW2) CAA1=HSPAN/(XW(JW3)-XW(JW2))	C1660
JW1P1=JW1+1	C1670
JW2P1=JW2+1	C1680
JW3P1=JW3+1	C1690
M=JW3	C1700
ZMACH=0.	

DO 240 J=1,JW1	C1710
FUNA(J)=1.	C1720
FUNB(J)=0.	C1730
FUN5(J)=0.	C1740
FUN6(J)=0.	C1750
FUN7(J)=0.	C1760
FUN2(J)=0.	C1770
FUN3(J)=R(J)**2	C1780
FUN4(J)=0.	C1790
IGUN(J)=IDIR	C1800
Y2PRM(J)=0.	C1810
FUNO(J)=0.	C1820
Y2(J)=0.	C1830
IFUN(J)=0	C1840
240 FUN(J)=0.	C1850
CNN1=1./((XW(JW3)-XW(JW1))	C1860
CNN2=HSPAN**4*CNN1**3*GAMP1*(1.+2.*DEL)**2	C1870
DELP1=DEL+1.	C1880
TDELP1=2.*DEL+1.	C1890
DELSQ=DEL**2	C1900
CNX=1.	C1910
IF (SND.LT.-1.E-06) CNX=-1.	C1920
CNNA=CNX*HSPAN*TDELP1*CNN1*SNALP	C1930
CNNAO=HSPAN*TDELP1*CNN1	C1940
CNNB=-CNX*HSPAN*TDELP1*DELSQ*CNN1**2*SNALP	C1950
JW1O=JW1P1	C1960
JW2O=JW2+1	C1970
CNN6=(GAMP1*CNN1**3)**3*(HSPAN**2*TDELP1)**4/128.	C1980
JCHCK=JW3	C2000
IF (IWING.EQ.0) GO TO 250	C2010
A2=-B2*(XW(JWD)-XW(JW1))	C2020
AX2=(HSPAN-A2)/B2	C2030
AY2=A2+B2*AX2	C2040
IF (AY2.LT.1.E-06) AY2=1.E-06	C2050
AK2=B2/(DEL*AY2)	C2060
IF (IWING.NE.2.AND.IWING.NE.-2) GO TO 250	C2070
A1=R(JW1)	C2080
AX1=-(A2-A1)/(B2-B1)	C2090
AX1O=AX1+XW(JW1)	C2100
AY1=A1+B1*AX1	C2110
IF (AY1.LT.1.E-06) AY1=1.E-06	C2120
AK1=(B2-B1)/(AY1*ABS(DEL1))	C2130
JCHCK=JW1	C2140



250	DO 410 J=JW1P1,JW3	C2150
	FUNA(J)=1.	C2160
	FUNB(J)=0.	C2170
	IF (IWING.NE.0) GO TO 260	C2180
	AX=(XW(JW3)-XW(J))*CNN1	C2190
	CNN3=SQRT(ABS(DEL SQ+TDELP1*AX**2))	C2200
	CNN4=1./CNN3	C2210
	Y2(J)=HSPAN*(DELP1-CNN3)	C2220
	FUNO(J)=HSPAN**2*CNN1*(DELP1*CNN4-1.)*TDELP1*AX	C2230
	IF (Y2(J).LT.3(J)) GO TO 400	C2240
	ROY2E4=(R(J)/Y2(J))**4	C2250
	FACO=1.-ROY2E4	C2260
	FUN(J)=.5*FACO**2*CNN2*(DELP1*CNN4-1.)*(1.-DELP1*DELSQ*CNN4**3)*AX	C2270
1	+2.*FACO*ROY2E4*FUNO(J)**3/Y2(J)**2*GAMP1	C2280
	FUNOJ=FUNO(J)	C2290
	FUN2(J)=FACO*FUNO(J)	C2300
	FUNO(J)=.5*FACO*(HSPAN*CNN1)**2*(1.-DELP1*DELSQ*CNN4**3)*TDELP1+2.	C2310
1	*ROY2E4*(FUNO(J)/Y2(J))**2	C2320
	IF (J.GT.JW2) GO TO 340	C2330
	GO TO 320	C2340
260	AX=XW(J)-XW(JW1)	C2350
	BX=AK2*(AX-AX2)	C2360
	IF (BX.LT.-100.) BX=-100.	C2370
	IF (BX.GT.100.) BX=100.	C2380
	IF (ABS(BX).LT.1.E-06) GO TO 270	C2390
	CX=EXP(-BX)	C2400
	XD=1./(1.-CX)	C2410
	Y2(J)=-B2*(AX-AX2)*XD	C2420
	Y2JP=-B2*(1.-(1.+BX)*CX)*XD**2	C2430
	Y2JDP=-B2*AK2*CX*(BX*(1.+CX)*XD-2.)*XD**2	C2440
	GO TO 280	C2450
270	Y2(J)=-B2/BX	C2460
	Y2JP=-.5*B2	C2470
	Y2JDP=-.5*B2*AK2	C2480
280	IF (IWING.EQ.2.OR.IWING.EQ.-2) GO TO 290	C2490
	Y2(J)=A2+B2*AX+Y2(J)	C2500
	Y2JP=B2+Y2JP	C2510
	GO TO 310	C2520
290	BX=AK1*(AX-AX1)	C2530
	IF (XW(J).LT.AX10) JCHCK=J-1	C2540
	IF (BX.LT.-100.) BX=-100.	C2550
	IF (BX.GT.100.) BX=100.	C2560
	IF (ABS(BX).LT.1.E-06) GO TO 300	C2570

CX=EXP(-BX)	C2580
XD=1./(1.-CX)	C2590
Y2(J)=Y2(J)+(B2-B1)*(AX-AX1)*XD+A1+B1*AX	C2600
Y2JP=Y2JP+(B2-B1)*(1.-(1.+BX)*CX)*XD**2+B1	C2610
Y2JDP=Y2JDP+(B2-B1)*AK1*CX*(BX*(1.+CX)*XD-2.)*XD**2	C2620
GO TO 310	C2630
300 Y2(J)=Y2(J)+A1+B1*AX+(B2-B1)/BX	C2640
Y2JP=Y2JP+.5*(B2-B1)	C2650
310 IF (Y2(J).LT.R(J)) GO TO 400	C2660
JG=J-JW10+3 \$ FUNAO(JG)=1. \$ FUNBO(JG)=0.	C2661
ROY2E4=(R(J)/Y2(J))**4	C2670
FACO=1.-ROY2E4	C2680
FUNOJ=Y2(J)*Y2JP	C2690
FUN2(J)=FACO*FUNOJ	C2700
FDP=Y2(J)*Y2JDP+Y2JP**2	C2710
FUN(J)=.5*GAMP1*FACO*FUNOJ*FDP	C2720
FUNO(J)=.5*FACO*FDP	C2730
IF (J.GT.JW2) GO TO 340	C2740
320 FUN3(J)=.5*Y2(J)**2*(1.+ROY2E4)	C2750
IJW=J+1	C2760
JW20=IJW	C2770
IF (IWING.NE.0) GO TO 330	C2780
FUN4(J)=CNNA*AX*CNN4	C2790
FUN4(J)=FUN4(J)*(1.+(1.-2.*SNO**2)*(R(J)/Y2(J))**2)	C2800
Y2PRM(J)=CNNAO*AX*CNN4	C2810
FUN5(J)=CNNB*CNN4**3	C2820
GO TO 360	C2830
330 FUN4(J)=CNX*SNALP*Y2JP	C2840
FUN4(J)=FUN4(J)*(1.+(1.-2.*SNO**2)*(R(J)/Y2(J))**2)	C2850
Y2PRM(J)=Y2JP	C2860
FUN5(J)=CNX*SNALP*Y2JDP	C2870
GO TO 360	C2880
340 Y1(J)=CAA1*(XW(J)-XW(JW2))	C2890
IF (J.EQ.JW3) Y1(J)=Y2(J)	C2900
IF (Y1(J).LE.R(J)) GO TO 320	C2910
AKBAR=Y1(J)/Y2(J)	C2920
ANUM1=(1.-AKBAR)/(1.+AKBAR)	C2930
FUN2(J)=.85*FACO*FUNO(J)*ANUM1	C2940
ROY2E2=(R(J)/Y2(J))**2	C2950
ROY1E2=(R(J)/Y1(J))**2	C2960
AKPRM=1./((1.-ROY2E2)*Y2(J))*((1.+ROY1E2)*CAA1-(1.-ROY1E2)*(1.+ROY	C2970
12E2)*Y1(J)*FUNOJ/((1.-ROY2E2)*Y2(J)))	C2980
FUN(J)=.7225*(FUN(J)*ANUM1-.5*GAMP1*(FUNOJ*FACO/(1.+AKBAR))**2*AKP	C2990

1 RM)	C3000
FUNO(J)=.85*FUNO(J)*SQRT(ABS(ANUM1))	C3010
IF (J.EQ.JW3) GO TO 350	C3020
FUNO(J)=FUNO(J)-.425*FUNOJ*(1.-ROY2E4)*AKPRM/SQRT((1.-AKBAR)*(1.+A	C3030
1KBAR)**3)	C3040
350 FUN4(J)=0.	C3050
FUN5(J)=0.	C3060
IF (IWING.EQ.0) Y2PRM(J)=CENNAO*AX*CNN4	C3070
IF (IWING.NE.0) Y2PRM(J)=Y2JP	C3080
360 IF (IVOR.EQ.0.OR.J.GT.JW10) GO TO 370	C3090
RBP=.5*PIR*SPRIME(J)/R(J)	C3100
CHEKK=(Y2(J)-R(J))/((Y2PRM(J)-RBP)*DX)	C3110
IF (CHEKK.LT..1) GO TO 400	C3120
370 ETA=0.	C3130
KJ=0	C3140
380 ETA=ETA+DELETA	C3150
KJ=KJ+1	C3160
RAD=ETA/(B-A*ETA)+RCOM	C3170
IF (RAD.GT.Y2(J)) GO TO 390	C3180
GO TO 380	C3190
390 IFUN(J)=KJ-1	C3200
IF (IFUN(J).EQ.0) IFUN(J)=1	C3210
IGUN(J)=IDIR+IFUN(J)	C3220
GO TO 410	C3230
400 IFUN(J)=0	C3240
IGUN(J)=IDIR	C3250
FUN4(J)=0.	C3260
FUN5(J)=0.	C3270
FUN6(J)=0.	C3280
FUN7(J)=0.	C3290
Y2PRM(J)=0.	C3300
FUN(J)=0.	C3310
FUNO(J)=0.	C3320
I JW=J+1	C3330
FUN2(J)=.0	C3340
FUN3(J)=R(J)**2	C3350
JW10=J+1	C3360
410 CONTINUE	C3370
FUNAO(2)=1.	C3371
JMCK=JW10-1	C3372
JW10M2=JW10-2	C3380
JW3P1=JW3+1	C3390
JW10M1=JW10-1	C3400

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JW3M1=JW3-1
IF (I JW.EQ.JW3P1) GO TO 430
DO 420 J=I JW,JW3
420 FUN3(J)=FUN3(J-1)+.5*DX*(FUN2(J)+FUN2(J-1))
430 DO 440 J=JW3P1,J5
FUNA(J)=1.
FUNB(J)=0.
FUN5(J)=0.
FUN6(J)=0.
FUN7(J)=0.
FUN2(J)=0.
FUN3(J)=FUN3(JW3)
FUN4(J)=0.
IGUN(J)=IGUN(JW3)
Y2PRM(J)=0.
Y2(J)=Y2(JW3)
IFUN(J)=IFUN(JW3)
FUNO(J)=0.
440 FUN(J)=0.
DO 450 J=J,J2
IF (XW(J).LT.-1.) GO TO 450
JXN=J
GO TO 460
450 CONTINUE
460 DLTPH=0.
IF (I WING.LT.0) CALL MACH

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C  
C  
C

#### PART 4 VORTEX OVER WING

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IF (I VOR.EQ.0) GO TO 720
IF (I VOR.NE.2) JCHCK=JW3
JHKM1=JCHCK-1
JAM=128
AJAM=JAM
AJAMR=1./AJAM
ADX2=DX*AJAMR
Y2P=Y2PRM(JW10)
RBP=.5*PIR*SPRIME(JW10)/R(JW10)
TOT=(1.-(Y2(JW10)-R(JW10))/(DX*(Y2P-RBP)))*AJAM+1.
NTOT=TOT
JT=JAM-NTOT
AJT=JT
RB=R(JW10)-RBP*AJT*ADX2

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C3410  
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C3780  
C3790  
C3800  
C3810  
C3820

Y2B=Y2(JW10)-Y2P*AJT*ADX2	C3830
RATIO=FUNA(JW10)-FUNB(JW10)*AJT*ADX2	C3840
RATIOP=FUNB(J)	C3841
ANUM0=SNALP/(Y2P-RBP)*RATIO	C3850
YA=-.00451+.56114*ANUM0-.12152*ANUM0**2	C3860
YVT=RB+(Y2B-RB)*(.99031-.98407*YA+2.29481*YA**2-1.78322*YA**3)	C3870
ZVT=(Y2B-RB)*YA	C3880
HB=Y2B+RB**2/Y2B	C3890
HBP=(1.-(RB/Y2B)**2)*Y2P+2.*RB/Y2B*RBP	C3900
AF1=(Y2B-RB)/RB	C3910
AF2=(YVT-RB)/RB	C3920
AF3=ZVT/RB	C3930
ANUM1=AF2**2-AF1**2-AF3**2	C3940
ETA=1.+.5*ANUM1	C3950
XI=AF2*AF3	C3960
ANUM2=SQRT(ANUM1**2+4.*(ETA*XI)**2)	C3970
BLAM=.70710678*SQRT(ANUM1+ANUM2)	C3980
BTAU=ETA*XI/BLAM	C3990
JSTAT=JW10-1	C4000
IF (NTOT.LE.0) GO TO 470	C4010
JJ2=JAM	C4020
JJ1=NTOT+1	C4030
GO TO 480	C4040
470 JJ2=JT	C4050
JJ1=1	C4060
480 DO 650 J=JSTAT,JW3	C4070
JG=J-JW10+3	C4080
L=JG	C4090
DO 640 JJ=JJ1,JJ2	C4100
AJJ=JJ	C4110
ADX3=ADX2	C4120
IQ=1	C4130
RBG=RB	C4140
Y2BG=Y2B	C4150
RBPB=RB	C4160
Y2PB=Y2P	C4170
HBG=HB	C4180
HBPB=HBP	C4190
BLAMG=BLAM	C4200
BTAUG=BTAU	C4210
RATIOG=RATIO	C4220
RATIOPG=RATIOP	C4221
490 AIQ=IQ	C4230

AIQR=1./AIQ	C4240
DO 640 IS=1,IQ	C4250
AIS=IS	C4260
ABC1=AJAMR*(AJAM-AJJ+1.-(AIS-.5)*AIQR)	C4270
ABC2=1.-ABC1	C4280
ABC3=ABC1-.5*AJAMR*AIQR	C4290
ABC4=1.-ABC3	C4300
IIC=1	C4310
500 ANUM1=1.+BLAM**2-BTAU**2	C4320
ANUM2=SQRT(ANUM1**2+4.*(BLAM*BTAU)**2)	C4330
ETA=.70710678*SQRT(ANUM1+ANUM2)	C4340
XI=BLAM*BTAU/ETA	C4350
CHCEK=Y2B/RB-1.	C4360
IF (CHCEK.LT..01) GO TO 510	C4370
ANUM10=ETA**2+XI**2+4.*(RB/HB)**2	C4380
ANUM20=SQRT(ABS(ANUM10**2-16.*(ETA*RB/HB)**2))	C4390
ARG=ETA**2+.5*(ANUM20-ANUM10)	C4400
GO TO 520	C4410
510 AF1=(Y2B-RB)**2	C4420
AF2=BLAM**2-BTAU**2	C4430
AF3=1./RB**2	C4440
ANUM10=.5*(AF1*AF3+AF2)	C4450
ANUM20=AF3*SQRT(AF1*(AF1+2.*RB**2*AF2)+RB**4*(BLAM**2+BTAU**2)**2)	C4460
ARG=ANUM10+.5*ANUM20	C4470
520 YVT=.5*HB*(ETA+SQRT(ABS(ARG)))	C4480
ZVT=XI*HB*YVT/(2.*YVT-ETA*HB)	C4490
ANUM=RB**2/(YVT**2+ZVT**2)	C4500
FNUM2=HB*(BLAM**2+BTAU**2)	C4510
AY=(YVT*BLAM+ZVT*BTAU)/FNUM2	C4520
AZ=(YVT*BTAU-ZVT*BLAM)/FNUM2	C4530
BY=(YVT**2-ZVT**2)**2-4.*(YVT*ZVT)**2	C4540
BZ=4.*YVT*ZVT*(YVT**2-ZVT**2)	C4550
ANUM3=RB**4/(BY**2+BZ**2)	C4560
BYO=1.-ANUM3*BY	C4570
BZO=-ANUM3*BZ	C4580
CY=AY*BYO-AZ*BZO	C4590
CZ=AZ*BYO+AY*BZO	C4600
DY=(AY**2-AZ**2)*BYO-2.*AY*AZ*BZO	C4610
DZ=2.*AY*AZ*BYO+(AY**2-AZ**2)*BZO	C4620
ANUM4=1./(YVT**2+ZVT**2)	C4630
ANUM5=ANUM*ANUM4	C4640
DYO=1.+3.*(YVT**2-ZVT**2)*ANUM5	C4650
DZO=6.*YVT*ZVT*ANUM5	C4660

ANUM6=1./ (BYO**2+BZO**2)	C4670
EY=ANUM6*(BYO*DYO+BZO*DZO)	C4680
EZ=ANUM6*(BYO*DZO-BZO*DYO)	C4690
FY=ANUM4*(ZVT*(EY-DY)-YVT*(DZ-EZ))	C4700
FZ=ANUM4*(YVT*(DY-EY)+ZVT*(EZ-DZ))	C4710
IF (J.GT.JCHCK) GO TO 530	C4720
IF (J.EQ.JCHCK.AND.JJ.GE.2) GO TO 530	C4730
GAN=.5*HB*(BLAM+BTAU**2/BLAM)	C4740
GAN=GAN*RATIO	C4750
GANSAB=GAN	C4760
AMY=(YVT-Y2B)*HB*RATIO *.5/GAN*(1.-(BTAU/BLAM)**2)	C4770
AMZ=ZVT*HB*RATIO *.5/GAN*(1.-(BTAU/BLAM)**2)	C4780
ANY=(YVT-Y2B)*HB*RATIO *BTAU/(GAN*BLAM)	C4790
ANZ=ZVT*HB*RATIO *BTAU/(GAN*BLAM)	C4800
APY=(YVT-Y2B)/RATIO	C4801
APZ=ZVT/RATIO	C4802
AOY=(YVT-Y2B)/HB	C4810
AOZ=ZVT/HB	C4820
GO TO 540	C4830
530 GAN=GANSAB	C4840
AMY=0.	C4850
AMZ=0.	C4860
ANY=0.	C4870
ANZ=0.	C4880
AOY=0.	C4890
AOZ=0.	C4900
APY=0.	C4900
APZ=0.	C4902
540 ANUM7=HB*BYO*ANUM4*ANUM6	C4910
ANUM8=HB*BZO*ANUM4*ANUM6	C4920
ANUM9=BLAM*YVT+BTAU*ZVT	C4930
ANUM10=BTAU*YVT-BLAM*ZVT	C4940
OY=ANUM7*ANUM9-ANUM8*ANUM10	C4950
OZ=ANUM7*ANUM10+ANUM8*ANUM9	C4960
GYO=(RB*ANUM4)**2*(YVT**2-ZVT**2)	C4970
GZO=-2.*YVT*ZVT*(RB*ANUM4)**2	C4980
GY=ANUM4/((1.-GYO)**2+GZO**2)*(YVT*(1.-GYO)+ZVT*GZO)	C4990
GZ=ANUM4/((1.-GYO)**2+GZO**2)*(YVT*GZO-ZVT*(1.-GYO))	C5000
GBARY=ANUM4*ANUM6*(YVT*BYO+ZVT*BZO)	C5010
GBARZ=ANUM4*ANUM6*(YVT*BZO-ZVT*BYO)	C5020
H11=OY*HB+AMY	C5030
H12=-OZ*HB+ANY	C5040
H21=OZ*HB+AMZ	C5050

H22=OY*HB+ANZ	C5060
H1=-SNALP*(CZ*RATIO-.5*GAN*(CZ/(BLAM*HB)-FY))*RB*(YVT*ANUM4+2.*GY)	C5070
1*RBP-(OY*BLAM-OZ*BTAU+AOY*HB*GBARY)*HBP-APY*RATIO	C5080
H2=SNALP*(CY*RATIO-.5*GAN*(CY/(BLAM*HB)+FZ))*RB*(ZVT*ANUM4+2.	C5090
1*GZ)*RBP-(OZ*BLAM+OY*BTAU+AOZ*HB*GBARZ)*HBP-APZ*RATIO	C5100
BNUMO=1./(H11*H22-H12*H21)	C5110
BNUM1=H1*BNUMO	C5120
BNUM2=H2*BNUMO	C5130
BLAMP=BNUM1*H22-BNUM2*H12	C5140
BTAUP=BNUM2*H11-BNUM1*H21	C5150
IF (IIC.GT.1) GO TO 580	C5160
IIC=2	C5170
BLAMO=BLAM	C5180
BTAUO=BTAU	C5190
BLAMP1=BLAMP	C5200
BTAUP1=BTAUP	C5210
BLAM=BLAM+.5*ADX3*BLAMP	C5220
BTAU=BTAU+.5*ADX3*BTAUP	C5230
IF (JJ.NE.1.OR.IQ.NE.1.OR.J.LT.JW10) GO TO 550	C5240
VLAMP(JG)=BLAMP	C5250
VTAUP(JG)=BTAUP	C5260
YV(JG)=YVT	C5270
ZV(JG)=ZVT	C5280
IF (J.EQ.JW3) GO TO 650	C5290
550 IF (J.LT.JW10) GO TO 560	C5300
RB=ABC1*R(J)+ABC2*R(J+1)	C5310
Y2B=Y2(J)*ABC1+Y2(J+1)*ABC2	C5320
RATIO=FUNA(J)*ABC1+FUNA(J+1)*ABC2	C5330
RATIO=FUNB(J)*ABC1+FUNB(J+1)*ABC2	C5331
RBP=.5*PIR*(SPRIME(J)/R(J)*ABC1+SPRIME(J+1)/R(J+1)*ABC2)	C5340
Y2P=Y2PRM(J)*ABC1+Y2PRM(J+1)*ABC2	C5350
GO TO 570	C5360
560 RB=R(JW10)-ABC1*DX*RBP	C5370
Y2B=Y2(JW10)-ABC1*DX*Y2P	C5380
RATIO=FUNA(JW10)-ABC1*DX*FUNA(JW10)	C5390
RATIO=FUNB(JW10)	C5391
570 HB=Y2B*RB**2/Y2B	C5400
HBP=Y2P*(1.-(RB/Y2B)**2)+2.*RB/Y2B*RBP	C5410
GO TO 500	C5420
580 IF (IIC.GT.2) GO TO 590	C5430
IIC=3	C5440
BLAM=BLAMO+.5*ADX3*BLAMP	C5450
BTAU=BTAUO+.5*ADX3*BTAUP	C5460



BLAMP2=BLAMP	C5470
BTAUP2=BTAUP	C5480
GO TO 500	C5490
590 IF (IIC.GT.3) GO TO 630	C5500
CHECKL=ABS((BLAMP2-BLAMP)/BLAMP2)	C5510
CHECKU=ABS((BTAUP2-BTAUP)/BTAUP2)	C5520
IF (CHECKL.LT..01.OR.CHECKU.LT..01) GO TO 600	C5530
RB=RBG	C5540
Y2B=Y2BG	C5550
RBP=RBPB	C5560
Y2P=Y2PB	C5570
HB=HBG	C5580
HBP=HBPB	C5590
BLAM=BLAMB	C5600
BTAU=BTAUB	C5610
IQ=2*IQ	C5620
ADX3=.5*ADX3	C5630
RATIO=RATIOG	C5640
RATIOB=RATIOB	C5641
GO TO 490	C5650
600 IIC=4	C5660
BLAM=BLAMB+ADX3*BLAMP	C5670
BTAU=BTAUB+ADX3*BTAUP	C5680
BLAMP3=BLAMP	C5690
BTAUP3=BTAUP	C5700
IF (J.LT.JW10) GO TO 610	C5710
RB=ABC3*R(J)+ABC4*R(J+1)	C5720
Y2B=ABC3*Y2(J)+ABC4*Y2(J+1)	C5730
RATIO=FUNA(J)*ABC3+FUNA(J+1)*ABC4	C5740
RATIOB=FUNB(J)*ABC3+FUNB(J+1)*ABC4	C5741
RBP=.5*PIR*(ABC3*SPRIME(J)/R(J)+ABC4*SPRIME(J+1)/R(J+1))	C5750
Y2P=ABC3*Y2PRM(J)+ABC4*Y2PRM(J+1)	C5760
GO TO 620	C5770
610 RB=R(JW10)-ABC3*DX*RBP	C5780
Y2B=Y2(JW10)-ABC3*DX*Y2P	C5790
RATIO=FUNA(JW10)-ABC3*DX*FUNB(JW10)	C5800
RATIOB=FUNB(JW10)	C5801
620 HB=Y2B+RB**2/Y2B	C5810
HBP=Y2P*(1.-(RB/Y2B)**2)+2.*RB/Y2B*RBP	C5820
GO TO 500	C5830
630 BLAM=BLAMB+(BLAMP1+2.*(BLAMP2+BLAMP3)+BLAMP)*ADX3/6.	C5840
640 BTAU=BTAUB+(BTAUP1+2.*(BTAUP2+BTAUP3)+BTAUP)*ADX3/6.	C5850
JAM=16	C5860

AJAM=JAM	C5870
AJAMR=1./AJAM	C5880
ADX2=DX*AJAMR	C5890
JJ2=JAM	C5900
JJ1=1	C5910
VLAM(JG+1)=BLAM	C5920
VTAU(JG+1)=BTAU	C5930
650 CONTINUE	C5940
JG=JW2-JW10+3	C5950
IF (JCHCK.LT.JW2) GO TO 660	C5960
DLTPH=2.*DX*SNALP*(2.*(Y2(JW2)+R(JW2)**2/Y2(JW2))*(VLAM(JG)*VLAMP(	C5970
1JG)+VTAU(JG)*VTAUP(JG))+((1.-(R(JW2)/Y2(JW2))**2)*Y2PRM(JW2)+P[R*S	C5980
2PRIME(JW2)/Y2(JW2))*VLAM(JG)**2+VTAU(JG)**2))/(1.-VTAU(JG)**2)*FU	C5990
3NA(JW2)+2.*DX*SNALP*(Y2(JW2)+R(JW2)**2/Y2(JW2))*(VLAM(JG)**2+VTAU(	C5991
4JG)**2))/(1.-VTAU(JG)**2)*FUNB(JW2)	C5992
GO TO 670	C6000
660 JG1=JCHCK-JW10+3	C6010
GAN=.5*Y2(JCHCK)*(VLAM(JG1)+VTAU(JG1)**2/VLAM(JG1))	C6020
GAN=GAN*(1.+(R(JCHCK)/Y2(JCHCK))**2)*FUNA(JCHCK)	C6030
DLTPH=2.*SNALP*GAN*DX*((1.-VTAU(JG))/(1.-VTAU(JG))**2+VLAM(JG)**	C6040
12)+1./((1.+VTAU(JG))*VLAMP(JG)+VLAM(JG)*(1./((1.-VTAU(JG))**2+VLAM	C6050
2(JG)**2)-1./((1.+VTAU(JG))**2)*VTAUP(JG))	C6060
670 DO 700 J=JW10,JW3	C6070
JG=J-JW10+3	C6080
IF (J.LE.JCHCK) GO TO 680	C6090
DGANDX=0.	C6100
GO TO 690	C6110
680 GAN=.5*(Y2(J)+R(J)**2/Y2(J))*(VLAM(JG)+VTAU(JG)**2/VLAM(JG))	C6120
DGANDX=.5*Y2PRM(J)*((1.-(R(J)/Y2(J))**2)*(VLAM(JG)+VTAU(JG)**2/VLAM	C6130
1(JG))+.5*(Y2(J)+R(J)**2/Y2(J))*VLAMP(JG)*(1.-(VTAU(JG)/VLAM(JG))**	C6140
22)+(Y2(J)+R(J)**2/Y2(J))*VTAU(JG)/VLAM(JG)*VTAUP(JG)	C6150
DGANDX=DGANDX*FUNA(J)+GAN*FUNB(J)	C6160
GAN=GAN*FUNA(J)	C6170
690 CP(J)=GAN*VLAM(JG)*(Y2(J)+R(J)**2/Y2(J))*2.	C6180
700 CPO(J)=((DGANDX*VLAM(JG)+GAN*VLAMP(JG))*(Y2(J)+R(J)**2/Y2(J))+GAN*	C6190
1VLAM(JG)*Y2PRM(J)*((1.-(R(J)/Y2(J))**2))*2.	C6200
DO 710 J=JW10,JW3	C6210
IF (J.EQ.JW10) DLFDOP=DXR*(CPO(JW10+1)-CPO(JW10))	C6220
IF (J.EQ.JW3) DLFDOP=DXR*(CPO(JW3)-CPO(JW3-1))	C6230
IF (J.GT.JW10.AND.J.LT.JW3) DLFDOP=.5*DXR*(CPO(J+1)-CPO(J-1))	C6240
FUN(J)=FUN(J)+.5*GAMP1*(2.*CPO(J)*FUNO(J)+DLFDOP*(FUN2(J)+CPO(J)))	C6250
FUNO(J)=FUNO(J)+.5*DLFDOP	C6260
FUN2(J)=FUN2(J)+CPO(J)	C6270

710	FUN3(J)=FUN3(J)+CP(J)	C6280
		C6290
C		C6300
C	PART 5 MORE WING GEOMETRY	C6310
C		C6320
720	DO 750 J=1,J5	C6330
	FUN(J)=SIGMA*FUN(J)	C6334
	FUN1(J)=2.*SNALP*SNO*FUNO(J)	C6360
	FUNO(J)=SIGMA*FUNO(J)	C6370
	FUN4(J)=FUN4(J)-FUNO(J)	C6380
	IF (IVOR.EQ.0.OR.J.LT.JW10.OR.J.GT.JW3) GO TO 740	C6390
	JG=J-JW10+3	C6400
	IF (J.GT.JCHCK) GO TO 730	C6410
	HB=Y2(J)+R(J)**2/Y2(J)	C6420
	HBP=(1.-(R(J)/Y2(J))**2)*Y2PRM(J)+PIR*SPRIME(J)/R(J)	C6430
	FUN4(J)=FUN4(J)+SNALP*(HBP*(VLAM(JG)**2+VTAU(JG)**2)+2.*HB*(VLAM(J	C6440
	1G)*VLAMP(JG)+VTAU(JG)*VTAUP(JG)))/(1.-VTAU(JG))*FUNA(J)+SNALP*HB*(	C6450
	2VLAM(JG)**2+VTAU(JG)**2)/(1.-VTAU(JG))*FUNB(J)	C6460
	FUNO(J)=FUNO(J)-SNALP*(HBP*(VLAM(JG)**2+VTAU(JG)**2)+2.*HB*(VLAM(J	C6470
	1G)*VLAMP(JG)+VTAU(JG)*VTAUP(JG)))/(1.-VTAU(JG)**2)*VTAU(JG)*FUNA(J	C6480
	2)-SNALP*HB*(VLAM(JG)**2+VTAU(JG)**2)/(1.-VTAU(JG)**2)*VTAU(JG)*FUN	C6490
	3B(J)	C6500
	GO TO 740	C6510
730	ADD1=GAN*((1.-VTAU(JG))*VLAMP(JG)+VLAM(JG)*VTAUP(JG))/((1.-VTAU(JG	C6520
	1)**2+VLAM(JG)**2)	C6530
	FUN4(J)=FUN4(J)+SNALP*ADD1	C6540
	ADD2=1./(1.+VTAU(JG))	C6550
	FUNO(J)=FUNO(J)-SNALP*(ADD1+GAN*ADD2*(VLAMP(JG)-VLAM(JG)*ADD2*VTAU	C6560
	1P(JG))	C6570
740	FUNY(J)=.25*CS20*FUN(J)	C6580
	FUN8(J)=FUN2(J)*FUN3(J)*2.*AMINF**2	C6590
	FUN9(J)=0.	C6600
	FUN10(J)=0.	C6610
	IF (Y2(J).LT.1.E-06) GO TO 750	C6620
	FUN9(J)=FUN2(J)/Y2(J)**4*2.*AMINF**2	C6630
	FUN10(J)=FUN9(J)*Y2(J)*PIR	C6640
	FUN9(J)=-FUN9(J)	C6650
750	FUNX(J)=FUNY(J)-.5*SIGMA*FUN2(J)	C6660
	CNNC=.125*SIGMA*CS20*DXR	C6670
	JW10P1=JW10+1	C6680
	JW3M1=JW3-1	C6690
	FUN6(JW10)=2.*CNNC*(FUN(JW10P1)-FUN(JW10))-FUNO(JW10)	C6700
	DO 760 J=JW10P1,JW3M1	C6710
760	FUN6(J)=CNNC*(FUN(J+1)-FUN(J-1))-FUNO(J)	

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FUN6(JW3)=2.*CNNC*(FUN(JW3)-FUN(JW3M1))-FUN0(JW3)
FUN7(JW10)=DXR*(FUN6(JW10P1)-FUN6(JW10))
DO 770 J=JW10P1,JW3M1
770 FUN7(J)=.5*DXR*(FUN6(J+1)-FUN6(J-1))
FUN7(JW3)=DXR*(FUN6(JW3)-FUN6(JW3M1))

```

C6720  
C6730  
C6750  
C6760  
C6770  
C6790

PART 6 FAR-FIELD MACH LINES

C6800  
C6810  
C6820  
C6830  
C6840  
C6850  
C6860  
C6870  
C6880

```

IF (AMINF.LE.1.) GO TO 850
XWM=XW(M)
XWMSQR=1./XWM**2
BETA=SQRT(-BETASQ)
J2P1=J2+1
DO 810 J=J2P1,J5
KUPA(J)=1
DO 780 K=1,KF
Z=XW(J)-BETA*RW(K)
IF (Z.LT.XW(J2)) GO TO 790
780 KUPA(J)=K
790 KUPA(J)=KUPA(J)-1
IF (J.LT.M) GO TO 810
KLOA(J)=1
DO 800 K=1,KF
Z=XW(J)-BETA*RW(K)
IF (Z.LT.XW(M)) GO TO 810
800 KLOA(J)=K
810 CONTINUE
DO 820 J=J2P1,J5
IGUNP1=IGUN(J)+1
JW1X=J
IF (IGUNP1.LE.KUPA(J)) GO TO 830
820 CONTINUE
830 DO 840 J=M,J5
IGUNP1=IGUN(J)+1
JW3X=J
IF (IGUNP1.LE.KLOA(J)) GO TO 850
840 CONTINUE

```

C6890  
C6900  
C6910  
C6920  
C6930  
C6940  
C6950  
C6960  
C6970  
C6980  
C6990  
C7000  
C7010  
C7020  
C7030  
C7040  
C7050  
C7060  
C7070  
C7080  
C7090  
C7100

PART 7 INITIALIZATION OF VELOCITY POTENTIAL

```

850 DO 1000 J=1,J5
IGUNJ=IGUN(J)
IGUNP1=IGUNJ+1

```

C7110  
C7120  
C7130  
C7140  
C7150  
C7160

DO 860 K=1, IGUNJ	C7170
860 PHI(J,K)=0.	C7180
IF (KF.NE.KM) PHI(J,KM)=0.	C7190
IF (AMINF.GT.1.) GO TO 900	C7200
DO 890 K=IGUNP1,KF	C7210
IF (J.LT.JXN) GO TO 870	C7220
IF (J.GT.J3) GO TO 870	C7230
AX=1.	C7240
GO TO 880	C7250
870 AX=ABS(XW(J))	C7260
880 XOCR=AX/SQRT(AX**2+BETASQ*RW(K)**2)	C7270
890 PHI(J,K)=RWR(K)*(XOCR*FUN3(J)+.5*(1.-XOCR)*FUN3(JW3))+XOCR**2*FUNX	C7280
1(J)	C7290
KUPA(J)=KM	C7300
GO TO 1000	C7310
900 IF (J.GT.JW1X) GO TO 910	C7320
KLO=IGUNP1	C7330
GO TO 980	C7340
910 IF (J.GT.JW3X) GO TO 920	C7350
KUP=KUPA(J)	C7360
KLO=IGUNP1	C7370
GO TO 940	C7380
920 KUP=KLOA(J)	C7390
XWJ=XW(J)	C7400
DO 930 K=IGUNP1,KUP	C7410
BR SQ=(BETA*RW(K))**2	C7420
ANUM1=SQRT(XWJ**2-BR SQ)	C7430
ANUM2=SQRT(ABS((XWJ-XWM)**2-BR SQ))	C7440
930 PHI(J,K)=RWR(K)*FUN3(M)*XWMSQR*(XWJ*ANUM1-(XWJ+XWM)*ANUM2+BR SQ*(AL	C7450
LOG(XWJ-XWM+ANUM2)-ALOG(XWJ+ANUM1)))	C7460
IF (KUP.EQ.KF) GO TO 1000	C7470
KLO=KUP+1	C7480
KUP=KUPA(J)	C7490
940 Z=XW(J)-BETA*RW(KLO)	C7500
JJ=-1	C7510
950 JJ=JJ+1	C7520
JX=J-JJ	C7530
IF (Z.LT.XW(JX)) GO TO 950	C7540
DO 970 K=KLO,KUP	C7550
BR=BETA*RW(K)	C7560
Z=XW(J)-BR	C7570
JJ=-1	C7580
960 JJ=JJ+1	C7590

JX=JX-JJ	C 7600
IF (Z.LT.XW(JX)) GO TO 960	C 7610
ZR=1./Z	C 7620
970 PHI(J,K)=RWR(K)*FUN3(JX)*(XW(J)*ZR**1.5*SQRT(XW(J)+BR)+(BR*ZR)**2*	C 7630
1(ALOG(BR)-ALOG(XW(J)+SQRT(XW(J)**2-BR**2))))+FUNX(J)	C 7640
IF (KUP.EQ.KF) GO TO 1000	C 7650
KLO=KUP+1	C 7660
980 DO 990 K=KLO,KF	C 7670
990 PHI(J,K)=0.	C 7680
1000 CONTINUE	C 7690
C	C 7700
C PART 8 TUNNEL WALL	C 7710
C	C 7720
IF (IWALL.EQ.0.OR.ALPHAD.EQ.0.) GO TO 1090	C 7730
IF (IWALL.EQ.2) GO TO 1070	C 7740
CARRY=0.	C 7750
CARRY1=0.	C 7760
JWXZ=JW10	C 7770
DO 1060 J=1,J5	C 7780
IF (J.LE.JW10) GO TO 1050	C 7790
IF (P.EQ.0.) GO TO 1030	C 7800
IF (AMINF.LE.1.) GO TO 1010	C 7810
IF (KUPA(J).LT.KM) GO TO 1040	C 7820
1010 IF (J.GT.JW3) GO TO 1020	C 7830
EXP1=EXP((XW(JWXZ)-XW(J))/(P*RW(KM)))	C 7840
EXP2=EXP1**2	C 7850
EXP2R=1./EXP2	C 7860
EXP4R=EXP2R**2	C 7870
EXP1M=EXP((XW(JWXZ)-XW(J-1))/(P*RW(KM)))	C 7880
EXP2M=EXP1M**2	C 7890
EXP2MR=1./EXP2M	C 7900
EXP4MR=EXP2MR**2	C 7910
CARRY=CARRY+.5*(EXP2R+EXP2MR)*(FUN3(J)*EXP1-FUN3(J-1)*EXP1M)	C 7920
CARRY1=CARRY1+2.*((EXP2R+EXP2MR)*(FUNY(J)-FUNY(J-1))-.5*(EXP4R+EXP4	C 7930
1MR)*(FUN8(J)*EXP2-FUN8(J-1)*EXP2M)/RW(KM)**2*SIGMA*CS20	C 7940
1020 FUN11(J)=-EXP1/RW(KM)**2*CARRY	C 7950
FUN12(J)=-EXP2/RW(KM)**2*CARRY1	C 7960
GO TO 1060	C 7970
1030 FUN11(J)=FUN3(J)/RW(KM)**2	C 7980
FUN12(J)=FUN8(J)/RW(KM)**4*SIGMA*CS20	C 7990
GO TO 1060	C 8000
1040 JWxz=J	C 8010
1050 FUN11(J)=0.	C 8020

	FUN12(J)=0.	C8030
1060	CONTINUE	C8040
	GO TO 1090	C8050
1070	ANUM0=(1.-P*RW(KM))/((1.+P*RW(KM))*RW(KM)**2)	C8060
	ANUM1=(2.-P*RW(KM))/(RW(KM)**4*(2.+P*RW(KM)))*SIGMA*CS20	C8070
	ANUM2=P/(RW(KM)*(2.-P*RW(KM)))*4.	C8080
	DO 1080 J=1,J5	C8090
	FUN12(J)=ANUM1*FUN8(J)-ANUM2*FUNY(J)	C8100
1080	FUN11(J)=FUN3(J)*ANUM0	C8110
C		C8120
C	PART 9     INITIALIZATION OF VELOCITY POTENTIAL UNDER WING	C8130
C		C8140
1090	IF (IW.EQ.0) GO TO 1110	C8150
	KU=IFUN(JW3)	C8160
	JGU=JW3-JW10+4	C8170
	DO 1100 J=1,JGU	C8180
	DO 1100 K=1,KU	C8190
1100	PHIU(J,K)=0.	C8200
C		C8210
C	PART 10    INDEXING OF WING TRAILING EDGE	C8220
C		C8230
1110	IF (JW2.EQ.JW3) GO TO 1160	C8240
	JGP=JW20-JW10+2	C8250
	DO 1120 J=1,JGP	C8260
1120	IFUM(J)=1	C8270
	JGP=JGP+1	C8280
	JGU=JW3-JW10+3	C8290
	DO 1150 JJ=JGP,JGU	C8300
	J=JW10+JJ-3	C8310
	K=0	C8320
1130	K=K+1	C8330
	IF (RW(K).GT.Y1(J)) GO TO 1140	C8340
	GO TO 1130	C8350
1140	IFUM(JJ)=K	C8360
	IF (K.EQ.IFUN(JW3).AND.JJ.LT.JGU) IFUM(JJ)=K-1	C8370
1150	CONTINUE	C8380
	IF (IFUM(JGU).GT.IFUN(J)) IFUM(JGU)=IFUM(J)	C8390
	GO TO 1180	C8400
1160	JGU=JW3-JW10+3	C8410
	DO 1170 J=1,JGU	C8420
1170	IFUM(J)=1	C8430
1180	IFUM(JW3-JW10+4)=IFUM(JW3)+1	C8440
C		C8450

C	PART 11	PRINTING	C8460
C			C8470
	PRINT 1230,	(K,RW(K),RWR(K),AXOCR(K),ABAR(K),K=1,KF)	C8480
	PRINT 1240,	(K,CON1(K),CON2(K),CON3(K),CON7(K),CON8(K),CON9(K),CON	C8490
	110(K),CON11(K),K=1,KF)		C8500
	PRINT 1250,	(J,XW(J),R(J),SPRIME(J),Y2(J),Y1(J),FUN3(J),FUN2(J),FU	C8510
	1NO(J),J=1,J5)		C8520
	PRINT 1260,	(J,XW(J),FUN(J),FUN4(J),FUN1(J),FUN5(J),FUN6(J),FUN7(J	C8530
	1),FUNX(J),J=1,J5)		C8540
	PRINT 1270,	(J,XW(J),FUNY(J),FUNA(J),FUNB(J),IFUN(J),IGUN(J),KUPA(	C8550
	1J),KLOA(J),J=1,JW10M1)		C8560
	DO 1190 J=JW10,JW3P1		C8570
	JG=J-JW10+3		C8580
1190	PRINT 1290,	J,XW(J),FUNY(J),FUNA(J),FUNB(J),IFUN(J),IGUN(J),KUPA(J	C8590
	1),KLOA(J),IFUM(JG)		C8600
	JW3P2=JW3+2		C8610
	PRINT 1280,	(J,XW(J),FUNY(J),FUNA(J),FUNB(J),IFUN(J),IGUN(J),KUPA(	C8620
	1J),KLOA(J),J=JW3P2,J5)		C8630
	IF (JW10.EQ.JW3P1) JW10=J3+1		C8640
	PRINT 1300		C8650
	PRINT 1310,	(J,XW(J),FUN8(J),FUN9(J),FUN10(J),FUN11(J),FUN12(J),Y2	C8660
	1PRM(J),J=1,J5)		C8670
	IF (IVOR.EQ.0) GO TO 1220		C8680
	PRINT 1320		C8690
	DO 1210 J=JW10,JW3		C8700
	JG=J-JW10+3		C8710
	IF (J.GT.JCHCK) GO TO 1200		C8720
	HB=Y2(J)+R(J)**2/Y2(J)		C8730
	HBP=(1.-(R(J)/Y2(J))**2)*Y2PRM(J)+PIR*SPRIME(J)/Y2(J)		C8740
	GAN=.5*HB*(VLAM(JG)+VTAU(JG)**2/VLAM(JG))		C8750
	DGANDX=.5*(HBP*(VLAM(JG)+VTAU(JG)**2/VLAM(JG))+HB*(1.-(VTAU(JG)/VL	C8760	
	1AM(JG))**2)*VLAMP(JG))+HB*VTAU(JG)/VLAM(JG)*VTAUP(JG)		C8770
	DGANDX=DGANDX*FUNA(J)+GAN*FUNB(J)		C8780
	GAN=GAN*FUNA(J)		C8790
	GO TO 1210		C8800
1200	DGANDX=0.		C8810
1210	PRINT 1330,	J,XW(J),VLAM(JG),VTAU(JG),VLAMP(JG),VTAUP(JG),GAN,DGAN	C8820
	1DX,YV(JG),ZV(JG),R(J),Y2(J)		C8830
1220	IF (IWING.GE.0) GO TO 1222		C8831
	PRINT 1333		C8832
	DO 1221 J=JW10,JW3		C8833
	JG=J-JW10+3		C8834
1221	PRINT 1334,	J,XW(J),FUNA(JG),FUNB(JG),UUOD(JG),UU90D(JG)	C8835



IF (AMINF.GT.1.) GO TO 1222	C8840
PRINT 1331	C8841
PRINT 1332, (NA,COEF(NA),NA=1,NAMXP1)	C8842
1222 PRINT 1340, SIGMA,DELTA,BETASQ,DXR,DXSQR,GAMP1,GP1DXR,KMM1,KFMI,KF	C8843
1,DELETA,PIR,CON4,CON5,H,JT,JI	C8850
PRINT 1350, JF,DX,JXN,SNO,CS20,SNALP,IJW,JW10,JW20,JW1X,JW3X,BETA,	C8860
1JW3M1,DLTPH,JCHCK,IW,JW10M2	C8870
PRINT 1360, JW3P1,JW10M1,M,XWM,XWMSQR	C8880
RETURN	C8890
C	C8900
1230 FORMAT (17H SUBROUTINE START////44H   ARRAYS AND PARAMETERS USED I	C8910
1N COMPUTATION/48H       J = AXIAL GRID INDEX, K = RADIAL GRID INDEX/	C8920
2//3X,1HK,5X,5HRW(K),12X,6HRWR(K),9X,8HAXOCR(K),9X,7HABAR(K)//(14,4	C8930
3E16.8))	C8940
1240 FORMAT (/3X,1HK,5X,7HCON1(K),10X,7HCON2(K),9X,7HCON3(K),10X,7HCON	C8950
17(K),8X,7HCON8(K),9X,7HCON9(K),9X,8HCON10(K),9X,8HCON11(K)//(14,8E	C8960
216.8))	C8970
1250 FORMAT (/3X,1HJ,5X,5HXW(J),12X,4HR(J),9X,9HSPRIME(J),8X,5HY2(J),1	C8980
10X,5HY1(J),11X,7HFUN3(J),9X,7HFUN2(J),9X,7HFUN0(J)//(14,8E16.8))	C8990
1260 FORMAT (/3X,1HJ,5X,5HXW(J),12X,6HFUN(J),9X,7HFUN4(J),10X,7HFUN1(J	C9000
1),11X,7HFUN5(J),9X,7HFUN6(J),9X,7HFUN7(J),9X,7HFUNX(J)//(14,8E16.8	C9010
2))	C9020
1270 FORMAT (/3X,1HJ,5X,5HXW(J),11X,7HFUNY(J),9X,7HFUNA(J),10X,7HFUN8(	C9030
1J),9X,7HFUN(J),2X,7HIGUN(J),2X,7HKUPA(J),2X,7HKLOA(J),2X,8HFUN(J	C9040
2G)//(14,4E16.8,4I9))	C9050
1280 FORMAT (14,4E16.8,4I9)	C9060
1290 FORMAT (14,4E16.8,5I9)	C9070
1300 FORMAT (/3X,1HJ,5X,5HXW(J),11X,7HFUN8(J),9X,7HFUN9(J),9X,8HFUN10(	C9080
1J),10X,8HFUN11(J),8X,8HFUN12(J),9X,8HY2PRM(J)/)	C9090
1310 FORMAT (14,7E16.8)	C9100
1320 FORMAT (/3X,1HJ,4X,5HXW(J),5X,8HVLAM(JG),3X,8HVTAU(JG),2X,9HVLAMP	C9110
1(JG),2X,9HVTAUP(JG),5X,3HGAN,6X,6HDGANDX,5X,6HYV(JG),5X,6HZV(JG),6	C9120
2X,4HR(J),6X,5HY2(J)/)	C9130
1330 FORMAT (14,11E11.3)	C9140
1331 FORMAT(/3X,2HNA,4X,8HCOEF(NA)/)	C9141
1332 FORMAT (14,E16.8)	C9142
1333 FORMAT (/3X,1HJ,5X,5HXW(J),9X,9HFUNAO(JG),7X,9HFUNBO(JG),9X,8HUUO	C9143
1D(JG),7X,9HUU90D(JG)/)	C9144
1334 FORMAT (14,5E16.8)	C9145
1340 FORMAT (/8H SIGMA =,E16.8//8H DELTA =,E16.8//9H BETASQ =,E16.8//7	C9150
1H DXR =,E16.8//8H DXSQR =,E16.8//8H GAMP1 =,E16.8//9H GP1DXR =,E1	C9160
26.8//7H KMM1 =,15//7H KFMI =,15//5H KF =,15//9H DELETA =,E16.8//6H	C9170
3 PIR =,E16.8//8H CON4 =,E16.8//7H CON5 =,E16.8//4H H =,E16.8//5H	C9180

4JT =,I5//5H JI =,I5)	C9190
1350 FORMAT (/9H JF =,I5//9H DX =,E16.8//9H JXN =,I5//9H SNO	C9200
.1 =,E16.8//9H CS20 =,E16.8//9H SNALP =,E16.8//9H IJW =,I5/	C9210
2/9H JW10 =,I5//9H JW20 =,I5//9H JW1X =,I5//9H JW3X =,I5//9	C9220
3H BETA =,E16.8//9H JW3M1 =,I5//9H OLTPH =,E16.8//9H JCHCK =,I	C9230
45//9H IW =,I5//9H JW10M2 =,I5)	C9240
1360 FORMAT (/9H JW3P1 =,I5//9H JW10M1 =,I5//9H M =,I5//9H XMM	C9250
1 =,E16.8//9H XWMSQR =,E16.8)	C9260
END	C9270-

# SUBROUTINE MACH

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COMMON SIGMA, DELTA, I, BETASQ, DXR, DXSQR, GAMP1, GP1DXR, KMM1, KFMI, KF, DE
1 LETA, PIR, CON4, CON5, H, JT, JI, JF, DPHIMX, DX, JXN, SNO, CS20, SNALP, IJW, JW1
20, JW20, JW1X, JW3X, BETA, JW3M1, DLTPH, JCHCK, IW, JW10M2, JW3P1, JW10M1, M, X
3 WM, XWMSQR, PI, AK2, AX2, AK1, AX1, AX10, CNX, NAMXP1, A1, A2, ZMACH, JMCK
COMMON R(120), SPRIME(120), FUN(120), XW(120), Y1(120), Y2(120), FUN1(12
10), FUNO(120), IFUN(120), FUN2(120), FUN3(120), FUN4(120), IGUN(120), CP(
2120), FUNX(120), SLAS(120,6), CPO(120), KLOA(120), KUPA(120), FUN5(120),
3 FUN6(120), FUN7(120), FUNY(120), CP1(120), CP2(120)
COMMON FUN8(120), FUN9(120), FUN10(120), FUN11(120), Y2PRM(120), FUN12(
1120), FUNA(120), FUNB(120)
COMMON CON7(100), CON8(100), CON9(100), CON10(100), CON11(100), CON1(10
10), CON2(100), CON3(100), OMEGA(100), ABAR(100), BBAR(100), CBAR(100), DB
2 AR(100), PHIO(100), RW(100), RWR(100), AXOCR(100), ACHK(100), PHIOLD(100
3), BCHK(100)
COMMON PHIUD(25), OMEGAU(25), ACHKU(25), BBARU(25), CBARU(25), DBARU(25
1), BCHKU(25), PHIUD(25)
COMMON IFUM(50), VLAM(50), VTAU(50), VLAMP(50), VTAUP(50), YV(50), ZV(50
1), FUNAO(50), FUNBO(50), UUOD(50), UU9OD(50)
COMMON PHI(109,50), PHIU(50,25), COEF(21)
COMMON /NMLIST/ J1, J2, J3, J4, J5, FAC, KM, RCOM, A, B, I, WALL, P, OMEGAD, ALPH
1 AD, HSPAN, AMINF, GAMMA, IR, RC, RMAX, RN, JS, RS, JW1, JW2, JW3, JWD, I, WING, B1,
2 B2, DEL1, DEL, IVOR, IDIR, EPSI, SUB, SUP, IMAX, SFACOR
DIMENSION ATHETA(19), ATAU(19), AXW(19), AY2B(19)
DIMENSION ARA(19,19), ARB(21), BRA(19,1), IPIVOT(19)
JXOC=JW10
ZMACH=BETASQ
MM=JW3
IF (AMINF.GE.1.) GO TO 210

```

## PART 1 LAWRENCE AND FLAX APPROXIMATION FOR SUBSONIC FREE-STREAM MACH NUMBERS

```

XOC=XW(JXOC)
YPCHK=Y2PRM(JW10)-DXR*(R(JW10)-R(JW10-1))
IF (ABS(YPCHK).GT.1.E-06) XOC=XOC-(Y2(JW10)-R(JW10))/YPCHK
XIC=XW(JW3)
X1MXO=XIC-XOC
X1MXOR=1./X1MXO
GPI=0.
NAMAX=20

```

M 0  
M 10  
M 20  
M 30  
M 40  
M 50  
M 60  
M 70  
M 80  
M 90  
M 100  
M 110  
M 120  
M 130  
M 140  
M 150  
M 160  
M 170  
M 180  
M 190  
M 200  
M 210  
M 220  
M 230  
M 231  
M 232  
M 240  
M 250  
M 260  
M 270  
M 280  
M 290  
M 300  
M 310  
M 320  
M 321  
M 322  
M 330  
M 350  
M 360  
M 370  
M 380

MAMAX=19	M 390
ANAMX=NAMAX	M 400
AMAMX=MAMAX	M 410
ANAMXR=1./ANAMX	M 420
AMAMXR=1./AMAMX	M 430
NAMXM1=NAMAX-1 \$ MAMXM1=MAMAX-1 \$ NAMXP1=NAMAX+1	M 440
ATHAMX=ACOS(X1MXOR*(2.*XW(JXOC)-XOC-X1C))	M 441
ATHAMX=ATHAMX*ANAMX/(ANAMX-1.)	M 442
DO 10 NA=1,NAMXM1	M 450
ANA=NA	M 460
ATHETA(NA)=ATHAMX*ANA*ANAMXR	M 470
10 AXW(NA)= .5*(X1C+XOC+X1MXO*COS(ATHETA(NA)))	M 480
DO 20 MA=1,MAMXM1	M 490
AMA=MA	M 500
20 ATAU(MA)=PI*AMA*AMAMXR	M 510
DO 70 NA=1,NAMXM1	M 520
AX=AXW(NA)-XW(JW1)	M 530
BX=AK2*(AX-AX2)	M 540
IF (BX.LT.-100.) BX=-100.	M 550
IF (BX.GT.100.) BX=100.	M 560
IF (ABS(BX).LT.1.E-06) GO TO 30	M 570
CX=EXP(-BX)	M 580
XD=1./(1.-CX)	M 590
AY2B(NA)=-B2*(AX-AX2)*XD	M 600
GO TO 40	M 610
30 AY2B(NA)=-B2/BX	M 620
40 IF (IWING.EQ.-2) GO TO 50	M 630
AY2B(NA)=A2+B2*AX+AY2B(NA)	M 640
GO TO 70	M 650
50 BX=AK1*(AX-AX1)	M 660
IF (BX.LT.-100.) BX=-100. \$ IF (BX.GT.100.) BX=100.	M 680
IF (ABS(BX).LT.1.E-06) GO TO 60	M 690
CX=EXP(-BX) \$ XD=1./(1.-CX)	M 700
AY2B(NA)=AY2B(NA)+(B2-B1)*(AX-AX1)*XD+A1+B1*AX	M 710
GO TO 70	M 720
60 AY2B(NA)=AY2B(NA)+A1+B1*AX+(B2-B1)/BX	M 730
70 CONTINUE	M 740
J=JW3	M 750
DO 100 NA=1,NAMXM1	M 760
80 IF (XW(J).LT.AXW(NA)) GO TO 90	M 770
J=J-1	M 780
GO TO 80	M 790
90 AR=R(J)+(R(J+1)-R(J))*DXR*(AXW(NA)-XW(J))	M 800

100	AY2B(NA)=AY2B(NA)-AR**2/AY2B(NA)	M 810
	BETA=SQRT(BETASQ)	M 830
	DO 110 NA=1,NAMXM1	M 840
	CST=COS(ATHETA(NA))	M 850
	BABR=2.*BETA*AY2B(NA)*X1MXOR	M 860
	BRA(NA,1)=(SQRT((1.-CST)**2+BABR**2)-BABR)/(1.-CST)	M 870
	ARA(NA,MAMAX)=(BABR-SQRT((1.+CST)**2+BABR**2))/(1.+CST)	M 880
	DO 110 MA=1,MAMXM1	M 890
	CSTU=COS(ATAU(MA))	M 900
	ACK1=CSTU-CST \$ ACK2=.01*BABR	M 910
	IF (BABR.LT.1.E-08) GO TO 102	M 911
	IF (ABS(ACK1).LT.ACK2) GO TO 101	M 912
	ARA(NA,MA)=(SQRT(ACK1**2+BABR**2)-BABR)/ACK1	M 913
	GO TO 110	M 914
101	ARA(NA,MA)=.5*ACK1/BABR*(1.-.25*(ACK1/BABR)**2)	M 915
	GO TO 110	M 916
102	ARA(NA,MA)=1.	M 917
	IF (ACK1.LT.0.) ARA(NA,MA)=-1.	M 918
110	CONTINUE	M 919
	DO 160 NA=1,NAMXM1	M 920
	DO 130 LA=1,NAMXP1	M 930
	ALA=LA	M 940
	SUM=0.	M 950
	DO 120 MA=1,MAMXM1	M 960
120	SUM=SUM+COS(ATAU(MA)*(ALA-1.))*ARA(NA,MA)	M 970
130	ARB(LA)=PI*AMAMXR*(.5*(BRA(NA,1)-(-1.))*LA*ARA(NA,MAMAX))+SUM)	M 980
	ARB(1)=2.*ATHETA(NA)+ARB(1)-3.*PI	M 990
	DO 140 LA=2,NAMXP1	M1000
	ALA=LA	M1010
	ALAM1=ALA-1.	M1020
140	ARB(LA)=2.*SIN(ALAM1*ATHETA(NA))*(1./ALAM1+PI*BETA*AY2B(NA)*X1MXOR	M1030
	1/SIN(ATHETA(NA)))+ARB(LA)	M1040
	DO 150 LA=1,NAMXM1	M1060
150	ARA(NA,LA)=ARB(LA+2)-ARB(LA)	M1070
160	BRA(NA,1)=3.*GPI+2.*PI*AY2B(NA)**2	M1080
	NL=NAMXM1	M1090
	NRHS=1	M1100
	IFAC=0	M1110
	CALL SIMEQ (ARA,NL,BRA,NRHS,DETERM,PIPOT,NAMXM1,ISCALE)	M1130
	IF (DETERM.NE.0.) GO TO 170	M1140
	STOP 201	M1150
170	DO 180 NA=1,NAMXM1	M1160
180	COEF(NA)=BRA(NA,1)	



IF (BBBB.GT.1.) RETURN	M1420
CHCK=.5*DXR*HSPAN*BETA	M1430
IF (CHCK.GT.1.) GO TO 220	M1440
JMCK=JW3	M1450
GO TO 270	M1460
220 JMCK=JXOC+1	M1470
JXOCP2=JXOC+2	M1480
DO 230 J=JXOCP2,JW3	M1490
IF (Y2PRM(J).LT.Y2PRM(J+1)) GO TO 230	M1500
CHCK=Y2PRM(J)/B2	M1510
IF (CHCK.LT..999) GO TO 240	M1520
230 JMCK=J	M1530
240 AX20=XW(JW1)+AX2	M1540
DO 250 J=JXOC,JW3	M1550
IF (XW(J).GT.AX20) GO TO 260	M1560
250 MM=J	M1570
260 JMP1=MM+1	M1580
HSPNB=HSPAN-R(JMP1)**2/HSPAN	M1590
270 NAMAX=20	M1591
ANAMX=NAMAX	M1592
ANAMXR=1./ANAMX	M1593
PHIO(NAMAX+1)=0.	M1594
NAMXP1=NAMAX+1	M1595
DO 271 NA=1,NAMAX	M1596
ANA=NA	M1597
271 PHIO(NA)=SQRT(1.-((ANA-1.)*ANAMXR)**2)	M1598
SUM=0.	M1599
DO 272 NA=1,NAMAX	M1600
272 SUM=SUM+2.*PIR*ANAMXR*(PHIO(NA)+PHIO(NA+1))	M1601
DO 280 J=JW10,JMCK	M1602
ARGO=BETA*Y2PRM(J)	M1603
IF (ARGO.LT.1.) ARG=1.-SQRT(1.-ARGO**2)	M1604
IF (ARGO.GE.1.) ARG=1.	M1610
ANUM3=0. \$ IF (ARG.GT.1.E-06) ANUM3=ARG*ALOG(ARG)	M1620
EC=1.+ .4630151*ARG+.1077812*ARG**2- (.2452727+.0412496*ARG)*ANUM3	M1630
FUNA(J)=1./EC	M1631
JG=J-JW10+3	M1632
FUNAO(JG)=SUM/EC	M1633
FUNBO(JG)=DXR*(FUNAO(JG)-FUNAO(JG-1))	M1634
FUNA(J)=1./EC	M1640
280 FUNB(J)=DXR*(FUNA(J)-FUNA(J-1))	M1650
FUNB(JW10)=FUNB(JW10+1)	M166
FUNBO(3)=FUNBO(4)	M166

IF (JMCK.EQ.JW3) GO TO 390	M1670
JMCKP1=JMCK+1	M1690
HSPNBP=Y2PRM(JMCKP1)*(1.+(R(JMCKP1)/Y2(JMCKP1))**2)-PIR*SPRIME(JMCKP1)/Y2(JMCKP1)	M1700
XWOO=XW(JMCKP1)-(Y2(JMCKP1)-R(JMCKP1)**2/Y2(JMCKP1))/HSPNBP	M1701
ANUM1=1./(1.+BETA*HSPNBP)	M1710
XUO=XWOO+(XW(JMCKP1)-XWOO)*ANUM1	M1720
DO 290 J=JXOC,JMP1	M1730
IF (XUO.LT.XW(J)) GO TO 300	M1740
290 JXUO=J	M1750
300 DO 380 J=JMCKP1,JW3	M1760
Y2B=Y2(J)-R(J)**2/Y2(J)	M1770
DYB=Y2B*ANAMXR	M1810
YB=-DYB	M1820
XU1=XWOO+(XW(J)-XWOO)*ANUM1	M1830
IF (J.LE. MM) GO TO 310	M1840
YU1=(XU1-XWOO)*HSPNBP	M1850
IF (YU1.LE.HSPNB) GO TO 310	M1860
XU1=XW(J)-BETA*HSPNB	M1870
310 IF (XU1.GE.XW(JXUO+1)) JXUO=JXUO+1	M1880
IF (XU1.GE.XW(JXUO+1)) GO TO 310	M1890
JXU1=JXUO	M1891
JXU2=JXU1	M1900
XU2=XU1	M1910
DO 360 NA=1,NAMXP1	M1920
YB=YB+DYB	M1930
IF (NA.EQ.1) GO TO 320	M1940
XU1=XU1+BETA*DYB*ANUM1	M1941
IF (J.LE. MM) GO TO 320	M1950
YU1=(XU1-XWOO)*HSPNB	M1960
IF (YU1.LE.HSPNB) GO TO 320	M1970
XU1=XU1+BETA*DYB*(1.-ANUM1)	M1980
320 IF (XU1.GE.XW(JXU1+1)) JXU1=JXU1+1	M1990
IF (XU1.GE.XW(JXU1+1)) GO TO 320	M2000
IF (JXU1.LT.JW10) GO TO 321	M2001
ABC2=(XU1-XW(JXU1))*DXR	M2002
ABC1=1.-ABC2	M2010
YUP=(1.+(R(JXU1)/Y2(JXU1))**2)*Y2PRM(JXU1)-PIR*SPRIME(JXU1)/Y2(JXU1)	M2011
11)	M2012
YUP1=(1.+(R(JXU1+1)/Y2(JXU1+1))**2)*Y2PRM(JXU1+1)-PIR*SPRIME(JXU1+1)/Y2(JXU1+1)	M2013
ALAM10=ABC1*YUP+ABC2*YUP1	M2014
ALAM1=ABC1*Y2PRM(JXU1)+ABC2*Y2PRM(JXU1+1)	M2015
	M2016
	M2017



	YUB=Y2(JXU1)-R(JXU1)**2/Y2(JXU1)	M2020
	YUB1=Y2(JXU1+1)-R(JXU1+1)**2/Y2(JXU1+1)	M2021
	YUC1=ABC1*YUB+ABC2*YUB1	M2022
321	IF (JXU1.LT.JMCKP1) YUC1=(XU1-XW00)*HSPNBP	M2023
	IF (JXU1.LT.JMCKP1) ALAM10=HSPNBP	M2024
	IF (JXU1.LT.JMCKP1) ALAM1=Y2PRM(JMCKP1)	M2025
	AB1=YUC1+(XW(J)-XU1)*ALAM10	M2026
	IF (NA.EQ.1) GO TO 330	M2027
	XU2=XU2-BETA*DYB*ANUM1	M2030
	IF (J.LE. MM) GO TO 330	M2040
	YU2=(XU2-XW00)*HSPNBP	M2050
	IF (YU2.LE.HSPNBP) GO TO 330	M2060
	XU2=XU2-BETA*DYB*(1.-ANUM1)	M2070
330	IF (XU2.LT.XW(JXU2)) JXU2=JXU2-1	M2080
	IF (XU2.LT.XW(JXU2)) GO TO 330	M2081
	IF (JXU2.LT.JW10) GO TO 331	M2082
	ABC2=(XU2-XW(JXU2))*DXR	M2090
	ABC1=1.-ABC2	M2091
	YUP=(1.+(R(JXU2)/Y2(JXU2))**2)*Y2PRM(JXU2)-PIR*SPRIME(JXU2)/Y2(JXU	M2092
	12)	M2093
	YUP1=(1.+(R(JXU2+1)/Y2(JXU2+1))**2)*Y2PRM(JXU2+1)-PIR*SPRIME(JXU2+	M2094
	11)/Y2(JXU2+1)	M2095
	ALAM20=ABC1*YUP+ABC2*YUP1	M2096
	ALAM2=ABC1*Y2PRM(JXU2)+ABC2*Y2PRM(JXU2+1)	M2097
	YUB=Y2(JXU2)-R(JXU2)**2/Y2(JXU2)	M2100
	YUB1=Y2(JXU2+1)-R(JXU2+1)**2/Y2(JXU2+1)	M2101
	YUC2=ABC1*YUB+ABC2*YUB1	M2102
331	IF (JXU2.LT.JMCKP1) YUC2=(XU2-XW00)*HSPNBP	M2103
	IF (JXU2.LT.JMCKP1) ALAM20=HSPNBP	M2104
	IF (JXU2.LT.JMCKP1) ALAM2=Y2PRM(JMCKP1)	M2105
	AB2=YUC2+(XW(J)-XU2)*ALAM20	M2106
	IF (ALAM2.GT.1.E-06) GO TO 340	M2110
	CB1=AB1 \$ CB2=AB2	M2120
	GO TO 350	M2130
340	DELB=.5*(YUC1-ALAM10*XU1-YUC2+ALAM20*XU2+(ALAM10-ALAM20)*XW(J))	M2140
	CB1=AB1-DELB \$ CB2=AB2+DELB	M2150
350	ANUM2=SQRT(2.*CB1/(CB1+CB2))	M2160
	ARGO=.5*BETA*(ALAM1+ALAM2)	M2161
	IF (ARGO.LT.1.) ARG=1.-SQRT(1.-ARGO**2)	M2162
	IF (ARGO.GE.1.) ARG=1.	M2163
	ANUM3=0. \$ IF (ARG.GT.1.E-06) ANUM3=ARG*ALOG(ARG)	M2170
	EC=1.+4630151*ARG+.1077812*ARG**2-(.2452727+.0412496*ARG)*ANUM3	M2180
	IF (NA.EQ.NAMXP1) GO TO 361	M2181

IF (NA.EQ.1) SAVC=ANUM2/EC*SQRT(AB1*AB2+4.*R(J)**2)	M2182
IF (NA.EQ.1.AND.J.EQ.JMCKP1) SAVA=(XW(JMCK)-XW00)*HSPNBP/EC	M2183
IF (NA.EQ.1.AND.J.EQ.JMCKP1) SAVB=SQRT(SAVA**2+4.*(R(JMCK)/EC)**2)	M2184
360 PHIO(NA)=ANUM2/EC*SQRT((AB1-YB)*(AB2+YB))	M2190
361 FUNA(J)=SQRT((AB1+AB2)/AB1*CB1/(CB1+CB2))/EC	M2191
SUM=0.	M2200
DO 370 NA=1,NAMAX	M2210
370 SUM=SUM+DYB*(PHIO(NA)+PHIO(NA+1))	M2220
JG=J-JW10+3	M2230
FUNAO(JG)=2.*SUM/(PI*Y2B**2)	M2231
FUNBO(JG)=DXR*(FUNAO(JG)-FUNAO(JG-1))	M2232
UUOD(JG)=DXR*(PHIO(1)-SAVA)*SNALP	M2233
UU9OD(JG)=DXR*(SAVC-SAVB)*SNALP	M2234
SAVA=PHIO(1) \$ SAVB=SAVC	M2235
380 FUNB(J)=DXR*(FUNA(J)-FUNA(J-1))	M2240
C	M2250
C PART 3 CORRECTION OF FUNCTIONS	M2260
C	M2270
390 DO 420 J=JW10,JW3	M2280
JG=J-JW10+3	M2281
IF (J.GT.JW10) GO TO 400	M2290
FUNBP=DXR*(FUNBO(4)-FUNBO(3))	M2300
GO TO 410	M2310
400 FUNBP=DXR*(FUNBO(JG)-FUNBO(JG-1))	M2320
410 FUNO(J)=FUNAO(JG)*FUNO(J)+FUNBO(JG)*FUN2(J)+.5*FUNBP*FUN3(J)	M2330
FUN2(J)=FUNAO(JG)*FUN2(J)+FUNBO(JG)*FUN3(J)	M2340
FUN3(J)=FUNAO(JG)*FUN3(J)	M2350
FUN(J)=GAMP1*FUN2(J)*FUNO(J)	M2360
420 FUN4(J)=FUNAO(JG)*FUN4(J)+CNX*FUNBO(JG)*Y2(J)*SNALP	M2370
RETURN	M2380
END	M2390

	SUBROUTINE SIMEQ(A,N,B,M,DETERM,IPIVOT,NMAX,ISCALE)	F4.1	1
	***** DOCUMENT DATE 08-01-68 SUBROUTINE REVISED 08-01-68 *****	F4.1	2
C	SOLUTION OF SIMULTANEOUS LINEAR EQUATIONS	F4.1	3
C		F4.1	4
	DIMENSION IPIVOT(N),A(NMAX,N),B(NMAX,M)	F4.1	5
	EQUIVALENCE (IROW,JROW),(ICOLUMN,JCOLUMN),(AMAX,T,SWAP)	F4.1	6
C		F4.1	7
C	INITIALIZATION	F4.1	8
C		F4.1	9
	5 ISCALE=0	F4.1	10
	6 R1=10.0**100	F4.1	11
	7 R2=1.0/R1	F4.1	12
	10 DETERM=1.0	F4.1	13
	15 DO 20 J=1,N	F4.1	14
	20 IPIVOT(J)=0	F4.1	15
	30 DO 550 I=1,N	F4.1	16
C		F4.1	17
C	SEARCH FOR PIVOT ELEMENT	F4.1	18
C		F4.1	19
	40 AMAX=0.0	F4.1	20
	45 DO 105 J=1,N	F4.1	21
	50 IF (IPIVOT(J)-1) 60,105,60	F4.1	22
	60 DO 100 K=1,N	F4.1	23
	70 IF (IPIVOT(K)-1) 80,100,740	F4.1	24
	80 IF (ABS(AMAX)-ABS(A(J,K))) 85,100,100	F4.1	25
	85 IROW=J	F4.1	26
	90 ICOLUMN=K	F4.1	27
	95 AMAX=A(J,K)	F4.1	28
	100 CONTINUE	F4.1	29
	105 CONTINUE	F4.1	30
	IF (AMAX) 110,106,110	F4.1	31
	106 DETERM=0.0	F4.1	32
	ISCALE=0	F4.1	33
	GO TO 740	F4.1	34
	110 IPIVOT(ICOLUMN)=IPIVOT(ICOLUMN)+1	F4.1	35
C		F4.1	36
C	INTERCHANGE ROWS TO PUT PIVOT ELEMENT ON DIAGONAL	F4.1	37
C		F4.1	38
	130 IF (IROW-ICOLUMN) 140,260,140	F4.1	39
	140 DETERM=-DETERM	F4.1	40
	150 DO 200 L=1,N	F4.1	41
	160 SWAP=A(IROW,L)	F4.1	42

170 A(IROW,L)=A(ICOLUM,L)	F4.1 43
200 A(ICOLUM,L)=SWAP	F4.1 44
205 IF (M) 260,260,210	F4.1 45
210 DO 250 L=1,M	F4.1 46
220 SWAP=B(IROW,L)	F4.1 47
230 B(IROW,L)=B(ICOLUM,L)	F4.1 48
250 B(ICOLUM,L)=SWAP	F4.1 49
260 PIVOT=A(ICOLUM,ICOLUM)	F4.1 50
IF (PIVOT) 1000,106,1000	F4.1 51
C	F4.1 52
C SCALE THE DETERMINANT	F4.1 53
C	F4.1 54
1000 PIVOTI=PIVOT	F4.1 55
1005 IF(ABS(DETERM)-R1)1030,1010,1010	F4.1 56
1010 DETERM=DETERM/R1	F4.1 57
ISCALE=ISCALE+1	F4.1 58
IF(ABS(DETERM)-R1)1060,1020,1020	F4.1 59
1020 DETERM=DETERM/R1	F4.1 60
ISCALE=ISCALE+1	F4.1 61
GO TO 1060	F4.1 62
1030 IF(ABS(DETERM)-R2)1040,1040,1060	F4.1 63
1040 DETERM=DETERM*R1	F4.1 64
ISCALE=ISCALE-1	F4.1 65
IF(ABS(DETERM)-R2)1050,1050,1060	F4.1 66
1050 DETERM=DETERM*R1	F4.1 67
ISCALE=ISCALE-1	F4.1 68
1060 IF(ABS(PIVOTI)-R1)1090,1070,1070	F4.1 69
1070 PIVOTI=PIVOTI/R1	F4.1 70
ISCALE=ISCALE+1	F4.1 71
IF(ABS(PIVOTI)-R1)320,1080,1080	F4.1 72
1080 PIVOTI=PIVOTI/R1	F4.1 73
ISCALE=ISCALE+1	F4.1 74
GO TO 320	F4.1 75
1090 IF(ABS(PIVOTI)-R2)2000,2000,320	F4.1 76
2000 PIVOTI=PIVOTI*R1	F4.1 77
ISCALE=ISCALE-1	F4.1 78
IF(ABS(PIVOTI)-R2)2010,2010,320	F4.1 79
2010 PIVOTI=PIVOTI*R1	F4.1 80
ISCALE=ISCALE-1	F4.1 81
320 DETERM=DETERM*PIVOTI	F4.1 82
C	F4.1 83
C DIVIDE PIVOT ROW BY PIVOT ELEMENT	F4.1 84
C	F4.1 85

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340 DO 351 L=1,N
341 IF (IPIVOT(L)-1) 350,351,740
350 A(ICOLUM,L)=A(ICOLUM,L)/PIVOT
351 CONTINUE
355 IF (M) 380,380,360
360 DO 370 L=1,M
370 B(ICOLUM,L)=B(ICOLUM,L)/PIVOT

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C  
C  
C

REDUCE NON-PIVOT ROWS

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380 DO 550 L1=1,N
390 IF (L1-ICOLUM) 400,550,400
400 T=A(L1,ICOLUM)
430 DO 451 L=1,N
431 IF (IPIVOT(L)-1) 450,451,740
450 A(L1,L)=A(L1,L)-A(ICOLUM,L)*T
451 CONTINUE
455 IF (M) 550,550,460
460 DO 500 L=1,M
500 B(L1,L)=B(L1,L)-B(ICOLUM,L)*T
550 CONTINUE
740 RETURN
END

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F4.1 86
F4.1 87
F4.1 88
F4.1 89
F4.1 90
F4.1 91
F4.1 92
F4.1 93
F4.1 94
F4.1 95
F4.1 96
F4.1 97
F4.1 98
F4.1 99
F4.1 100
F4.1 101
F4.1 102
F4.1 103
F4.1 104
F4.1 105
F4.1 106
F4.1 107
F4.1 108

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OVERLAY (DICK,1,2)	D	0
PROGRAM WORK	D	10
COMMON SIGMA,DELTA,I,BETASC,DXR,DXSQR,GAMP1,GP1DXR,KMM1,KFM1,KF,DE	D	20
1 LETA,PIR,CON4,CON5,H,JT,JI,JF,DPHIMX,DX,JXN,SNO,CS20,SNALP,IJW,JW1	D	30
20,JW2C,JW1X,JW3X,BETA,JW3M1,DLTPH,JCHCK,IW,JW10M2,JW3P1,JW1CM1,M,X	D	40
3WM,XWMSQR,PI,AK2,AX2,AK1,AX1,AX10,CNX,NAMXP1,A1,A2,ZMACH,JMCK	D	50
COMMON R(120),SPRIME(120),FUN(120),XW(120),Y1(120),Y2(120),FUN1(12	D	60
10),FUN0(120),IFUN(120),FUN2(120),FUN3(120),FUN4(120),IGUN(120),CP(	D	70
2120),FUNX(120),SLAS(120,6),CPO(120),KLOA(120),KUPA(120),FUN5(120),	D	80
3FUN6(120),FUN7(120),FUNY(120),CP1(120),CP2(120)	D	90
COMMON FUN8(120),FUN9(120),FUN10(120),FUN11(120),Y2PRM(120),FUN12(	D	100
1120),FUNA(120),FUNB(120)	D	110
COMMON CON7(100),CON8(100),CON9(100),CON10(100),CCN11(100),CON1(10	D	120
10),CON2(100),CON3(100),OMEGA(100),ABAR(100),BBAR(100),CBAR(100),DB	D	130
2AR(100),PHIO(100),RW(100),RWR(100),AXOCR(100),ACHK(100),PHIOLD(100	D	140
3),BCHK(100)	D	150
COMMON PHIUD(25),OMEGAU(25),ACHKU(25),BBARU(25),CEARU(25),DBARU(25	D	160
1),BCHKU(25),PHIOU(25)	D	170
COMMON IFUM(50),VLAM(50),VTAU(50),VLAMP(50),VTAUP(50),YV(50),ZV(50	D	180
1),FUNAO(50),FUNBO(50),UUOD(50),UU90D(50)	D	190
COMMON PHI(109,50),PHIU(50,25),COEF(21)	D	200
COMMON /NMLIST/ J1,J2,J3,J4,J5,FAC,KM,RCOM,A,B,IWALL,P,OMEGAD,ALPH	D	210
1AD,HSPAN,AMINF,GAMMA,IR,RC,RMAX,RN,JS,RS,JW1,JW2,JW3,JWD,IWING,B1,	D	220
2B2,DEL1,DEL,IVOR,IDIR,EPSI,SUB,SUP,IMAX,SFACTOR	D	230
PRINT 810	D	240
PRINT 820	D	250
PRINT 830	D	260
PRINT 840	D	270
SUPP=1.	D	280
10 I=I+1	D	290
JIM1=JI-1	D	300
DO 20 K=1,KF	D	310
PHIOLD(K)=PHI(JIM1,K)	D	320
20 ACHK(K)=BETASQ	D	330
DPHIMX=0.	D	340
DO 780 J=JI,JF	D	350
JP1=J+1	D	360
JM1=J-1	D	370
JM2=J-2	D	380
JM3=J-3	D	390
JG=J-JW10+3	D	400
IF (J.LT.J1) GO TO 290	D	410

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IF (J.GT.J4) GO TO 290
PART 1  PRIMARY B AND D ARRAYS IN INNER REGION
IFUNJ=IFUN(J)
IFNJPI=IFUNJ+1
KGUN=IGUN(J)
KGUNPI=KGUN+1
KLO=1
KUP=KGUN-1
PHIM1=PHI(JM1,1)
PHIM10=PHIOLD(1)
30 DO 120 K=KLO,KUP
  IF (K.LE.IFUNJ) GO TO 40
  U=FUN2(J)*RWR(K)+FUN6(J)
  IWO=0
  IF ((IWO.EQ.1.AND.K.LE.IFUN(JPI)) IWO=1
  GO TO 50
40 U=FUN4(J)
  IWO=0
50 ALAMB=BETASQ-.5*GP1DXR*(PHI(JP1,K)-PHIM10)-GAMP1*U
  IF (IWO.EQ.1) ALAMB=ALAMB+.25*GP1DXR*(PHI(JP1,K)-PHIU(JG+1,K))
  IF (ALAMB.LT.0.) GO TO 80
  OMEGA(K)=SUB
  ACHECK=ACHK(K)
  ACHK(K)=ALAMB
  BCHK(K)=ACHK(K)-ZMACH
  BBAR(K)=-2.*DXSQR*ALAMB
  DBAR(K)=ALAMB*DXSQR*(PHI(JP1,K)+PHIM1)
  IF (IWO.EQ.1) DBAR(K)=DBAR(K)+.5*ALAMB*DXSQR*(PHIU(JG+1,K)-PHI(JP1
1,K))
  IF (ACHECK.GT.0.) GO TO 110
  IF ((IGUN(JM2).LT.K) GO TO 60
  PHIM2=PHI(JM2,K)
  GO TO 70
60 PHIM2=PHI(JM2,K)-RWR(K)*FUN3(JM2)-FUNX(JM2)
70 BBAR(K)=BBAR(K)+ACHECK*DXSQR
  DBAR(K)=DBAR(K)+ACHECK*DXSQR*(-2.*PHIM1+PHIM2)
  BCHK(K)=BCHK(K)+ACHECK-ZMACH
  OMEGA(K)=1.
  GO TO 110
80 OMEGA(K)=1.
  IF ((IGUN(JM2).LT.K) GO TO 90

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PHIM2=PHI(JM2,K)	D 850
GO TO 100	D 860
90 PHIM2=PHI(JM2,K)-RWR(K)*FUN3(JM2)-FUNX(JM2)	D 870
100 SAVE=ALAMB	D 880
ALAMB=BETASQ-GP1DXR*(PHI(J,K)-PHIM10)-GAMP1*U	D 890
IF (ALAMB.GT.0.) ALAMB=0.	D 900
IF (ACHK(K).GT.0.) OMEGA(K)=SUPP	D 910
ACHK(K)=SAVE	D 920
BCHK(K)=ALAMB-ZMACH	D 930
BBAR(K)=DXSQR*ALAMB	D 940
DBAR(K)=DXSQR*ALAMB*(-2.*PHIM1+PHIM2)	D 950
110 PHIM1=PHI(JM1,K+1)	D 960
PHIM10=PHIOLD(K+1)	D 970
IF (IGUN(JM1).GT.K) GO TO 120	D 980
PHIM1=PHIM1-RWR(K+1)*FUN3(JM1)-FUNX(JM1)	D 990
PHIM10=PHIM10-RWR(K+1)*FUN3(JM1)-FUNX(JM1)	D1000
120 CONTINUE	D1010
IF (KLO.NE.1) GO TO 130	D1020
KLO=KGUN	D1030
KUP=KGUN	D1040
GO TO 30	D1050
130 IF (IW.EQ.0) GO TO 210	D1060
C	D1070
C PART 2 B AND D ARRAYS BENEATH WING	D1080
C	D1090
IF (J.LT.JW10.OR.J.GT.JW3) GO TO 190	D1100
IFUMJ=IFUM(JG)	D1110
JGM1=JG-1	D1120
JGP1=JG+1	D1130
JGM2=JG-2	D1140
IFNJP2=IFUN(J+2)	D1150
IF (J.GT.JW10) GO TO 150	D1160
DO 140 K=IFUMJ,IFNJP2	D1170
PHIU(1,K)=PHI(JW10M2,K)	D1180
140 PHIU(2,K)=PHI(JW10M1,K)	D1190
GO TO 161	D1200
150 IFNO1=IFUN(JM1)+1	D1210
IFNO2=IFUN(JP1)	D1220
DO 160 K=IFNO1,IFNO2	D1221
160 PHIU(JGM1,K)=PHI(JM1,K)	D1222
161 U=-FUN4(J)-2.*FUNO(J)	D1223
DO 180 K=IFUMJ,IFUNJ	D1230
ALAMBU=BETASQ-.5*GP1DXR*(PHIU(JGP1,K)-PHIUO(K))-GAMP1*U	D1240



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IF (ALAMBU.LT.0.) GO TO 170
OMEGAU(K)=SUB
ACHECK=ACHKU(K)
ACHKU(K)=ALAMBU
BCHKU(K)=ALAMBU-ZMACH
BBARU(K)=-2.*DXSQR*ALAMBU
DBARU(K)=ALAMBU*DXSQR*(PHIU(JGP1,K)+PHIU(JGM1,K))
IF (ACHECK.GT.0.) GO TO 180
BBARU(K)=BBARU(K)+ACHECK*DXSQR
DBARU(K)=DBARU(K)+ACHECK*DXSQR*(-2.*PHIU(JGM1,K)+PHIU(JGM2,K))
BCHKU(K)=ALAMBU+ACHECK-2.*ZMACH
OMEGAU(K)=1.
GO TO 180
170 OMEGAU(K)=1.
SAVE=ALAMBU
ALAMBU=BETASQ-GP1DXR*(PHIU(JG,K)-PHIUO(K))-GAMP1*U
IF (ALAMBU.GT.0.) ALAMBU=0.
IF (ACHKU(K).GT.0.) OMEGAU(K)=SUPP
ACHKU(K)=SAVE
BCHKU(K)=ALAMBU-ZMACH
BBARU(K)=DXSQR*ALAMBU
DBARU(K)=DXSQR*ALAMBU*(-2.*PHIU(JGM1,K)+PHIU(JGM2,K))
180 CONTINUE
190 IF (J.NE.JW10M1) GO TO 210
KUO=IFUN(JW10+1)
DO 200 K=1,KUO
ACHKU(K)=ACHK(K)
BCHKU(K)=BCHK(K)
200 PHIUO(K)=PHI(JW10M1,K)

C
C PART 3 B AND D ARRAYS IN OUTER REGION
C
210 IF (IGUM(JP1).LT.KGUNP1) GO TO 220
PHIP1=PHI(JP1,KGUNP1)+RWR(KGUNP1)*FUN3(JP1)+FUNX(JP1)
GO TO 230
220 PHIP1=PHI(JP1,KGUNP1)
230 DO 260 K=KGUNP1,KMM1
ALAMB=BETASQ-.5*GP1DXR*(PHIP1-PHIOLD(K))
IF (ALAMB.LT.0.) GO TO 240
OMEGA(K)=SUB
ACHECK=ACHK(K)
ACHK(K)=ALAMB
BBAR(K)=-2.*DXSQR*ALAMB

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DBAR(K)=ALAMB*DXSQR*(PHIP1+PHI(JM1,K))	D1690
IF (ACHECK.GT.0.) GO TO 250	D1700
BBAR(K)=BBAR(K)+ACHECK*DXSQR	D1710
DBAR(K)=DBAR(K)+ACHECK*DXSQR*(-2.*PHI(JM1,K)+PHI(JM2,K))	D1720
OMEGA(K)=1.	D1740
GO TO 250	D1750
240 OMEGA(K)=1.	D1760
SAVE=ALAMB	D1770
ALAMB=BETASQ-GP1DXR*(PHI(J,K)-PHIOLD(K))	D1780
IF (ALAMB.GT.0.) ALAMB=0.	D1790
IF (ACHK(K).GT.0.) OMEGA(K)=SUPP	D1800
ACHK(K)=SAVE	D1810
BBAR(K)=DXSQR*ALAMB	D1830
DBAR(K)=DXSQR*ALAMB*(-2.*PHI(JM1,K)+PHI(JM2,K))	D1840
250 PHIP1=PHI(JP1,K+1)	D1850
IF (IGUN(JP1).LE.K) GO TO 260	D1860
PHIP1=PHIP1+RWR(K+1)*FUN3(JP1)+FUNX(JP1)	D1870
260 CONTINUE	D1880
	D1890
C	D1900
C	D1910
C	D1920
PART 4 B AND D ARRAYS AT OUTER WALL	D1930
IF (IWALL.EQ.0) GO TO 280	D1940
ALAMB=BETASQ-.5*GP1DXR*(PHIP1-PHIOLD(KM))	D1950
IF (ALAMB.LT.0.) GO TO 270	D1960
OMEGA(KM)=SUB	D1970
ACHECK=ACHK(KM)	D1990
ACHK(KM)=ALAMB	D2000
BBAR(KM)=-2.*DXSQR*ALAMB	D2010
DBAR(KM)=ALAMB*DXSQR*(PHIP1+PHI(JM1,KM))	D2020
IF (ACHECK.GT.0.) GO TO 280	D2030
BBAR(KM)=BBAR(KM)+ACHECK*DXSQR	D2050
DBAR(KM)=DBAR(KM)+ACHECK*DXSQR*(-2.*PHI(JM1,KM)+PHI(JM2,KM))	D2060
OMEGA(KM)=1.	D2070
GO TO 280	D2080
270 OMEGA(KM)=1.	D2090
SAVE=ALAMB	D2100
ALAMB=BETASQ-GP1DXR*(PHI(J,KM)-PHIOLD(KM))	D2110
IF (ALAMB.GT.0.) ALAMB=0.	D2120
IF (ACHK(KM).GT.0.) OMEGA(KM)=SUPP	D2140
ACHK(KM)=SAVE	D2150
BBAR(KM)=DXSQR*ALAMB	D2160
DBAR(KM)=DXSQR*ALAMB*(-2.*PHI(JM1,KM)+PHI(JM2,KM))	
280 DX23=2.*DX	

	DX12=2.*DX	D2170
	DX2=DX	D2180
	GO TO 340	D2190
C		D2200
C	PART 5 B AND D ARRAYS IN X-STRETCHED REGION	D2210
C		D2220
290	DX2=XW(J)-XW(JM1)	D2230
	IF (J.EQ.J5) GO TO 300	D2240
	DX3=XW(JP1)-XW(J)	D2250
	DX23=DX2+DX3	D2260
	DDD23R=1./(DX2*DX3*DX23)	D2270
	D23=DDD23R*GAMP1	D2280
300	IF (J.EQ.2) GO TO 310	D2290
	DX1=XW(JM1)-XW(JM2)	D2300
	DX12=DX1+DX2	D2310
	DDD12R=1./(DX1*DX2*DX12)	D2320
	D12=DDD12R*GAMP1	D2330
310	DO 330 K=1,KF	D2340
	ALAMB=BETASQ-D23*(DX2**2*PHI(JP1,K)+(DX3-DX2)*DX23*PHI(J,K)-DX3**2	D2350
	1*PHIOLD(K))	D2360
	ACHECK=ACHK(K)	D2361
	ACHK(K)=ALAMB	D2370
	BCHK(K)=ALAMB-ZMACH	D2380
	IF (ALAMB.LT.0..AND.J.NE.2) GO TO 320	D2390
	OMEGA(K)=SUB	D2400
	BBAR(K)=-2.*DX23*DDD23R*ALAMB	D2410
	DBAR(K)=2.*DDD23R*ALAMB*(DX2*PHI(JP1,K)+DX3*PHI(JM1,K))	D2420
	IF (ACHECK.GT.0..OR.J.EQ.2) GO TO 330	D2421
	BBAR(K)=BBAR(K)+2.*DDD12R*DX1*ACHECK	D2422
	DBAR(K)=DBAR(K)+2.*DDD12R*(-DX12*PHI(JM1,K)+DX2*PHI(JM2,K))*ACHECK	D2423
	BCHK(K)=BCHK(K)+ACHECK-ZMACH	D2424
	OMEGA(K)=1.	D2425
	GO TO 330	D2430
320	OMEGA(K)=1.	D2440
	ALAMB=BETASQ-D12*DX1*DX12*(PHI(J,K)-PHIOLD(K))	D2441
	IF (ALAMB.GT.0.) ALAMB=0.	D2442
	IF (ACHECK.GT.0.) OMEGA(K)=SUPP	D2443
	BCHK(K)=ALAMB-ZMACH	D2444
	BBAR(K)=2.*DDD12R*DX1*ALAMB	D2450
	DBAR(K)=2.*DDD12R*(-DX12*PHI(JM1,K)+DX2*PHI(JM2,K))*ALAMB	D2451
330	CONTINUE	D2470
C		D2480
C	PART 6 C ARRAY, FINAL PREPARATION OF B ARRAY	D2490

C		D2500
	340 DO 350 K=1,KF	D2510
	BBAR(K)=-2.*CON2(K)*BBAR(K)	D2520
	350 CBAR(K)=1.*CON1(K)	D2530
C		D2540
C	PART 7 FINAL PREPARATION OF PRIMARY D ARRAY IN INNER REGION	D2550
C		D2560
	KGUN=IGUN(J)	D2570
	DO 370 K=1,KGUN	D2580
	IF (K.LE.IFUN(J)) GO TO 360	D2590
	DBAR(K)=-BCHK(K)*(CON3(K)*RW(K)*FUN1(J)+CON2(K)*FUN7(J))-CON2(K)*D	D2600
	1 BAR(K)+CON7(K)*FUN8(J)+4.*CON3(K)*FUNY(J)	D2610
	GO TO 370	D2620
	360 DBAR(K)=-CON2(K)*(BCHK(K)*FUN5(J)+DBAR(K))+CON8(K)*FUN9(J)+CON9(K)	D2630
	1 *FUN10(J)	D2640
	370 CONTINUE	D2650
	IF (IW.NE.0.OR.ALPHAD.EQ.0.) GO TO 390	D2660
	IF (J.LT.JW10) GO TO 390	D2670
	IF (IWALL.EQ.0.OR.KUPA(J).LT.KM) GO TO 390	D2680
	DO 380 K=IFNJPI,KGUN	D2690
	380 DBAR(K)=DBAR(K)-CON10(K)*FUN11(J)	D2700
	390 DBAR(1)=DBAR(1)+CON4*SPRIME(J)	D2710
	KGUNPI=KGUN+1	D2720
	DBAR(KGUN)=DBAR(KGUN)+CBAR(KGUN)*(RWR(KGUNPI)*FUN3(J)+FUNX(J))	D2730
		D2740
C		D2750
C	PART 8 C ARRAY BENEATH WING, FINAL PREPARATION OF B AND D ARRAYS	D2760
C	BENEATH WING	D2770
C		D2780
	IF (IW.EQ.0) GO TO 420	D2790
	IF (J.LT.JW10.OR.J.GT.JW3) GO TO 420	D2800
	DO 400 K=IFUMJ,IFUNJ	D2810
	BBARU(K)=-2.*CON2(K)*BBARU(K)	D2820
	CBARU(K)=CBAR(K)	D2830
	400 DBARU(K)=CON2(K)*(BCHKU(K)*FUN5(J)-DBARU(K))+CON8(K)*FUN9(J)+CON9(	D2840
	1 K)*FUN10(J)	D2850
	IF (IFUMJ.GT.1) GO TO 410	D2860
	DBARU(1)=DBARU(1)+CON4*SPRIME(J)	D2870
	GO TO 420	D2880
	410 DBARU(IFUMJ)=DBARU(IFUMJ)-ABAR(IFUMJ)*PHIU(JG,IFUMJ-1)	D2890
		D2900
C		D2910
C	PART 9 FINAL PREPARATION OF D ARRAY IN OUTER REGION FOR SUBSONIC	D2920
C	FREE STREAM MACH NUMBERS	

420	IF (AMINF.GT.1.) GO TO 480	D2930
	AX=ABS(XW(J))	D2940
	IF (J.GE.JXN.AND.J.LE.J3) GO TO 440	D2950
	DO 430 K=KGUNP1,KF	D2960
	XOCR=AX/SQRT(AX**2+BETASQ*RW(K)**2)	D2970
430	DBAR(K)=CON3(K)*(RWR(K)*(XOCR*FUN3(J)+.5*(1.-XOCR)*FUN3(JW3))+4.*X	D2980
	1OCR**2*FUNY(J))-CON2(K)*DBAR(K)+CON7(K)*FUN8(J)	D2990
	GO TO 470	D3000
440	DO 450 K=KGUNP1,KF	D3010
	XOCR=AXOCR(K)	D3020
450	DBAR(K)=CON3(K)*(RWR(K)*(XOCR*FUN3(J)+.5*(1.-XOCR)*FUN3(JW3))+4.*X	D3030
	1OCR**2*FUNY(J))-CON2(K)*DBAR(K)+CON7(K)*FUN8(J)	D3040
	IF (ALPHAD.EQ.0.) GO TO 470	D3050
	IF (J.LT.JW10) GO TO 470	D3060
	IF (IWALL.EQ.0) GO TO 470	D3070
	DO 460 K=KGUNP1,KF	D3080
460	DBAR(K)=DBAR(K)-CON10(K)*FUN11(J)-CON11(K)*FUN12(J)	D3090
470	DBAR(KGUNP1)=DBAR(KGUNP1)-ABAR(KGUNP1)*(RWR(KGUN)*FUN3(J)+FUNX(J))	D3100
	GO TO 620	D3110
C		D3120
C	PART 10 FINAL PREPARATION OF D ARRAY IN OUTER REGION FOR	D3130
C	SUPERSONIC FREE STREAM MACH NUMBERS	D3140
C		D3150
480	IF (J.GT.JW1X) GO TO 490	D3160
	KLO=KGUNP1	D3170
	GO TO 590	D3180
490	IF (J.GT.JW3X) GO TO 500	D3190
	KUP=KUPA(J)	D3200
	KLO=KGUNP1	D3210
	GO TO 520	D3220
500	KUP=KLJA(J)	D3230
	XWJ=XW(J)	D3240
	DO 510 K=KGUNP1,KUP	D3250
	BRSQ=(BETA*RW(K))**2	D3260
	ANUM1=SQRT(XWJ**2-BRSQ)	D3270
	ANUM2=SQRT(ABS((XWJ-XWM)**2-BRSQ))	D3280
510	DBAR(K)=-CON2(K)*DBAR(K)+CON3(K)*RWR(K)*FUN3(M)*XWMSQR*(XWJ*ANUM1-	D3290
	1(XWJ+XWM)*ANUM2+BRSQ*(ALOG(XWJ-XWM+ANUM2)-ALOG(XWJ+ANUM1)))	D3300
	IF (KUP.EQ.KF) GO TO 610	D3310
	KLO=KUP+1	D3320
	KUP=KUPA(J)	D3330
520	Z=XW(J)-BETA*RW(KLO)	D3340
	JJ=-1	D3350

530	JJ=JJ+1	D3360
	JX=J-JJ	D3370
	IF (Z.LT.XW(JX)) GO TO 530	D3380
	XWJ=XW(J)	D3390
	DO 550 K=KLO,KUP	D3400
	BR=BETA*RW(K)	D3410
	Z=XWJ-BR	D3420
	ZR=1./Z	D3430
	JJ=-1	D3440
540	JJ=JJ+1	D3450
	JX=JX-JJ	D3460
	IF (Z.LT.XW(JX)) GO TO 540	D3470
550	DBAR(K)=CON3(K)*(RWR(K)*FUN3(JX)*(XWJ*ZR**1.5*SQRT(XWJ+BR)+(BR*ZR)	D3480
	1**2*(ALOG(BR)-ALOG(XWJ+SQRT(XWJ**2-BR**2)))+4.*FUNY(J))-CON2(K)*D	D3490
	2BAR(K)+CON7(K)*FUN8(J)	D3500
	IF (ALPHAD.EQ.0.) GO TO 570	D3510
	IF (J.LT.JW10) GO TO 570	D3520
	IF (KUP.LT.KM) GO TO 580	D3530
	IF (IWALL.EQ.0) GO TO 570	D3540
	DO 560 K=KLO,KUP	D3550
560	DBAR(K)=DBAR(K)-CON10(K)*FUN11(J)-CON11(K)*FUN12(J)	D3560
570	IF (KUP.EQ.KF) GO TO 610	D3570
580	KLO=KUP+1	D3580
590	DO 600 K=KLO,KF	D3590
600	DBAR(K)=-CON2(K)*DBAR(K)	D3600
610	DBAR(KGUNP1)=DBAR(KGUNP1)-ABAR(KGUNP1)*(RWR(KGUN)*FUN3(J)+FUNX(J))	D3610
C		D3620
C	PART 11 FINAL PREPARATION OF B AND D ARRAYS AT WALL	D3630
C		D3640
620	IF (IWALL.EQ.0) GO TO 640	D3650
	IF (IWALL.EQ.2) GO TO 630	D3660
	BBAR(KM)=BBAR(KM)+CBAR(KM)-H/DX2	D3670
	DBAR(KM)=DBAR(KM)-H/DX2*PHI(JM1,KM)	D3680
	IF (OMEGA(KM).GT.1.) OMEGA(KM)=1.	D3690
	GO TO 640	D3700
630	BBAR(KM)=BBAR(KM)+CBAR(KM)-H	D3710
C		D3720
C	PART 12 FIRST SWEEP OF THOMAS ALGORITHM(ABOVE AND BENEATH WING)	D3730
C		D3740
640	IF (IW.EQ.0) GO TO 670	D3750
	IF (IFUNJ.EQ.1) GO TO 660	D3760
	IF (J.LT.JW10.OR.J.GT.JW3) GO TO 670	D3770
	DO 650 K=2,IFUNJ	D3780

	KM1=K-1	D3790
	BBAR(K)=ABAR(K)*CBAR(KM1)-BBAR(K)*BBAR(KM1)	D3800
	CBAR(K)=-CBAR(K)*BBAR(KM1)	D3810
	DBAR(K)=ABAR(K)*DBAR(KM1)-DBAR(K)*BBAR(KM1)	D3820
	IF (K.LE. IFUMJ) GO TO 650	D3830
	BBARU(K)=ABAR(K)*CBARU(KM1)-BBARU(K)*BBARU(KM1)	D3840
	CBARU(K)=-CBARU(K)*BBARU(KM1)	D3850
	DBARU(K)=ABAR(K)*DBARU(KM1)-DBARU(K)*BBARU(KM1)	D3860
650	CONTINUE	D3870
660	K=IFNJPI	D3880
	KM1=K-1	D3890
	BBAR(K)=.5*ABAR(K)*(BBARU(KM1)*CBAR(KM1)+BBAR(KM1)*CBARU(KM1))-BBA	D3900
	1R(K)*BBARU(KM1)*BBAR(KM1)	D3910
	CBAR(K)=-CBAR(K)*BBARU(KM1)*BBAR(KM1)	D3920
	DBAR(K)=.5*ABAR(K)*(BBARU(KM1)*DBAR(KM1)+BBAR(KM1)*DBARU(KM1))-DBA	D3930
	1R(K)*BBARU(KM1)*BBAR(KM1)	D3940
C		D3950
C	PART 13 FIRST SWEEP OF THOMAS ALGORITHM(GENERAL CASE)	D3960
C		D3970
	KB=K+1	D3980
	KT=KF-IFNJPI	D3990
	GO TO 680	D4000
670	KB=2	D4010
	KT=KFM1	D4020
680	DO 690 K=KB,KF	D4030
	KM1=K-1	D4040
	BBAR(K)=ABAR(K)*CBAR(KM1)-BBAR(K)*BBAR(KM1)	D4050
	CBAR(K)=-CBAR(K)*BBAR(KM1)	D4060
690	DBAR(K)=ABAR(K)*DBAR(KM1)-DBAR(K)*BBAR(KM1)	D4070
C		D4080
C	PART 14 SECOND SWEEP OF THOMAS ALGORITHM	D4090
C		D4100
	PHIO(KF)=DBAR(KF)/BBAR(KF)	D4110
	DO 700 KK=1,KT	D4120
	K=KF-KK	D4130
	KP1=K+1	D4140
700	PHIO(K)=(DBAR(K)-CBAR(K)*PHIO(KP1))/BBAR(K)	D4150
	IF (IW.EQ.0) GO TO 720	D4160
	IF (J.LT.JW10.OR.J.GT.JW3) GO TO 720	D4170
	PHIOU(IFUNJ+1)=PHIO(IFUNJ+1)	D4180
	DO 710 KK=1,IFUNJ	D4190
	K=IFNJPI-KK	D4200
	KP1=K+1	D4210

	PHIO(K)=(DBAR(K)-CBAR(K)*PHIO(KP1))/BBAR(K)	D4220
710	PHIOU(K)=(DBARU(K)-CBARU(K)*PHIOU(KP1))/BBARU(K)	D4230
C		D4240
C	PART 15 NEW VALUES OF VELOCITY POTENTIAL, MAXIMUM DPHI	D4250
C		D4260
720	DO 730 K=1,KF	D4270
	PHIOLD(K)=PHI(J,K)	D4280
	DPHI=OMEGA(K)*(PHIO(K)-PHI(J,K))	D4290
	IF (ABS(DPHI).LE.ABS(DPHIMX)) GO TO 730	D4300
	DPHIMX=DPHI	D4310
	JMARK=J	D4320
	KMARK=K	D4330
730	PHI(J,K)=PHI(J,K)+DPHI	D4340
	IF (IW.EQ.0) GO TO 780	D4350
	IF (J.LT.JW10.OR.J.GT.JW3P1) GO TO 780	D4360
	IF (J.LE.JW2.OR.IFUM(JG).EQ.1) GO TO 750	D4370
	IFUMM1=IFUM(JG)-1	D4380
	IFMJM1=IFUM(JG-1)	D4390
	DO 740 K=IFMJM1,IFUMM1	D4400
740	PHIU(JG,K)=PHI(J,K)+PHIU(JG-1,K)-PHI(J-1,K)+DLTPH	D4410
	IF (IFUMM1.EQ.IFUMJ) GO TO 780	D4420
750	IFNJPI=IFUN(J+1)	D4430
	DO 760 K=1,IFNJPI	D4440
760	PHIUD(K)=PHIU(JG,K)	D4450
	DO 770 K=IFUMJ,IFUNJ	D4460
	DPHI=OMEGA(K)*(PHIOU(K)-PHIU(JG,K))	D4470
	IF (ABS(DPHI).LE.DPHIMX) GO TO 770	D4480
	DPHIMX=DPHI	D4490
	JMARK=-J	D4500
	KMARK=-K	D4510
770	PHIU(JG,K)=PHIU(JG,K)+DPHI	D4520
780	CONTINUE	D4530
	IF (AMINF.LE.1.) GO TO 800	D4540
	DO 790 K=1,KF	D4550
C		D4570
C	PART 16 PRINT MAXIMUM DPHI, CHECK CONVERGENCE	D4580
C		D4590
790	PHI(J5,K)=2.*PHI(J5-1,K)-PHI(J5-2,K)	D4560
800	PRINT 850, I,JMARK,KMARK,DPHIMX	D4600
	IF (I.GT.1) SUPP=SUP	D4610
	IF (I.EQ.IMAX) RETURN	D4620
	IF (ABS(DPHIMX).GE.EPS1) GO TO 10	D4630
	RETURN	D4640



C

810 FORMAT (16H SUBROUTINE WORK///)  
820 FORMAT (52H LOCATION AND VALUE OF GREATEST CHANGE IN VELOCITY)  
830 FORMAT (48H POTENTIAL ( NEGATIVE LOCATION INDICES ARE FOR)  
840 FORMAT (22H POINTS UNDER WING ///)  
850 FORMAT (3H I=15,2X,6HJMARK=15,2X,6HKMARK=15,2X,7HDPHIMX=E16.8)  
END

D4650  
D4660  
D4670  
D4680  
D4690  
D4700  
D4710-

OVERLAY (DICK,1,3)	E	0
PROGRAM RESULT	E	10
COMMON SIGMA,DELTA,I,BETASQ,DXR,DXSQR,GAMP1,GP1DXR,KMM1,KFM1,KF,DE	E	20
1LETA,PIR,CON4,CON5,H,JT,JI,JF,DPHIMX,DX,JXN,SNO,CS20,SNALP,IJW,JW1	E	30
20,JW20,JW1X,JW3X,BETA,JW3M1,DLTPH,JCHCK,IW,JW1CM2,JW3P1,JW1DM1,M,X	E	40
3WM,XWMSQR,PI,AK2,AX2,AK1,AX1,AX10,CNX,NAMXP1,A1,A2,ZMACH,JMCK	E	50
COMMON R(120),SPRIME(120),FUN(120),XW(120),Y1(120),Y2(120),FUN1(12	E	60
10),FUN0(120),IFUN(120),FUN2(120),FUN3(120),FUN4(120),IGUN(120),CP(	E	70
2120),FUNX(120),SLAS(120,6),CPO(120),KLOA(120),KUPA(120),FUN5(120),	F	80
3FUN6(120),FUN7(120),FUNY(120),CP1(120),CP2(120)	E	90
COMMON FUN8(120),FUN9(120),FUN10(120),FUN11(120),Y2PRM(120),FUN12(	E	100
1120),FUNA(120),FUNB(120)	E	110
COMMON CON7(100),CON8(100),CON9(100),CON10(100),CON11(100),CON1(10	F	120
10),CON2(100),CON3(100),OMEGA(100),ABAR(100),BBAR(100),CBAR(100),DB	E	130
2AR(100),PHIO(100),RW(100),RWR(100),AXOCR(100),ACHK(100),PHIDLD(100	F	140
3),BCHK(100)	E	150
COMMON PHIUO(25),OMEGAU(25),ACHKU(25),BBARU(25),CBARU(25),DBARU(25	E	160
1),BCHKU(25),PHIOU(25)	E	170
COMMON IFUM(50),VLAM(50),VTAU(50),VLAMP(50),VTAUP(50),YV(50),ZV(50	E	180
1),FUNAO(50),FUNBO(50),UUOD(50),UU9OD(50)	E	190
COMMON PHI(109,50),PHIU(50,25),COEF(21)	E	200
COMMON /NMLIST/ J1,J2,J3,J4,J5,FAC,KM,RCOM,A,B,IWALL,P,OMEGAD,ALPH	E	210
1AD,HSPAN,AMINF,GAMMA,IR,RC,RMAX,RN,JS,RS,JW1,JW2,JW3,JWD,IWING,B1,	E	220
2B2,DEL1,DEL,IVOR,IDIR,EPSI,SUB,SUP,IMAX,SFACTOR	E	230
DIMENSION NAM(2)	E	240
DATA NAM/7HBBAR(K),6HFUN(J)/	F	250
	E	260
PART 1 SHOCK-WAVE AND SONIC LINE LOCATIONS	E	270
	E	280
PRINT 1070	E	290
IF (AMINF.GT.1.) J1=J1+2	E	300
IF (AMINF.GT.1.) J4=J4-2	E	310
DO 250 J=J1,J4	E	320
KK=1	F	330
KK2=1	E	340
JP1=J+1	E	350
JM1=J-1	E	360
JM2=J-2	E	370
DO 170 K=1,KF	E	380
IF (RW(K).LT.R(J)) GO TO 160	E	390
IF (K.LE.IGUN(JM1).AND.K.GT.IFUN(J)) GO TO 10	E	400
PHIM1=PHI(JM1,K)	E	410

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IF (K.LE.IGUN(JP1).AND.K.GT.IFUN(J)) GO TO 20	E 420
PHIP1=PHI(JP1,K)	E 430
GO TO 30	E 440
10 PHIM1=PHI(JM1,K)+RWR(K)*FUN3(JM1)+FUNX(JM1)	E 450
20 PHIP1=PHI(JP1,K)+RWR(K)*FUN3(JP1)+FUNX(JP1)	E 460
30 U=.5*DXR*(PHIP1-PHIM1)	E 470
IF (K.LE.IFUN(J)) U=U+FUN4(J)	E 480
ALAMB=BETASQ-GAMP1*U	E 490
IF (K.LE.IGUN(JM2).AND.K.GT.IFUN(J)) GO TO 40	E 500
PHIM2=PHI(JM2,K)	E 510
IF (K.LE.IGUN(J).AND.K.GT.IFUN(J)) GO TO 50	E 520
PHIMO=PHI(J,K)	E 530
IF (K.LE.IGUN(J+2).AND.K.GT.IFUN(J)) GO TO 60	E 540
FIP2=PHI(J+2,K)	E 550
GO TO 70	E 560
40 PHIM2=PHI(JM2,K)+RWR(K)*FUN3(JM2)+FUNX(JM2)	E 570
50 PHIMO=PHI(J,K)+RWR(K)*FUN3(J)+FUNX(J)	E 580
60 FIP2=PHI(J+2,K)+RWR(K)*FUN3(J+2)+FUNX(J+2)	E 590
70 FIP1=PHIP1	E 600
FIMO=PHIMO	E 610
FIM1=PHIM1	E 620
FIM2=PHIM2	E 630
IF (ALAMB.GT.0.) GO TO 80	E 640
U=.5*DXR*(3.*PHIMO-4.*PHIM1+PHIM2)	E 650
IF (K.LE.IFUN(J)) U=U+FUN4(J)	E 660
ALAMB=BETASQ-GAMP1*U	E 670
IF (ALAMB.LT.0.) GO TO 80	E 680
U=BETASQ/GAMP1	E 690
80 IF (K.EQ.1) GO TO 130	E 700
IF (K.EQ.KF) GO TO 140	E 710
KM1=K-1	E 720
KP1=K+1	E 730
DR1=RW(K)-RW(KM1)	E 740
DR2=RW(KP1)-RW(K)	E 750
DD1=DR1/(DR2*(DR1+DR2))	E 760
DD2=(DR2-DR1)/(DR1*DR2)	E 770
DD3=-DR2/(DR1*(DR1+DR2))	E 780
IF (KP1.LE.IGUN(J).AND.K.GT.IFUN(J)) GO TO 90	E 790
PHIP1=PHI(J,KP1)	E 800
IF (K.LE.IGUN(J).AND.K.GT.IFUN(J)) GO TO 100	E 810
PHIMO=PHI(J,K)	E 820
IF (KM1.LE.IGUN(J).AND.K.GT.IFUN(J)) GO TO 110	E 830
PHIM1=PHI(J,KM1)	E 840

GO TO 120	E 850
90 PHIP1=PHI(J,KP1)+RWR(KP1)*FUN3(J)+FUNX(J)	E 860
100 PHIMO=PHI(J,K)+RWR(K)*FUN3(J)+FUNX(J)	E 870
110 PHIM1=PHI(J,KM1)+RWR(KM1)*FUN3(J)+FUNX(J)	E 880
120 V=DD1*PHIP1+DD2*PHIMO+DD3*PHIM1	E 890
GO TO 150	E 900
130 V=.5*DXR*(R(JP1)-R(JM1))-SNALP*SNO	E 910
GO TO 150	E 920
140 KM1=K-1	E 930
V=(PHI(J,K)-PHI(J,KM1))/(RW(K)-RW(KM1))	E 940
150 CSO=SQRT(ABS(1.-SNO**2))	E 950
SN2O=2.*SNO*CSO	E 960
W=(SNALP*CSO/RW(K)*FUN3(J)-.5*FUN(J)*SN2O)/RW(K)	E 970
IF (K.LE.IFUN(J)) V=V-SNALP*SNO	E 980
IF (K.LE.IFUN(J)) W=0.	E 990
USQ=(1.+U)**2+V**2+W**2	E1000
OMEGA(K)=AMINF*SQRT(ABS(USQ/(1.+5*(GAMMA-1.)*AMINF**2*(1.-USQ))))	E1010
PHIOLD(K)=(FIP1-FIM2-3.*(FIMO-FIM1))*DXR**3	E1020
PHIO(K)=(FIP2-FIM1-3.*(FIP1-FIMO))*DXR**3	E1030
BBAR(K)=DXR**2*(FIP1+FIM1-2.*FIMO)	E1040
GO TO 170	E1050
160 KK=KK+1	E1060
170 CONTINUE	E1070
KKP1=KK+1	E1080
KTT=KF+KKP1	E1090
IIC=0	E1100
KKP10=KKP1	E1110
DO 180 II=1,6	E1120
180 SLAS(J,II)=0.	E1130
DO 240 I=1,6	E1140
DO 220 KI=KKP1,KF	E1150
K2=KTT-K1	E1160
K2M1=K2-1	E1170
IF (OMEGA(K2).GT.1..AND.OMEGA(K2M1).GT.1.) GO TO 190	E1180
IF (OMEGA(K2).LT.1..AND.OMEGA(K2M1).LT.1.) GO TO 220	E1190
SLAS(J,II)=RW(K2)-(RW(K2)-RW(K2M1))*(OMEGA(K2)-1.)/(OMEGA(K2)-OMEG	E1200
1A(K2M1))	E1210
GO TO 230	E1220
190 IF (PHIOLD(K2).GT.0..OR.PHIO(K2).LT.0.) GO TO 220	E1230
IF (BBAR(K2).GT.0.) GO TO 220	E1240
IF (K2.EQ.KF.OR.K2.EQ.KKP10) GO TO 220	E1250
IF (PHIOLD(K2M1).GT.0..AND.PHIOLD(K2+1).GT.0.) GO TO 220	E1260
IF (PHIOLD(K2M1).GT.0.) GO TO 200	E1270

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      IF (PHIOLD(K2+1).GT.0.) GO TO 210
      GO TO 220
200  SLAS(J,II)=RW(K2)+(RW(K2-1)-RW(K2))*PHIOLD(K2)/(PHIOLD(K2)-PHIOLD(
      IK2-1))
      GO TO 230
210  SLAS(J,II)=RW(K2)+(RW(K2+1)-RW(K2))*PHIOLD(K2)/(PHIOLD(K2)-PHIOLD(
      IK2+1))
      GO TO 230
220  CONTINUE
      GO TO 250
230  KKP1=K1+1
      IF (KKP1.GT.KF) GO TO 250
240  CONTINUE
250  PRINT 1080, J,XW(J),(SLAS(J,II),II=1,6)

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E1280  
 E1290  
 E1300  
 E1310  
 E1320  
 E1330  
 E1340  
 E1350  
 E1360  
 E1370  
 E1380  
 E1390  
 E1400  
 E1410  
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 E1430  
 E1440  
 E1450  
 E1460  
 E1470  
 E1471  
 E1480  
 E1490  
 E1500  
 E1510  
 E1520  
 E1530  
 E1540  
 E1550  
 E1560  
 E1570  
 E1580  
 E1590  
 E1600  
 E1610  
 E1620  
 E1630  
 E1640  
 E1650  
 E1660  
 E1670  
 E1680  
 E1690

C  
 C  
 C

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      PART 2  PRESSURE COEFFICIENTS AT GRID POINTS

      PRINT 1090
      IF (IW.EQ.0) GO TO 290
      IFNJW3=IFUN(JW3)
      PHIU(JW3-JW10+3,IFNJW3+1)=PHI(JW3,IFNJW3+1)
      DO 280 K=1,IFNJW3
      IMK=0
      DO 280 J=JW2,JW3P1
      JG=J-JW10+3
      IF (IMK.EQ.1) GO TO 260
      IF (IMK.EQ.2) GO TO 270
      IF (IFUM(JG+1).LE.K) GO TO 280
      IMK=1
      CGNN=PHIU(JG,K)-PHI(J,K)
      GO TO 280
260  IMK=2
      GO TO 280
270  PHIU(JG,K)=PHI(J,K)+CGNN
280  CONTINUE
290  IF (IVOR.EQ.0) GO TO 300
      IF (JCHCK.EQ.JW3) GO TO 300
      JG=JCHCK-JW10+3
      GAND=.5*Y2(JCHCK)*(VLAM(JG)+VTAU(JG)**2/VLAM(JG))
      GAND=GAND*FUNA(JCHCK)*(1.+(R(JCHCK)/Y2(JCHCK))**2)
300  DO 530 K=1,KF
      ALAMB=1.
      DO 520 J=J1,J4

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JP1=J+1	E1700
JM1=J-1	F1710
JM2=J-2	E1720
ACHKK=ALAMB	E1730
JG=J-JW10+3	E1740
IF (K.GT.IFUN(J)) GO TO 310	E1750
PHIM1=PHI(JM1,K)	E1760
PHIM0=PHI(J,K)	E1770
PHIP1=PHI(JP1,K)	E1780
GO TO 350	E1790
310 IF (K.LE.IGUN(JM1)) GO TO 320	E1800
PHIM1=PHI(JM1,K)	E1810
IF (K.LE.IGUN(J)) GO TO 330	E1820
PHIM0=PHI(J,K)	E1830
IF (K.LE.IGUN(JP1)) GO TO 340	E1840
PHIP1=PHI(JP1,K)	E1850
GO TO 350	E1860
320 PHIM1=PHI(JM1,K)+RWR(K)*FUN3(JM1)+FUNX(JM1)	E1870
330 PHIM0=PHI(J,K)+RWR(K)*FUN3(J)+FUNX(J)	E1880
340 PHIP1=PHI(JP1,K)+RWR(K)*FUN3(JP1)+FUNX(JP1)	E1890
IF (K.LE.IFUN(JP1)) PHIP1=PHI(JP1,K)	E1900
IF (IW.EQ.0.OR.K.GT.IFUN(JP1).OR.J.GT.JW3) GO TO 350	E1910
PHIP1=PHIP1+.5*(PHIU(JG+1,K)-PHI(JP1,K))	E1920
350 U=.5*DXR*(PHIP1-PHIM1)	E1930
IF (K.LE.IFUN(J)) U=U+FUN4(J)	E1940
ALAMB=BETASQ-GAMP1*U	E1950
IF (ALAMB.GT.0..OR.ACHKK.GT.0.) GO TO 360	E1960
SAVE=U	E1970
U=DXR*(PHIM0-PHIM1)	E1980
IF (K.LE.IFUN(J)) U=U+FUN4(J)	E1990
CHECK=BETASQ-GAMP1*U	E2000
IF (CHECK.GT.0.) U=SAVE	E2010
ALAMB=BETASQ-GAMP1*U	E2020
360 IF (ACHKK.LT.0..AND.ALAMB.GT.0.) U=DXR*(PHIM0-PHIM1)	E2030
IF (ACHKK.LT.0..AND.ALAMB.GT.0..AND.K.LE.IFUN(J)) U=U+FUN4(J)	E2040
IF (IW.EQ.0.OR.K.GT.IFUN(J).OR.J.GT.JW3) GO TO 380	E2050
UO=.5*DXR*(PHIU(JG+1,K)-PHIU(JG-1,K))-FUN4(J)	E2060
UU=DXR*(PHIU(JG,K)-PHIU(JG-1,K))-FUN4(J)	E2070
UO=UO-2.*FUN0(J)	E2080
UU=UU-2.*FUN0(J)	E2090
ALAMBO=BETASQ-GAMP1*UO	E2100
IF (ALAMBO.LT.0.) GO TO 370	E2110
ALAMBU=BETASQ-GAMP1*UU	E2120

IF (ALAMBU.LT.0.) UO=UU	E2130
GO TO 380	E2140
370 UO=UU	E2150
380 IF (K.EQ.1) GO TO 440	E2160
IF (K.EQ.KF) GO TO 450	E2170
KM1=K-1	E2180
KP1=K+1	E2190
DR1=RW(K)-RW(KM1)	E2200
DR2=RW(KP1)-RW(K)	E2210
DD1=DR1/(DR2*(DR1+DR2))	E2220
DD2=(DR2-DR1)/(DR1*DR2)	E2230
DD3=-DR2/(DR1*(DR1+DR2))	E2240
IF (K.GT.IFUN(J)) GO TO 390	E2250
V=DD1*PHI(J,KP1)+DD2*PHI(J,K)+DD3*PHI(J,KM1)	E2260
W=0.	E2270
IF (IW.EQ.0.OR.J.GT.JW3) GO TO 470	E2280
VO=DD1*PHIU(JG,KP1)+DD2*PHIU(JG,K)+DD3*PHIU(JG,KM1)	E2290
GO TO 470	E2300
390 IF (KP1.LE.IGUN(J)) GO TO 400	E2310
PHIPI=PHI(J,KP1)	E2320
IF (K.LE.IGUN(J)) GO TO 410	E2330
PHIMO=PHI(J,K)	E2340
IF (KM1.LE.IGUN(J)) GO TO 420	E2350
PHIMI=PHI(J,KM1)	E2360
GO TO 430	E2370
400 PHIPI=PHI(J,KP1)+RWR(KP1)*FUN3(J)+FUNX(J)	E2380
410 PHIMO=PHI(J,K)+RWR(K)*FUN3(J)+FUNX(J)	E2390
420 PHIMI=PHI(J,KM1)+RWR(KM1)*FUN3(J)+FUNX(J)	E2400
430 V=DD1*PHIPI+DD2*PHIMO+DD3*PHIMI	E2410
GO TO 460	E2420
440 V=(PHI(J,2)-PHI(J,1))/(RW(2)-RW(1))	E2430
IF (K.GT.IFUN(J)) GO TO 460	E2440
W=0.	E2450
IF (IW.EQ.0.OR.J.GT.JW3) GO TO 470	E2460
VO=(PHIU(JG,2)-PHIU(JG,1))/(RW(2)-RW(1))	E2470
GO TO 470	E2480
450 KM1=K-1	E2490
V=(PHI(J,K)-PHI(J,KM1))/(RW(K)-RW(KM1))	E2500
460 CSO=SQRT(ABS(1.-SNO**2))	E2510
SN2O=2.*SNO*CSO	E2520
W=(SNALP*CSO/RW(K)*FUN3(J)-.5*FUN(J)*SN2O)/RW(K)	E2530
470 CP(J)=-2.*U-V**2-W**2	E2540
IF (IW.EQ.0.OR.J.LT.JW10.OR.J.GT.JW3.OR.K.GT.IFUN(JW3)) GO TO 520	E2550

IF (K.GT.IFUN(J)) GO TO 510	E2560
CP0(J)=-2.*U0-V0**2	E2570
IF (Y2(J).LT.RW(K)) GO TO 510	E2580
IF (RW(K).LT.RMAX) GO TO 520	E2590
HB=Y2(J)+R(J)**2/Y2(J)	E2600
HBP=Y2PRM(J)*(1.-(R(J)/Y2(J))**2)+PIR/Y2(J)*SPRIME(J)	E2610
FNUM1=0.	E2620
ARG1=HB**2-(RW(K)+R(J)**2/RW(K))**2	E2621
IF (ARG1.GT.1.E-06) FNUM1=1./SQRT(ARG1)	E2622
JG=J-JW10+3	E2630
FNUM1=FNUM1*FUNAD(JG)	E2631
DUX=SNALP*(HB*HBP-(1.+(R(J)/RW(K))**2)*SPRIME(J)*PIR)*FNUM1-FUN4(J	E2640
1)	E2650
DUX=DUX+SQRT(HB**2-(RW(K)+R(J)**2/RW(K))**2)*SNALP*FUNBO(JG)	E2660
U3=U+DUX-FUNO(J)	E2670
U4=U0-DUX+FUNO(J)	E2680
DVX=-SNALP*FNUM1*(1.-(R(J)/RW(K))**2)*(RW(K)+R(J)**2/RW(K))	E2690
V3=V+DVX	E2700
V4=V0-DVX	E2710
IF (IVOR.EQ.0) GO TO 500	E2720
IF (J.GT.JCHCK) GO TO 480	E2730
DUY=SNALP*(HBP*(VLAM(JG)**2+VTAU(JG)**2)+2.*HB*(VLAM(JG)*VLAMP(JG)	E2740
1+VTAU(JG)*VTAUP(JG)))	E2750
DUY=DUY*FUNA(J)+SNALP*HB*(VLAM(JG)**2+VTAU(JG)**2)*FUNB(J)	E2760
U=U3-DUY*VTAU(JG)/(1.-VTAU(JG)**2)	E2770
U0=U4-DUY*VTAU(JG)/(1.-VTAU(JG)**2)	E2780
BNUM1=.5*(VLAM(JG)+VTAU(JG)**2/VLAM(JG))	E2790
GAN=BNUM1*HB	E2800
DGANDX=BNUM1*HBP+HB*(.5*(1.-(VTAU(JG)/VLAM(JG))**2)*VLAMP(JG)+VTAU	E2810
1(JG)/VLAM(JG)*VTAUP(JG))	E2820
DGANDX=DGANDX*FUNA(J)+GAN*FUNB(J)	E2830
GAN=GAN*FUNA(J)	E2840
GO TO 490	E2850
480 GAN=GAND	E2860
DGANDX=0.	E2870
DUY=SNALP*GAN*(((1.-VTAU(JG))/(1.-VTAU(JG))**2+VLAM(JG)**2)+1./((1	E2880
1.+VTAU(JG)))*VLAMP(JG)+VLAM(JG)*(1./((1.-VTAU(JG))**2+VLAM(JG)**2)	E2890
2-1./((1.+VTAU(JG))**2)*VTAUP(JG))	E2900
U=U3-DUY	F2910
U0=U4-DUY	E2920
490 V=V3	E2930
V0=V4	E2940
Y2N=(RW(K)+R(J)**2/PW(L))/HB	E2950



	BNUM2=SQRT(1.-Y2N**2)	E2960
	CNUM3=BNUM2-VTAU(JG)	E2970
	CNUM4=BNUM2+VTAU(JG)	E2980
	BNUM3=Y2N**2/(BNUM2*HB)*VLAM(JG)	E2990
	BNUM4=VLAM(JG)/(BNUM2*HB*RW(K))*Y2N*PIR	E3000
	DNUM3=CNUM3**2+VLAM(JG)**2	E3010
	DNUM4=CNUM4**2+VLAM(JG)**2	E3020
	ENUM3=CNUM3**2-VLAM(JG)**2	E3030
	ENUM4=CNUM4**2-VLAM(JG)**2	E3040
	ARG3=2.*VLAM(JG)*CNUM3	E3050
	ARG4=2.*VLAM(JG)*CNUM4	E3060
	THETA3=ATAN2(ARG3,ENUM3)	E3070
	THETA4=-ATAN2(ARG4,ENUM4)	E3080
	U3=U+SNALP*(THETA3*DGANDX+2.*GAN/DNUM3*(CNUM3*VLAMP(JG)-BNUM3*HBP+ 1VLAM(JG)*VTAUP(JG)+BNUM4*SPRIME(J)))	E3090 E3100
	U4=UO-SNALP*(THETA4*DGANDX+2.*GAN/DNUM4*(CNUM4*VLAMP(JG)-BNUM3*HBP 1-VLAM(JG)*VTAUP(JG)+BNUM4*SPRIME(J)))	E3110 E3120
	BNUM4=1.-(R(J)/RW(K))**2	E3130
	V3=V+2.*SNALP*Y2N*VLAM(JG)*GAN*BNUM4/(BNUM2*DNUM3)	E3140
	V4=VO-2.*SNALP*Y2N*VLAM(JG)*GAN*BNUM4/(BNUM2*DNUM3)	E3150
500	W3=-SNALP	E3160
	W4=-SNALP	E3170
	CP1(J)=-2.*(U3+SNALP*W3)-V3**2-W3**2	E3180
	CP2(J)=-2.*(U4+SNALP*W4)-V4**2-W4**2	E3190
	GO TO 520	E3200
510	CP0(J)=CP(J)	E3210
	CP1(J)=0.	E3220
	CP2(J)=0.	E3230
520	CONTINUE	E3240
	PRINT 1110, K, J1, J4, (CP(J), J=J1, J4)	E3250
	IF (IW.EQ.0.OR.K.GT.IFUN(JW3)) GO TO 530	E3260
	PRINT 1100, K, JW10, JW3, (CP0(J), J=JW10, JW3)	E3270
	IF (RW(K).LT.RMAX) GO TO 530	E3280
	PRINT 1100, K, JW10, JW3, (CP1(J), J=JW10, JW3)	E3290
	PRINT 1100, K, JW10, JW3, (CP2(J), J=JW10, JW3)	E3300
530	CONTINUE	E3310
C		E3320
C	PART 3 PERTURBATION VELOCITY POTENTIAL AT GRID POINTS	E3330
C		E3340
	PRINT 1120	E3350
	JOL=1	E3360
	JPU=JW3-JW10+4	E3370
	DO 540 K=1,KF	E3380

PRINT 1110, K, J1, J4, (PHI(J,K), J=J1, J4)	E3390
IF (IW.EQ.0.OR.K.GT.IFUN(JW3)) GO TO 540	E3400
PRINT 1100, K, JOL, JPU, (PHIU(J,K), J=1, JPU)	E3410
540 CONTINUE	E3420
C	E3430
C	E3440
C	E3450
IF (ALPHAD.EQ.0..OR.HSPAN.EQ.0.) GO TO 750	F3460
PRINT 1130	E3470
JG=JW3-JW10+3	F3480
AINI=0.	E3490
IF (IW.EQ.0) GO TO 570	E3500
K=1	E3510
AINI=-2.*(PHI(JW3,1)-PHIU(JG,1))*RW(1)	E3520
550 K=K+1	E3530
IF (K.GT.IFUN(JW3)) GO TO 560	E3540
AINI=-(PHI(JW3,K)+PHI(JW3,K-1)-PHIU(JG,K)-PHIU(JG,K-1))*(RW(K)-RW(	E3550
1 K-1))+AINI	E3560
GO TO 550	E3570
560 AINI=AINI-(PHI(JW3,K-1)-PHIU(JG,K-1))*(Y2(JW3)-RW(K-1))	E3580
570 AINI=-AINI	E3590
ALA=SNALP/PIR*((Y2(JW3)-R(JW3)**2/Y2(JW3))**2*FUNAO(JW3-JW10+3)+R(	E3600
1 JW3)**2)+AINI	E3601
IF (IVOR.EQ.0) GO TO 590	E3610
IF (JCHCK.LT.JW3) GO TO 580	E3620
ALS=ALA+SNALP/PIR*2.*(VLAM(JG)**2+VTAU(JG)**2)*(Y2(JW3)+R(JW3)**2/	E3630
1 Y2(JW3))**2*FUNA(J)	E3640
GO TO 600	E3650
580 ALS=ALA+SNALP/PIR*4.*GAND*VLAM(JG)*(Y2(JW3)+R(JW3)**2/Y2(JW3))	E3660
GO TO 600	E3670
590 ALS=ALA	E3680
600 ALANS=ALA-AINI	E3690
ALSNS=ALS-AINI	E3700
AINI0=AINI	E3710
SMA=ALS-ALA	E3720
CP(J2)=0.	E3730
CPO(J2)=0.	E3740
CP1(J2)=0.	E3750
CP2(J2)=0.	E3760
JW10M1=JW10-1	E3770
J2P1=J2+1	E3780
IF (JW10M1.LE.J2) GO TO 620	E3790
DO 610 J=J2P1, JW10M1	E3800

CP(J)=SNALP*SPRIME(J)	E3810
CP1(J)=CP(J)	E3820
CP2(J)=CP(J)	E3830
610 CPO(J)=CP(J)	E3840
620 DO 700 J=JW10,JW3	E3850
AINT=0.	E3860
JG=J-JW10+3	E3870
IF (IW.EQ.0) GO TO 650	E3880
IF (IFUN(J).EQ.0) GO TO 660	E3890
K=1	E3900
AINT=-(PHI(J+1,1)-PHI(J-1,1)-PHIU(JG+1,1)+PHIU(JG-1,1))*DXR*RW(1)	E3910
630 K=K+1	E3920
IF (K.GT.IFUN(J)) GO TO 640	E3930
AINT=AINT-.5*DXR*(PHI(J+1,K)-PHI(J-1,K)+PHI(J+1,K-1)-PHI(J-1,K-1)-	E3940
1PHIU(JG+1,K)+PHIU(JG-1,K)-PHIU(JG+1,K-1)+PHIU(JG-1,K-1))*(RW(K)-RW	E3950
2(K-1))	E3960
GO TO 630	E3970
640 AINT=AINT-.5*DXR*(PHI(J+1,K-1)-PHI(J-1,K-1)-PHIU(JG+1,K-1)+PHIU(JG	E3980
1-1,K-1))*(Y2(J)-RW(K-1))	E3990
650 AINT=-AINT	E4000
660 Y2P=Y2PRM(J)	E4010
JG=J-JW10+3	E4011
CP(J)=SNALP*(2.*((1.-(R(J)/Y2(J))**4)*Y2(J)*Y2P/PIR-2.*((1.-(R(J)/Y	E4020
12(J))**2)*SPRIME(J))*FUNAO(JG)+(Y2(J)-R(J)**2/Y2(J))**2/PIR*FUNBO(	E4030
2JG)+SPRIME(J))	E4040
IF (J.GE.JW20) CP(J)=.85*CP(J)*SQRT(ABS((Y2(J)-Y1(J))/(Y2(J)+Y1(J)	E4060
1)))	E4070
CP(J)=CP(J)+AINT	E4080
HB=Y2(J)+R(J)**2/Y2(J)	E4090
HBP=Y2P*(1.-(R(J)/Y2(J))**2)+PIR/Y2(J)*SPRIME(J)	E4100
IF (IVOR.EQ.0) GO TO 680	E4110
IF (J.GT.JCHCK) GO TO 670	E4120
CPO(J)=CP(J)+4./PIR*SNALP*HB*(HB*(VLAM(JG)*VLAMP(JG)+VTAU(JG)*VTAU	E4130
1P(JG))+HBP*(VLAM(JG)**2+VTAU(JG)**2)*FUNA(J)+2./PIR*SNALP*HB**2*(	E4140
2VLAM(JG)**2+VTAU(JG)**2)*FUNB(J)	E4150
GO TO 690	E4160
670 CPO(J)=CP(J)+4./PIR*SNALP*GAND*(HB*VLAMP(JG)+VLAM(JG)*HBP)	E4170
GO TO 690	E4180
680 CPO(J)=CP(J)	E4190
690 CP1(J)=CP(J)-AINT	E4200
CP2(J)=CPO(J)-AINT	E4210
DCP=CPO(J)-CP(J)	E4220
700 PRINT 1060, J,CP(J),CPO(J),CP1(J),CP2(J),AINT,DCP	E4230

AMA=0.	E4240
AMS=0.	E4250
AMANS=0.	E4260
AMSNS=0.	E4270
DO 710 J=J2P1,JW3	E4280
AMA=AMA+.5*(CP(J)+CP(J-1))*(XW(J)-.5*DX)*DX	E4290
AMANS=AMANS+.5*(CP1(J)+CP1(J-1))*(XW(J)-.5*DX)*DX	E4300
AMSNS=AMSNS+.5*(CP2(J)+CP2(J-1))*(XW(J)-.5*DX)*DX	E4310
710 AMS=AMS+.5*(CPO(J)+CPO(J-1))*(XW(J)-.5*DX)*DX	E4320
IF (JW2.EQ.JW3) GO TO 730	E4330
DLO=SNALP/PIR*((Y2(JW20)-R(JW20)**2/Y2(JW20))**2+R(JW20)**2-(Y2(JW	E4340
13)-R(JW3)**2/Y2(JW3))**2-R(JW3)**2)	E4350
DO 720 J=JW20,JW3M1	E4360
720 DLO=DLO+.5*DX*(CP1(J)+CP1(J+1))	E4370
ALA=ALA+DLO	E4380
ALS=ALS+DLO	E4390
ALANS=ALANS+DLO	E4400
ALSNS=ALSNS+DLO	E4410
730 XBARA=AMA/ALA	E4420
XBARS=AMS/ALS	E4430
XBARAN=AMANS/ALANS	E4440
XBARSN=AMSNS/ALSNS	E4450
AREA=0.	E4460
JW1P1=JW1+1	E4470
DO 740 J=JW1P1,JW3	E4480
AREA=AREA+.5*DX*(Y2(J)+Y2(J-1)-R(J)-R(J-1))	E4490
IF (J.LE.JW20) GO TO 740	E4500
AREA=AREA-.5*DX*(Y1(J)+Y1(J-1))	E4510
740 CONTINUE	E4520
AREA=2.*AREA	E4530
IF (HSPAN.LE.RMAX) AREA=RMAX**2/PIR	E4540
ARR=2./AREA	E4550
CLA=ALA*ARR	E4560
CLS=ALS*ARR	E4570
CLANS=ALANS*ARR	E4580
CLSNS=ALSNS*ARR	E4590
CAINTO=AINTO*ARR	E4600
CSMA=SMA*ARR	E4610
CMA=AMA*ARR	E4620
CMS=AMS*ARR	E4630
CMANS=AMANS*ARR	E4640
CMSNS=AMSNS*ARR	F4650
PRINT 1140, ALA,ALS,AMA	E4660

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PRINT 1150, AMS,XBARA,XBARS,ALANS,ALSNS,AMANS,AMSNS,XBARAN,XBARSN,
1 AINTJ
PRINT 1160, SMA,CLA,CLS,CLANS,CLSNS,CAINTO,CSMA,CMA,CMS,CMANS
PRINT 1170, CMSNS,AREA

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# PART 5 BODY SURFACE PRESSURE COEFFICIENTS

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PRINT 1180
IF (ABS(SNALP).LT.1.E-06) GO TO 770
IF (ABS(OMEGAD).GT.1.E-06) GO TO 760
PRINT 1190
IF (IVOR.EQ.0) GO TO 750
PRINT 1200
GO TO 780
750 PRINT 1210
GO TO 780
760 CHK=SNO-1.
IF (ABS(CHK).LT.1.E-06) PRINT 1220
CHK=1.+SNO
IF (ABS(CHK).LT.1.E-06) PRINT 1230
IF (IVOR.EQ.0) GO TO 770
PRINT 1240
PRINT 1250
GO TO 780
770 PRINT 1260
780 J2P1=J2+1
J3M1=J3-1
ALAMB=1.
K=1
DO 1030 J=J2P1,J3M1
JP1=J+1
JM1=J-1
JM2=J-2
JM3=J-3
JG=J-JW10+3
ACHKK=ALAMB
ALAMB=BETASQ-.5*GP1DXR*(PHI(JP1,K)-PHI(JM1,K))-GAMP1*FUN4(J)
IF (ALAMB.LE.0) GO TO 790
AA=.5*PIR*ALOG(R(J)/RW(K))
PHI1=PHI(JM1,K)+AA*SPRIME(JM1)
IF (J.EQ.JS.AND.ABS(R(J)-R(J-1)).LT.1.E-06) PHI1=PHI(JM1,K)
PHI1=PHI(JP1,K)+AA*SPRIME(JP1)
U=.5*DXR*(PHI1-PHI1)

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E4670  
E4680  
E4690  
E4700  
E4710  
E4720  
E4730  
E4740  
E4750  
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E4980  
E4990  
E5000  
E5010  
E5011  
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E5040  
E5050  
E5060  
E5070  
E5080  
E5090

IF (ACHKK.GE.0.) GO TO 800	E5100
PHIMO=PHI(J,1)+AA*SPRIME(J)	E5110
U=DXR*(PHIMO-PHIM1)	E5120
GO TO 800	E5130
790 ALAMB=BETASQ-GP1DXR*(PHI(J,K)-PHI(JM1,K))-GAMP1*FUN4(J)	E5140
AA=.5*PIR*ALOG(R(J)/RW(K))	E5150
PHIMO=PHI(J,K)+AA*SPRIME(J)	F5160
PHIM1=PHI(JM1,K)+AA*SPRIME(JM1)	E5170
PHIM2=PHI(JM2,K)+AA*SPRIME(JM2)	E5180
U=.5*DXR*(3.*PHIMO-4.*PHIM1+PHIM2)	E5190
IF (J.NE.JS.OR.ABS(R(J)-R(JM1)).GE.1.E-06) GO TO 800	E5200
PHIM1=PHI(JM1,K)	E5210
U=DXR*(PHIMO-PHIM1)	E5220
800 V=.5*DXR*(R(JP1)-R(JM1))	E5230
IF (IW.EQ.0) GO TO 850	E5240
IF (J.LT.JW10.OR.J.GT.JW3) GO TO 850	E5250
IF (J.GT.JW10) GO TO 810	E5260
ACHKK=ALAMB	E5270
GO TO 820	E5280
810 ACHKK=ALAMBU	E5290
820 JGM1=JG-1	E5310
JGP1=JG+1	E5320
JGM2=JG-2	F5330
ALAMBU=BETASQ-.5*GP1DXR*(PHIU(JGP1,K)-PHIU(JGM1,K))+GAMP1*FUN4(J)	E5340
PHIM1=PHIU(JGM1,K)+AA*SPRIME(JM1)	E5350
IF (ALAMBU.LE.0.) GO TO 840	E5360
IF (ACHKK.LT.0.) GO TO 830	E5370
PHIP1=PHIU(JGP1,K)+AA*SPRIME(JP1)	E5380
UO=.5*DXR*(PHIP1-PHIM1)	E5390
GO TO 860	E5400
830 PHIMO=PHIU(JG,K)+AA*SPRIME(J)	E5410
UO=DXR*(PHIMO-PHIM1)	E5420
GO TO 860	E5430
840 ALAMBU=BETASQ-.5*GP1DXR*(PHIU(JG,K)-PHIU(JGM2,K))-GAMP1*FUN4(J)	E5440
PHIMO=PHIU(JG,K)+AA*SPRIME(J)	E5450
PHIM2=PHIU(JGM2,K)+AA*SPRIME(JM2)	E5460
UO=.5*DXR*(3.*PHIMO-4.*PHIM1+PHIM2)	E5470
GO TO 860	E5480
850 UO=U	E5490
ALAMBU=ALAMB	E5500
860 IF (IVOR.EQ.0.OR.J.LT.JW10.OR.J.GT.JW2) GO TO 880	E5510
IF (J.GT.JCHCK) GO TO 870	E5520
HB=Y2(J)+R(J)**2/Y2(J)	E5530

HBP=(1.-(R(J)/Y2(J))**2)*Y2PRM(J)+PIR*SPRIME(J)/Y2(J)	E 5540
FUNO(J)=FUNO(J)+SNALP*(HBP*(VLAM(JG)**2+VTAU(JG)**2)+2.*HB*(VLAM(J	E 5550
1G)*VLAMP(JG)+VTAU(JG)*VTAUP(JG)))/(1.-VTAU(JG)**2)*VTAU(JG)*FUNA(J	E 5560
2)+SNALP*HB*(VLAM(JG)**2+VTAU(JG)**2)/(1.-VTAU(JG)**2)*VTAU(JG)*FUN	E 5570
3B(J)	E 5580
GO TO 880	E 5590
870 FUNO(J)=FUNO(J)+SNALP*GAN*(((1.-VTAU(JG))/(1.-VTAU(JG))**2+VLAM(J	E 5600
1G)**2)+1./(1.+VTAU(JG))*VLAMP(JG)+VLAM(JG)*(1./((1.-VTAU(JG))**2+	E 5610
2VLAM(JG)**2)-1./(1.+VTAU(JG))**2)*VTAUP(JG))	E 5620
880 UO=UO-FUNO(J)	E 5630
U=U-FUNO(J)	E 5640
DRDX=.5*DXR*(R(JP1)-R(JM1))	E 5650
ROY2J=1.	E 5660
IF (Y2(J).GT.R(J).AND.J.NE.J2) ROY2J=R(J)/Y2(J)	E 5670
UU=SNALP*(2.*ROY2J*DRDX/(1.-ROY2J**2)*Y2PRM(J))	E 5680
IF (J.GT.JW2.AND.J.LE.JW3) UU= 2.*SNALP*ROY2J*DRDX	E 5681
Y2JO=R(J)	E 5690
IF (Y2(J).GT.R(J)) Y2JO=Y2(J)	E 5700
UU=UU*FUNA(J)+SNALP*Y2JO*(1.+ROY2J**2)*FUNB(J)	E 5710
IF (IWING.LT.0.AND.J.GT.JMCK.AND.J.LE.JW3) UU=UU90D(JG)*SQRT(1.+DR	E 5711
1DX**2*4.)	E 5712
U1=U+UU	E 5720
U2=UO-UU	E 5730
V1=V-SNALP	E 5740
V2=V+SNALP	E 5750
IF (J.LT.JW10) GO TO 890	E 5760
UU=SNALP*(-2.*ROY2J*DRDX+(1.+ROY2J**2)*Y2PRM(J))	E 5770
IF (J.GT.JW2.AND.J.LE.JW3) UU=-2.*SNALP*ROY2J*DRDX	E 5771
UU=UU*FUNA(J)+SNALP*Y2JO*(1.-ROY2J**2)*FUNB(J)	E 5780
IF (IWING.LT.0.AND.J.GT.JMCK.AND.J.LE.JW3) UU=UUOD(JG)	E 5781
U3=U+UU	E 5790
U4=UO-UU	E 5800
W3=-SNALP	E 5810
W4=-SNALP	E 5820
GO TO 900	E 5850
890 U3=U	E 5860
U4=UO	E 5870
W3=SNALP	E 5880
W4=SNALP	E 5890
900 V3=V	E 5920
V4=V	E 5930
IF (ABS(SNALP).LT.1.E-06) GO TO 990	E 5940
IF I G=0	E 5950

IF (ABS(OMEGAD).GT.1.E-06) GO TO 950	E5960
CP(J)=-2.*(U3+SNALP*W3)-V3**2-W3**2	E5970
CPO(J)=-2.*(U4+SNALP*W4)-V4**2-W4**2	E5980
CP1(J)=-2.*(U1+SNALP*V1)-V1**2	E5990
CP2(J)=-2.*(U2+SNALP*V2)-V2**2	E6000
IF (J.GF.JW10.AND.J.LE.JW2) GO TO 910	E6010
PRINT 1060, J,CP(J),CPO(J),CP1(J),CP2(J)	E6020
GO TO 1030	E6030
910 IF (IVOR.EQ.0) GO TO 1010	E6040
CPX=CP(J)	E6050
CPOX=CPO(J)	E6060
CP1X=CP1(J)	E6070
CP2X=CP2(J)	E6080
920 HB=Y2(J)+R(J)**2/Y2(J)	E6090
HBP=Y2PRM(J)*(1.-(R(J)/Y2(J))**2)+PIR/Y2(J)*SPRIME(J)	E6100
L=JG	E6110
BNUM1=.5*(VLAM(L)+VTAU(L)**2/VLAM(L))	E6120
IF (J.GT.JCHCK) GO TO 930	E6130
GAN=BNUM1*HB	E6140
DGANDX=BNUM1*HBP+HB*(.5*(1.-(VTAU(L)/VLAM(L))**2)*VLAMP(L)+VTAU(L)	E6150
1/VLAM(L)*VTAU(L))	E6160
DGANDX=DGANDX*FUNA(J)+GAN*FUNB(J)	E6170
GAN=GAN*FUNA(J)	E6180
GO TO 940	E6190
930 GAN=GAND	E6200
DGANDX=0.	E6210
940 Y2N=2.*R(J)/HB	E6220
CNUM1=1.-VTAU(L)	E6230
CNUM2=1.+VTAU(L)	E6240
BNUM2=SQRT(1.-Y2N**2)	E6250
CNUM3=BNUM2-VTAU(L)	E6260
CNUM4=BNUM2+VTAU(L)	E6270
BNUM3=Y2N**2/(BNUM2*HB)*VLAM(L)	E6280
BNUM4=2.*VLAM(L)/(BNUM2*HB**2)*PIR	E6290
DNUM1=CNUM1**2+VLAM(L)**2	E6300
DNUM2=CNUM2**2+VLAM(L)**2	E6310
DNUM3=CNUM3**2+VLAM(L)**2	E6320
DNUM4=CNUM4**2+VLAM(L)**2	E6330
ENUM1=CNUM1**2-VLAM(L)**2	E6340
ENUM2=CNUM2**2-VLAM(L)**2	E6350
ENUM3=CNUM3**2-VLAM(L)**2	E6360
ENUM4=CNUM4**2-VLAM(L)**2	E6370
ARG1=2.*VLAM(L)*CNUM1	E6380



ARG2=2.*VLAM(L)*CNUM2	E6390
ARG3=2.*VLAM(L)*CNUM3	E6400
ARG4=2.*VLAM(L)*CNUM4	E6410
THETA1=ATAN2(ARG1,ENUM1)	E6420
THETA2=-ATAN2(ARG2,ENUM2)	E6430
THETA3=ATAN2(ARG3,ENUM3)	E6440
THETA4=-ATAN2(ARG4,ENUM4)	E6450
U1=U1+SNALP*(THETA1*DGANDX+2.*GAN/DNUM1*(CNUM1*VLAMP(L)+VLAM(L)*VT	E6460
1AUP(L)))	E6470
U2=U2-SNALP*(THETA2*DGANDX+2.*GAN/DNUM2*(CNUM2*VLAMP(L)-VLAM(L)*VT	E6480
1AUP(L)))	E6490
U3=U3+SNALP*(THETA3*DGANDX+2.*GAN/DNUM3*(CNUM3*VLAMP(L)-BNUM3*HBP+	E6500
1VLAM(L)*VTAUP(L)+BNUM4*SPRIME(J)))	E6510
U4=U4-SNALP*(THETA4*DGANDX+2.*GAN/DNUM4*(CNUM4*VLAMP(L)-BNUM3*HBP-	E6520
1VLAM(L)*VTAUP(L)+BNUM4*SPRIME(J)))	E6530
IF (ABS(OMEGAD).GT.1.E-06) GO TO 950	E6540
CP(J)=-2.*(U3+SNALP*W3)-V3**2-W3**2	E6550
CPO(J)=-2.*(U4+SNALP*W4)-V4**2-W4**2	E6560
CP1(J)=-2.*(U1+SNALP*V1)-V1**2	E6570
CP2(J)=-2.*(U2-SNALP*V2)-V2**2	E6580
PRINT 1060, J,CP(J),CPO(J),CP1(J),CP2(J),CPX,CPOX,CP1X,CP2X	E6590
GO TO 1030	E6600
950 CHK=SNO+1.	E6610
IF (ABS(CHK).GT.1.E-06) GO TO 970	E6620
CP(J)=-2.*(U2-SNALP*V2)-V2**2	E6630
IF (J.GE.JW10.AND.J.LE.JW2) GO TO 960	E6640
GO TO 1000	E6650
960 IF (IVOR.EQ.0) GO TO 1000	E6660
IF (IFLG.EQ.1) GO TO 1020	E6670
IFLG=1	E6680
CPX=CP(J)	E6690
GO TO 920	E6700
970 CHK=SNO-1.	E6710
IF (ABS(CHK).GT.1.E-06) GO TO 990	E6720
CP(J)=-2.*(U1+SNALP*V1)-V1**2	E6730
IF (J.GE.JW10.AND.J.LE.JW2) GO TO 980	E6740
GO TO 1000	E6750
980 IF (IVOR.EQ.0) GO TO 1000	E6760
IF (IFLG.EQ.1) GO TO 1020	E6770
IFLG=1	E6780
CPX=CP(J)	E6790
GO TO 920	E6800
990 CP(J)=-2.*U-V**2	E6810

1000	PRINT 1060, J,CP(J)	E6820
	GO TO 1030	E6830
1010	PRINT 1060, J,CP(J),CPO(J),CP1(J),CP2(J)	E6840
	GO TO 1030	E6850
1020	PRINT 1060, J,CP(J),CPX	E6860
1030	CONTINUE	E6870
	IF (ABS(AMINF).LT.1.E-08) AMINF=1.E-08	E6871
	CPSTAR=2.*(1.-SQRT(((GAMMA-1.)*AMINF**2+2.)/(GAMMA+1.))/AMINF)	E6880
	PRINT 1270, CPSTAR	E6890
C		E6900
C	PART 6 REMOTE TERMINAL OUTPUT	E6910
C		E6920
	BLK3=10HCP(J)	E6930
	WRITE (7,1280) BLK3,J2P1,J3M1,I,(CP(J),J=J2P1,J3M1)	E6940
	BLK4=10HCPO(J)	E6950
	IF (IW.EQ.1) WRITE (7,1280) BLK4,J2P1,J3M1,I,(CPO(J),J=J2P1,J3M1)	E6960
	WRITE (7,1290) DPHIMX	E6970
		E6980
C		E6990
C	PART 7 WAVE DRAG	E7000
C		E7010
	DRAG=0.	E7020
	J2P2=J2+2	E7030
	J3M3=J3-3	E7040
	DO 1050 J=J2P2,J3M3	E7050
	JP1=J+1	E7060
	IF (IW.EQ.0) GO TO 1040	E7070
	DRAG=DRAG+.39269908*(CP(J)+CP(JP1)+CPO(J)+CPO(JP1))*(R(J)+R(JP1))*	E7080
	1(R(JP1)-R(J))	E7090
	GO TO 1050	E7100
1040	DRAG=DRAG+.78539816*(CP(J)+CP(JP1))*(R(J)+R(JP1))*(R(JP1)-R(J))	E7110
1050	CONTINUE	E7120
	IF (IW.EQ.0) DRAG=DRAG+1.57079632*(CP(J2P1)*R(J2P2)**2+CP(J3M1)*(R	E7130
	1(J3)**2-R(J3-2)**2))	E7140
	IF (IW.EQ.1) DRAG=DRAG+.78539816*((CP(J2P1)+CPO(J2P1))*R(J2P2)**2+	E7150
	1(CP(J3M1)+CPO(J3M1))*(R(J3)**2-R(J3-2)**2))	E7160
	PRINT 1300, DRAG	E7170
		E7180
C		E7190
C	PART 8 PLOTTING INPUT	E7200
C		E7210
	WRITE (1) IWALL,J1,J2,J3,J4,JW10,JW20,JW2,JW3,KM,CPSTAR,AMINF,RMAX	E7220
	1,HSPAN,SNALP,SNO,SFACTOR	E7230
	WRITE (1) CPO,XW,RW,Y1,Y2,R,SLAS,CP,CP1,CP2	
	RETURN	

C

1060	FORMAT (I4,8E16.8)	E7240
1070	FORMAT (18H SUBROUTINE RESULT////36H SHOCK WAVE AND SONIC LINE LOCATIONS//3X,1HJ,6X,5HXW(J),9X,9HSLAS(J,1),7X,9HSLAS(J,2),7X,9HSLAS(J,3),7X,9HSLAS(J,4),7X,9HSLAS(J,5),7X,9HSLAS(J,6))	E7250
1080	FORMAT (I4,7E16.8)	E7260
1090	FORMAT (///38H PRESSURE COEFFICIENTS AT GRID POINTS /51H 1 GENERAL 1AL POINTS ( COMPUTATIONAL APPROXIMATION )/54H 2 POINTS UNDER WING 2G ( COMPUTATIONAL APPROXIMATION )/23H 3 POINTS ABOVE WING /22H 3 4 POINTS UNDER WING)	E7270
1100	FORMAT (/3I5/(8E16.8))	E7280
1110	FORMAT (/3I5/(8E16.8))	E7290
1120	FORMAT (///34H VELOCITY POTENTIAL AT GRID POINTS/19H 1 GENERAL P 10INTS/22H 2 POINTS UNDER WING)	E7300
1130	FORMAT (///24H AXIAL LIFT DISTRIBUTION/37H CP(J) = LIFT MINUS VORTEX EFFECT /16H CPO(J) = LIFT/52H CP1(J) = LIFT MINUS THICKNESS AND VORTEX EFFECTS /39H CP2(J) = LIFT MINUS THICKNESS EFFECT 3/28H AINT = THICKNESS EFFECT/26H DCP = VORTEX EFFECT //3X 4,1HJ,6X,5HCP(J),11X,6HCPO(J),10X,6HCP1(J),10X,6HCP2(J),11X,4HAINT,513X,3HDCP/)	E7310
1140	FORMAT (///16H LIFT AND MOMENT/59H AL = LIFT, AM = MOMENT, X 1BAR = MOMENT ARM ABOUT NOSE/45H A = ATTACHED FLOW, S = SEPARATED FLOW/25H NS = NEGLECT SHOCK/42H AINTO = SHOCK LIFT 3, SMA = VORTEX LIFT/29H AREA = EXPOSED WING AREA/46H 4 OR MAXIMUM CROSS-SECTIONAL AREA//11H ALA =,E16.8//11H 5 ALS =,E16.8//11H AMA =,E16.8//11H	E7320
1150	FORMAT (11H AMS =,E16.8//11H XBARA =,E16.8//11H XBARS = 1,E16.8//11H ALANS =,E16.8//11H ALSNS =,E16.8//11H AMANS = 2,E16.8//11H AMSNS =,E16.8//11H XBARAN =,E16.8//11H XBARSN = 3,E16.8//11H AINTO =,E16.8//11H	E7330
1160	FORMAT (11H SMA =,E16.8//11H CLA =,E16.8//11H CLS = 1,E16.8//11H CLANS =,E16.8//11H CLSNS =,E16.8//11H CAINTO = 2,E16.8//11H CSMA =,E16.8//11H CMA =,E16.8//11H CMS = 3,E16.8//11H CMANS =,E16.8//11H	E7340
1170	FORMAT (11H CMSNS =,E16.8//11H AREA =,E16.8)	E7350
1180	FORMAT (///36H BODY SURFACE PRESSURE COEFFICIENTS )	E7360
1190	FORMAT (48H CP(J) - OMEGA = +0 DEGREES ( LEEWARD SIDE )/49H 1CPO(J) - OMEGA = -0 DEGREES ( WINDWARD SIDE )/32H CP1(J) - OMEGA = +90 DEGREES /32H CP2(J) - OMEGA = -90 DEGREES )	E7370
1200	FORMAT (53H CPX,CPOX,CPIX AND CP2X - VORTEX EFFECTS NEGLECTED // 1/3X,1HJ,7X,5HCP(J),10X,6HCPO(J),9X,6HCP1(J),10X,6HCP2(J),13X,3HCPX 2,13X,4HCPOX,12X,4HCP1X,12X,4HCP2X/)	E7380
1210	FORMAT (/3X,1HJ,7X,5HCP(J),10X,6HCPO(J),9X,6HCP1(J),10X,6HCP2(J)/	E7390
		E7400
		E7410
		E7420
		E7430
		E7440
		E7450
		E7460
		E7470
		E7480
		E7490
		E7500
		E7510
		E7520
		E7530
		E7540
		E7550
		E7560
		E7570
		E7580
		E7590
		E7600
		E7610
		E7620
		E7630
		E7640
		E7650
		E7660

1)  
1220 FORMAT (32H CP(J) - OMEGA = +90 DEGREES )  
1230 FORMAT (32H CP(J) - OMEGA = -90 DEGREES )  
1240 FORMAT (34H CPX -VORTEX EFFECTS NEGLECTED )  
1250 FORMAT (/3X,1HJ,7X,5HCP(J),10X,3HCPX/)  
1260 FORMAT (/3X,1HJ,7X,5HCP(J)/)  
1270 FORMAT (/8H CPSTAR=,E16.8)  
1280 FORMAT (1X1A10,3I5/(7E16.8))  
1290 FORMAT (8H DPHIMX=E16.8)  
1300 FORMAT (/6H DRAG=E16.8/)  
END

E7670  
E7680  
E7690  
E7700  
E7710  
E7720  
E7730  
E7740  
E7750  
E7760  
E7770-

OVERLAY (DICK,2,0)	F	0
PROGRAM TWO0	F	10
DIMENSION CPO(120), XW(120), RW(100), Y1(120), Y2(120), R(120), SL	F	20
1AS(120,6), CP(120), CP1(120), CP2(120)	F	30
DIMENSION TMP1(200), TMP2(200), TMP3(200)	F	40
DIMENSION NAME(6), LBLE1(8), LBLE2(8)	F	50
DATA NAME/3HM =,3HF =,3HH =,7HALPHA =,7HOMEGA =,4HDEG./	F	60
COMMON /CALLP/ NREAD,NCASES	F	70
YTIC=-1.	F	80
XTIC=-1.	F	90
YDV=10.	F	100
XDV=10.	F	110
NREAD=NREAD+1	F	120
REWIND 1	F	130
RAD=57.29577951	F	140
READ (1) IWALL,J1,J2,J3,J4,JW10,JW20,JW2,JW3,KM,CPSTAR,AMINF,RMAX,	F	150
1HSPAN,SNALP,SNO,SFACTOR	F	160
READ (1) CPO,XW,RW,Y1,Y2,R,SLAS,CP,CP1,CP2	F	170
F=.5/RMAX	F	180
ALPHA=ASIN(SNALP)	F	190
ALPHA=ALPHA*RAD	F	200
J2P1=J2+1	F	210
J3M1=J3-1	F	220
IF (ABS(ALPHA).LT.1.E-08) ALPHA=0.	F	230
OMEGA=ASIN(SNO)	F	240
OMEGA=OMEGA*RAD	F	250
CALL PSEUDO	F	260
CALL LEROY	F	270
CALL CALPLT (2.,2.5,-3)	F	280
YSHIFT=1.0	F	290
IF (SNO.LT.-1.E-06) YSHIFT=7.5	F	300
CALL CALPLT (0.,YSHIFT,-3)	F	310
ENCODE (30,240,LBLE1(1) )NAME(1),AMINF,NAME(2),F,NAME(3),HSPAN	F	320
ENCODE (40,250,LBLE2(1) )NAME(4),ALPHA,NAME(6),NAME(5),OMEGA,NAME(	F	330
16)	F	340
	F	350
FIGURE 1 - PLOT BODY	F	360
	F	370
NCOUNT=0	F	380
DO 10 J=J2,J3	F	390
NCOUNT=NCOUNT+1	F	400
TMP1(NCOUNT)=XW(J)	F	410

C  
C  
C

```

      TMP2(NCOUNT)=R(J)
      TMP3(NCOUNT)=-R(J)
10  CONTINUE
      TMP1(NCOUNT+1)=TMP1(1)
      TMP2(NCOUNT+1)=TMP1(NCOUNT+1)
      TMP3(NCOUNT+1)=TMP1(NCOUNT+1)
      TMP1(NCOUNT+2)=SFACTOR
      TMP2(NCOUNT+2)=TMP1(NCOUNT+2)
      TMP3(NCOUNT+2)=TMP1(NCOUNT+2)
      CALL LINE (TMP1,TMP2,NCOUNT,1,+0,3,.07)
      CALL LINE (TMP1,TMP3,NCOUNT,1,+0,3,.07)
      IF (HSPAN.LT.RMAX) GO TO 80
      IF (ABS(SNO).LT.1.E-06) GO TO 20
      GO TO 80

```

```

C
C  FIGURE 1 - PLOT  Y2(J)  VERSUS  XW(J)
C

```

```

20  NCOUNT=0
      DO 30 J=JW10,JW3
      NCOUNT=NCOUNT+1
      TMP1(NCOUNT)=XW(J)
      TMP2(NCOUNT)=Y2(J)
30  CONTINUE
      TMP1(NCOUNT+1)=0.
      TMP2(NCOUNT+1)=TMP1(NCOUNT+1)
      TMP3(NCOUNT+1)=TMP1(NCOUNT+1)
      TMP1(NCOUNT+2)=SFACTOR
      TMP2(NCOUNT+2)=TMP1(NCOUNT+2)
      TMP3(NCOUNT+2)=TMP1(NCOUNT+2)
      CALL LINE (TMP1,TMP2,NCOUNT,1,+0,3,.07)
      DO 40 J=1,NCOUNT
40  TMP2(J)=-TMP2(J)
      CALL LINE (TMP1,TMP2,NCOUNT,1,+0,3,.07)
      IF (JW3.GT.JW2) GO TO 50

```

```

C
C  DRAW LINE IF  JW2=JW3
C

```

```

      TMP1(1)=XW(JW3)/SFACTOR
      TMP2(1)=Y2(JW3)/SFACTOR
      TMP1(2)=XW(JW3)/SFACTOR
      TMP2(2)=R(JW3)/SFACTOR
      CALL DRAW (TMP1,TMP2,2)
      TMP2(1)=-TMP2(1)

```

```

F 420
F 430
F 440
F 450
F 460
F 470
F 480
F 490
F 500
F 510
F 520
F 530
F 540
F 550
F 560
F 570
F 580
F 590
F 600
F 610
F 620
F 630
F 640
F 650
F 660
F 670
F 680
F 690
F 700
F 710
F 720
F 730
F 740
F 750
F 760
F 770
F 780
F 790
F 800
F 810
F 820
F 830
F 840

```

	TMP2(2)=-TMP2(2)	F 850
	CALL DRAW (TMP1,TMP2,2)	F 860
	GO TO 80	F 870
C		F 880
C	PLOT Y1(J) VERSUS XW(J)	F 890
C		F 900
	50 NCOUNT=0	F 910
	DO 60 J=JW20,JW3	F 920
	NCOUNT=NCOUNT+1	F 930
	TMP1(NCOUNT)=XW(J)	F 940
	TMP2(NCOUNT)=Y1(J)	F 950
	60 CONTINUE	F 960
	TMP1(NCOUNT+1)=0.	F 970
	TMP2(NCOUNT+1)=TMP1(NCOUNT+1)	F 980
	TMP3(NCOUNT+1)=TMP1(NCOUNT+1)	F 990
	TMP1(NCOUNT+2)=SFACTOR	F1000
	TMP2(NCOUNT+2)=TMP1(NCOUNT+2)	F1010
	TMP3(NCOUNT+2)=TMP1(NCOUNT+2)	F1020
	CALL LINE (TMP1,TMP2,NCOUNT,1,+0.3,.07)	F1030
	DO 70 J=1,NCOUNT	F1040
	70 TMP2(J)=-TMP2(J)	F1050
	CALL LINE (TMP1,TMP2,NCOUNT,1,+0.3,.07)	F1060
C		F1070
C	FIGURE 1 - PLOT SLAS(J,1) VERSUS XW(J)	F1080
C		F1090
	80 DO 120 II=1,6	F1110
	NCOUNT=0	F1120
	DO 90 J=J1,J4	F1130
	IF (SLAS(J,II).LE.0.) GO TO 90	F1140
	IF (SLAS(J,II).GT.YSHIFT.AND.SNO.LT.-1.E-06) GO TO 90	F1141
	NCOUNT=NCOUNT+1	F1150
	TMP1(NCOUNT)=XW(J)	F1160
	TMP2(NCOUNT)=SLAS(J,II)	F1170
	90 CONTINUE	F1190
	TMP1(NCOUNT+1)=0.	F1200
	TMP2(NCOUNT+1)=TMP1(NCOUNT+1)	F1210
	TMP3(NCOUNT+1)=TMP1(NCOUNT+1)	F1220
	TMP1(NCOUNT+2)=SFACTOR	F1230
	TMP2(NCOUNT+2)=TMP1(NCOUNT+2)	F1240
	TMP3(NCOUNT+2)=TMP1(NCOUNT+2)	F1250
	IF (SNO.GT.-1.E-06) GO TO 110	F1260
	DO 100 J=1,NCOUNT	F1270
	100 TMP2(J)=-TMP2(J)	F1280

```

110 IF (NCOUNT.EQ.0) GO TO 130
    CALL LINE (TMP1,TMP2,NCOUNT,1,-1.4,.07)
120 CONTINUE

```

```

C
130 YSHFTN=-YSHIFT-1.
    YSHFT1=YSHFTN-.25
    YSHFT2=YSHFTN-.50
    YSHFT3=YSHFTN-.75
    CALL NOTATE (0.,YSHFT1,.14,25HSONIC LINE AND SHOCK WAVE,0.,25)
    CALL NOTATE (0.,YSHFT2,.14,LBLE1(1),0.,30)
    CALL NOTATE (0.,YSHFT3,.14,LBLE2(1),0.,40)
    IF (ABS(SNO).LT.1.E-06) GO TO 140
    TMP1(1)=XW(JW10)/SFACTOR
    TMP1(2)=XW(JW3)/SFACTOR
    TMP2(1)=0.
    TMP2(2)=TMP2(1)
    CALL DRAW (TMP1,TMP2,2)
140 IF (IWALL.EQ.0) GO TO 150
    TMP1(1)=-1./SFACTOR
    TMP1(2)=+2./SFACTOR
    TMP2(1)=RW(KM)/SFACTOR
    TMP2(2)=TMP2(1)
    IF (SNO.LT.-1.E-06) TMP2(1)=-RW(KM)/SFACTOR
    TMP2(2)=TMP2(1)
    CALL DRAW (TMP1,TMP2,2)
150 CALL NFRAME
    CALL CALPLT (2.,2.5,-3)

```

```

C
C
    XPG=5.
    YPG=8.
    TOPBND=-.8
    BOTBND=+.8
    SKIP=4.
    SCF=+.2
    YMOVE=SKIP-CPSTAR/SCF
    IF (ALPHA.EQ.0.) GO TO 200
    IF (ABS(SNO).GT.1.E-06) GO TO 200

```

```

C
C
C
    FIGURE 3 = CP VERSUS X

```

```

    NCOUNT=0
    DO 160 J=J2P1,J3M1

```

```

F1290
F1300
F1310
F1320
F1350
F1360
F1370
F1380
F1390
F1400
F1410
F1420
F1430
F1440
F1450
F1460
F1470
F1480
F1490
F1500
F1510
F1520
F1530
F1540
F1550
F1560
F1570
F1580
F1590
F1600
F1610
F1620
F1630
F1640
F1650
F1660
F1670
F1680
F1690
F1700
F1710
F1720
F1730

```



```

NCOUNT=NCOUNT+1
TMP1(NCOUNT)=XW(J)
TMP2(NCOUNT)=CP(J)
TMP3(NCOUNT)=CPO(J)
IF (TMP2(NCOUNT).LT.TOPBND) TMP2(NCOUNT)=TOPBND
IF (TMP3(NCOUNT).LT.TCPBND) TMP3(NCOUNT)=TOPBND
IF (TMP2(NCOUNT).GT.BOTBND) TMP2(NCOUNT)=BOTBND
IF (TMP3(NCOUNT).GT.BOTBND) TMP3(NCOUNT)=BOTBND

```

F1740  
F1750  
F1760  
F1770  
F1780  
F1790  
F1800  
F1810  
F1820  
F1830  
F1840  
F1850  
F1860  
F1870  
F1880  
F1890  
F1900  
F1910  
F1920  
F1930  
F1940  
F1950  
F1960  
F1970  
F1980  
F1990  
F2000  
F2010  
F2020  
F2030  
F2040  
F2050  
F2060  
F2070  
F2080  
F2090  
F2100  
F2110  
F2120  
F2130  
F2140  
F2150  
F2160

160 CONTINUE

```

TMP1(NCOUNT+1)=0.
TMP1(NCOUNT+2)=SCF
TMP2(NCOUNT+1)=BOTBND
TMP3(NCOUNT+1)=TMP2(NCOUNT+1)
TMP2(NCOUNT+2)=-SCF
TMP3(NCOUNT+2)=TMP2(NCOUNT+2)
CALL AXES (0.0,0.0,0.0,XPG,TMP1(NCOUNT+1),TMP1(NCOUNT+2),XTIC,XDV,1
1HX,.14,-1)
CALL AXES (-.5,0.,90.,YPG,TMP2(NCOUNT+1),TMP2(NCOUNT+2),YTIC,YDV,2
1HCP,.14,+2)

```

DRAW LINE FOR CPSTAR

```

CALL CALPLT (-.500,YMOVE,-3)
CALL CALPLT (.5,0.,2)
CALL CALPLT (+.500,-YMOVE,-3)
CALL LINE (TMP1,TMP2,NCOUNT,1,+1,3,.08)
CALL LINE (TMP1,TMP3,NCOUNT,1,+1,4,.07)
IF (HSPAN.LT.RMAX) GO TO 170

```

DRAW LINES FOR JW10 AND JW3

```

TMP1(1)=XW(JW10)/SCF
TMP1(2)=TMP1(1)
TMP2(1)=0.
TMP2(2)=.5
CALL DRAW (TMP1,TMP2,2)
TMP1(1)=XW(JW3)/SCF
TMP1(2)=TMP1(1)
CALL DRAW (TMP1,TMP2,2)
IF (JW2.EQ.JW3) GO TO 170
TMP1(1)=XW(JW20)/SCF
TMP1(2)=TMP1(1)
CALL DRAW (TMP1,TMP2,2)

```

170	CONTINUE	F2170
	CALL NOTATE (0.,-1.25,.14,26HBODY PRESSURE DISTRIBUTION,0.,26)	F2180
	CALL NOTATE (0.,-1.50,.14,13HIN WING PLANE,0.,13)	F2190
	CALL NOTATE (0.,-1.75,.14,LBL1(1),0.,30)	F2200
	CALL NOTATE (0.,-2.00,.14,LBL2(1),0.,40)	F2210
	CALL NFRAME	F2220
	CALL CALPLT (2.,2.5,-3)	F2230
C		F2240
C	FIGURE 2 - CP VERSUS X	F2250
C		F2260
	NCOUNT=0	F2270
	DO 180 J=J2P1,J3M1	F2280
	NCOUNT=NCOUNT+1	F2290
	TMP1(NCOUNT)=XW(J)	F2300
	TMP2(NCOUNT)=CP1(J)	F2310
	TMP3(NCOUNT)=CP2(J)	F2320
	IF (TMP2(NCOUNT).LT.TOPBND) TMP2(NCOUNT)=TOPBND	F2330
	IF (TMP3(NCOUNT).LT.TOPBND) TMP3(NCOUNT)=TOPBND	F2340
	IF (TMP2(NCOUNT).GT.BOTBND) TMP2(NCOUNT)=BOTBND	F2350
	IF (TMP3(NCOUNT).GT.BOTBND) TMP3(NCOUNT)=BOTBND	F2360
180	CONTINUE	F2370
	TMP1(NCOUNT+1)=0.	F2380
	TMP1(NCOUNT+2)=SCF	F2390
	TMP2(NCOUNT+1)=BOTBND	F2400
	TMP3(NCOUNT+1)=TMP2(NCOUNT+1)	F2410
	TMP2(NCOUNT+2)=-SCF	F2420
	TMP3(NCOUNT+2)=TMP2(NCOUNT+2)	F2430
	CALL AXES (0.0,0.0,0.,XPG,TMP1(NCOUNT+1),TMP1(NCOUNT+2),XTIC,XDV,1	F2440
	1HX,.14,-1)	F2450
	CALL AXES (-.5,0.,90.,YPG,TMP2(NCOUNT+1),TMP2(NCOUNT+2),YTIC,YDV,2	F2460
	1HCP,.14,+2)	F2470
C		F2480
C	DRAW LINE FOR CPSTAR	F2490
C		F2500
	CALL CALPLT (-.500,YMOVE,-3)	F2510
	CALL CALPLT (.5,0.,2)	F2520
	CALL CALPLT (+.500,-YMOVE,-3)	F2530
	CALL LINE (TMP1,TMP2,NCOUNT,1,+1,3,.08)	F2540
	CALL LINE (TMP1,TMP3,NCOUNT,1,+1,4,.07)	F2550
	IF (HSPAN.LT.RMAX) GO TO 190	F2560
C		F2570
C	DRAW LINES FOR JW10 AND JW3	F2580
C		F2590

	TMP1(1)=XW(JW10)/SCF	F2600
	TMP1(2)=TMP1(1)	F2610
	TMP2(1)=0.	F2620
	TMP2(2)=.5	F2630
	CALL DRAW (TMP1,TMP2,2)	F2640
	TMP1(1)=XW(JW3)/SCF	F2650
	TMP1(2)=TMP1(1)	F2660
	CALL DRAW (TMP1,TMP2,2)	F2670
	IF (JW2.EQ.JW3) GO TO 190	F2680
	TMP1(1)=XW(JW20)/SCF	F2690
	TMP1(2)=TMP1(1)	F2700
	CALL DRAW (TMP1,TMP2,2)	F2710
190	CONTINUE	F2720
	CALL NOTATE (0.,-1.25,.14,26HBODY PRESSURE DISTRIBUTION,0.,26)	F2730
	CALL NOTATE (0.,-1.50,.14,17HIN SYMMETRY PLANE,0.,17)	F2740
	CALL NOTATE (0.,-1.75,.14,LBLE1(1),0.,30)	F2750
	CALL NOTATE (0.,-2.00,.14,LBLE2(1),0.,40)	F2760
	CALL NFRAME	F2770
	CALL CALPLT (2.,2.5,-3)	F2780
	GO TO 230	F2790
C		F2800
C	FIGURE 4 - CP VERSUS X	F2810
C		F2820
200	NCOUNT=0	F2830
	DO 210 J=J2P1,J3M1	F2840
	NCOUNT=NCOUNT+1	F2850
	TMP1(NCOUNT)=XW(J)	F2860
	TMP2(NCOUNT)=CP(J)	F2870
	IF (TMP2(NCOUNT).LT.TOPBND) TMP2(NCOUNT)=TOPBND	F2880
	IF (TMP2(NCOUNT).GT.BOTBND) TMP2(NCOUNT)=BOTBND	F2890
210	CONTINUE	F2900
	TMP1(NCOUNT+1)=0.	F2910
	TMP1(NCOUNT+2)=SCF	F2920
	TMP2(NCOUNT+1)=BOTBND	F2930
	TMP3(NCOUNT+1)=TMP2(NCOUNT+1)	F2940
	TMP2(NCOUNT+2)=-SCF	F2950
	TMP3(NCOUNT+2)=TMP2(NCOUNT+2)	F2960
	CALL AXES (0.0,0.0,0.0,XPG,TMP1(NCOUNT+1),TMP1(NCOUNT+2),XTIC,XDV,1	F2970
	1HX,.14,-1)	F2980
	CALL AXES (-.5,0.,90.,YPG,TMP2(NCOUNT+1),TMP2(NCOUNT+2),YTIC,YDV,2	F2990
	1HCP,.14,+2)	F3000
C		F3010
C	DRAW LINE FOR CPSTAR	F3020

C	CALL CALPLT (-.500,YMOVE,-3)	F3030
	CALL CALPLT (.5,0.,2)	F3040
	CALL CALPLT (+.500,-YMOVE,-3)	F3050
	CALL LINE (TMP1,TMP2,NCOUNT,1,+1,3,-.08)	F3060
	IF (HSPAN.LT.RMAX) GO TO 220	F3070
C		F3080
C	DRAW LINES FOR JW10 AND JW3	F3090
C		F3100
	TMP1(1)=XW(JW10)/SCF	F3110
	TMP1(2)=TMP1(1)	F3120
	TMP2(1)=0.	F3130
	TMP2(2)=.5	F3140
	CALL DRAW (TMP1,TMP2,2)	F3150
	TMP1(1)=XW(JW3)/SCF	F3160
	TMP1(2)=TMP1(1)	F3170
	CALL DRAW (TMP1,TMP2,2)	F3180
	IF (JW2.EQ.JW3) GO TO 220	F3190
	TMP1(1)=XW(JW20)/SCF	F3200
	TMP1(2)=TMP1(1)	F3210
	CALL DRAW (TMP1,TMP2,2)	F3220
220	CONTINUE	F3230
	CALL NOTATE (0.,-1.25,.14,26HBODY PRESSURE DISTRIBUTION,0.,26)	F3240
	CALL NOTATE (0.,-1.50,.14,LBLE1(1),0.,30)	F3250
	CALL NOTATE (0.,-1.75,.14,LBLE2(1),0.,40)	F3260
	CALL NFRAME	F3270
230	IF (NREAD.EQ.NCASES) CALL CALPLT (0.,0.,999)	F3280
	IF (AMINF.GT.1.) J1=J1-2	F3290
	IF (AMINF.GT.1.) J4=J4+2	F3300
	RETURN	F3310
C		F3320
		F3330
240	FORMAT (A3,F5.3,2X,A3,F6.3,2X,A3,F5.3,1X)	F3340
250	FORMAT (A7,F6.2,1X,A4,2X,A7,F6.2,1X,A4,2X)	F3350
	END	F3360

## APPENDIX B

### SAMPLE INPUT

The input for a sample case is presented in this appendix. This case involves a lifting configuration composed of a parabolic-arc body with a fineness ratio of 10 and a wing with a strake and a swept trailing edge. The flow is separated at the leading edge. The free-stream Mach number and angle of attack are  $M_\infty = 0.98$  and  $\alpha = 4^\circ$ , respectively. The computation is made in the wing plane.

\$NAME  
 J1 = 18,  
 J2 = 30,  
 J3 = 80,  
 J4 = 92,  
 J5 = 109,  
 FAC = 0.12E+01,  
 KM = 50,  
 RCOM = 0.0,  
 A = 0.1E+01,  
 B = 0.1E+01,  
 IMALL = 0,  
 P = 0.0,  
 OMEGAD = 0.0,  
 ALPHAD = 0.4E+01,  
 HSPAN = 0.3E+00,  
 AMINF = 0.98E+00,  
 GAMMA = 0.14E+01,  
 IR = 0,  
 RC = 0.4E+01,  
 RMAX = 0.5E-01,  
 RN = 0.2E+01,  
 JS = 80,  
 RS = 0.0,  
 JW1 = 42,  
 JW2 = 70,  
 JW3 = 78,  
 JWD = 49,  
 IWING = 2,  
 B1 = 0.2E+00,  
 B2 = 0.8391E+00,  
 DEL1 = 0.1E+00,  
 DEL = 0.1E+00,  
 IVOR = 1,  
 IDIR = 4,  
 EPSI = 0.5E-05,  
 SUB = 0.13E+01,  
 SUP = 0.85E+00,  
 IMAX = 200,  
 SFACTOR = 0.5E+00,  
 \$END

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## APPENDIX C

### SAMPLE OUTPUT

In this appendix the output for the calculation described in appendix B is given. The printed output is given first, and then the plotted output is given in figures 7, 8, and 9.

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## SUBROUTINE START

ARRAYS AND PARAMETERS USED IN COMPUTATION  
J = AXIAL GRID INDEX, K = RADIAL GRID INDEX

K	RW(K)	RWR(K)	AXOCR(K)	ABAR(K)
1	2.04081633E-02	0.	9.99991754E-01	0.
2	4.16666667E-02	0.	9.99965627E-01	7.60416667E-01
3	6.33297872E-02	0.	9.99919347E-01	8.43971631E-01
4	8.69555217E-02	0.	9.99850317E-01	8.5869565E-01
5	1.11111111E-01	0.	9.99755645E-01	9.11111111E-01
6	1.36363636E-01	0.	9.99632021E-01	9.28030303E-01
7	1.62790698E-01	0.	9.99475657E-01	9.40199336E-01
8	1.90476190E-01	0.	9.99282406E-01	9.49404762E-01
9	2.19512195E-01	0.	9.99047288E-01	9.56639566E-01
10	2.50000000E-01	0.	9.98764792E-01	9.62500000E-01
11	2.82051282E-01	0.	9.98428564E-01	9.67365967E-01
12	3.15789474E-01	0.	9.98031314E-01	9.71491228E-01
13	3.51351351E-01	0.	9.97564659E-01	9.75051975E-01
14	3.88888889E-01	0.	9.97018939E-01	9.78174603E-01
15	4.23571429E-01	0.	9.96382985E-01	9.80952381E-01
16	4.70588235E-01	0.	9.95643855E-01	9.83455882E-01
17	5.15151515E-01	0.	9.94786511E-01	9.85734750E-01
18	5.62500000E-01	0.	9.93793421E-01	9.87847222E-01
19	6.12903226E-01	0.	9.92644090E-01	9.89813243E-01
20	6.66666667E-01	0.	9.91314482E-01	9.91666667E-01
21	7.24137921E-01	0.	9.89776311E-01	9.93431856E-01
22	7.85714286E-01	0.	9.87996180E-01	9.95126705E-01
23	8.51851852E-01	0.	9.85934520E-01	9.96779388E-01
24	9.23076923E-01	0.	9.83544279E-01	9.98397436E-01
25	1.00000000E+00	0.	9.80769303E-01	1.00000000E+00
26	1.08233333E+00	0.	9.77542327E-01	1.00160256E+00
27	1.17391304E+00	0.	9.73782477E-01	1.00322061E+00
28	1.27272727E+00	0.	9.69392160E-01	1.00487013E+00
29	1.38095238E+00	0.	9.64253190E-01	1.00656314E+00
30	1.50000000E+00	0.	9.58221963E-01	1.00833333E+00
31	1.63157895E+00	0.	9.51123465E-01	1.01018676E+00
32	1.77777778E+00	0.	9.42743860E-01	1.01215278E+00
33	1.94117647E+00	0.	9.32821463E-01	1.01426025E+00
34	2.12500000E+00	0.	9.21035739E-01	1.01654412E+00
35	2.33333333E+00	0.	9.06994502E-01	1.01904762E+00
36	2.57142857E+00	0.	8.90219313E-01	1.02182550E+00
37	2.84615385E+00	0.	8.70130103E-01	1.02494802E+00
38	3.16666667E+00	0.	8.46030955E-01	1.02850877E+00
39	3.54545455E+00	0.	8.17100566E-01	1.03263403E+00
40	4.00000000E+00	0.	7.82396930E-01	1.03750300E+00
41	4.55555556E+00	0.	7.40878518E-01	1.04336043E+00
42	5.25000000E+00	0.	6.91470507E-01	1.05059524E+00
43	6.14285714E+00	0.	6.33178544E-01	1.05980066E+00
44	7.33333333E+00	0.	5.65269540E-01	1.07196970E+00
45	9.00000000E+00	0.	4.87509156E-01	1.08888889E+00
46	1.15000000E+01	0.	4.00413440E-01	1.11413047E+00
47	1.56666667E+01	0.	3.05439309E-01	1.15602877E+00
48	2.40000000E+01	0.	2.04538687E-01	1.23956375E+00
49	4.90000000E+01	0.	1.02019786E-01	1.48979592E+00

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K	CON1(K)	CON2(K)	CON3(K)	CON7(K)	CON8(K)	CON9(K)	CON10(K)	CON11(K)
1	1.00000000E+00	5.84305735E-04	1.40291807E+00	0.	1.18417810E-09	5.80247270E-08	0.	2.43353323E-07
2	2.39583333E-01	4.70950280E-04	2.71267361E-01	0.	3.97852061E-09	9.54844948E-08	0.	8.17672013E-07
3	1.56028369E-01	5.12328372E-04	1.25748202E-01	0.	1.01509756E-08	1.59125045E-07	0.	2.08725045E-06
4	1.14130435E-01	5.58352795E-04	7.38421550E-02	0.	2.05438556E-08	2.36254385E-07	0.	4.22749918E-06
5	8.88888889E-02	6.09663161E-04	4.93827160E-02	0.	3.66246912E-08	3.29622221E-07	0.	7.52670569E-06
6	7.19696970E-02	6.67005228E-04	3.58700643E-02	0.	6.03925310E-08	4.42585227E-07	0.	1.24029916E-05
7	5.98006645E-02	7.31250517E-04	2.75935144E-02	0.	9.42962435E-08	5.79248353E-07	0.	1.93707319E-05
8	5.05952381E-02	8.03420486E-04	2.21447444E-02	0.	1.41832222E-07	7.44650663E-07	0.	2.91470389E-05
9	4.33604336E-02	8.76471727E-04	1.83655172E-02	0.	2.07439246E-07	9.45001007E-07	0.	4.26306434E-05
10	3.75000000E-02	9.76542300E-04	1.56250000E-02	0.	2.96994972E-07	1.18797989E-06	0.	6.10351562E-05
11	3.26303263E-02	1.08064135E-03	1.35889297E-02	0.	4.18318213E-07	1.48312821E-06	0.	8.59681033E-05
12	2.8508719E-02	1.19816276E-03	1.20229301E-02	0.	5.81794964E-07	1.84235072E-06	0.	1.19564134E-04
13	2.49480249E-02	1.33293225E-03	1.08056241E-02	0.	8.01282035E-07	2.28057195E-06	0.	1.64670714E-04
14	2.18253648E-02	1.48843545E-03	9.84189972E-03	0.	1.09534294E-06	2.81659613E-06	0.	2.25102892E-04
15	1.90476190E-02	1.6597231E-03	9.7029478E-03	0.	1.48896091E-06	3.47424213E-06	0.	3.05994951E-04
16	1.6544117E-02	1.87073869E-03	8.44777249E-03	0.	2.01593028E-06	4.28835185E-06	0.	4.14291938E-04
17	1.4202496E-02	2.10066222E-03	7.94354365E-03	0.	2.72222018E-06	5.2840776E-06	0.	5.99440197E-04
18	1.2152777E-02	2.38418579E-03	7.53520448E-03	0.	3.67074475E-06	6.52516844E-06	0.	7.54371855E-04
19	1.0186757E-02	2.70703103E-03	7.20625157E-03	0.	4.94818678E-06	8.07335738E-06	0.	1.01684190E-03
20	8.33333333E-03	3.08041975E-03	6.94444444E-03	0.	6.67484997E-06	1.00122750E-05	0.	1.3717441E-03
21	6.56814450E-03	3.53466303E-03	6.74070659E-03	0.	9.01902618E-06	1.24548457E-05	0.	1.64369155E-03
22	4.87012987E-03	4.06731570E-03	6.58837915E-03	0.	1.22181716E-05	1.55504002E-05	0.	2.01054908E-03
23	3.22061192E-03	4.70419106E-03	6.4821320E-03	0.	1.66104781E-05	1.94992569E-05	0.	3.41363068E-03
24	1.60254410E-02	5.47074682E-03	6.42052926E-03	0.	2.26825272E-05	2.4727379E-05	0.	4.66146175E-03
25	2.64217094E-03	6.40000000E-03	6.43000000E-03	0.	3.11421800E-05	3.11421800E-05	0.	6.40000000E-03
26	1.60254410E-03	7.53520448E-03	6.42052926E-03	0.	3.930316790E-05	3.97215498E-05	0.	8.84349970E-03
27	3.22061192E-03	8.93344446E-03	6.4821320E-03	0.	5.99058946E-05	5.16309472E-05	0.	1.23112338E-02
28	4.87012987E-03	1.06720472E-02	6.58837915E-03	0.	8.41180165E-05	6.60927272E-05	0.	1.72670144E-02
29	6.56814450E-03	1.28547262E-02	6.74070659E-03	0.	1.19285944E-04	8.63794769E-05	0.	2.45443117E-02
30	8.33333333E-03	1.56250000E-02	6.94444444E-03	0.	1.71069104E-04	1.14046069E-04	0.	3.5156430E-02
31	1.0186757E-02	1.91834310E-02	7.02625157E-03	0.	2.48491094E-04	1.52300993E-04	0.	5.10671599E-02
32	1.2152777E-02	2.38149672E-02	7.53520448E-03	0.	3.66246912E-04	2.06013880E-04	0.	7.5707369E-02
33	1.4202496E-02	2.99225918E-02	7.94354365E-03	0.	5.48837019E-04	2.83742222E-04	0.	1.1279777E-01
34	1.6544117E-02	3.81469727E-02	8.44777249E-03	0.	8.38198702E-04	3.9446448E-04	0.	1.72257423E-01
35	1.90476190E-02	4.93827160E-02	9.07329478E-03	0.	1.30827059E-03	5.60687398E-04	0.	2.6386154E-01
36	2.18253648E-02	6.56770312E-02	9.84189972E-03	0.	2.09325129E-03	8.14275500E-04	0.	4.3030530E-01
37	2.49480249E-02	8.75319492E-02	1.08056241E-02	0.	3.45026442E-03	1.21225507E-03	0.	7.0906082E-01
38	2.8508719E-02	1.20586272E-01	1.20229301E-02	0.	5.88286338E-03	1.85774633E-03	0.	1.20891170E+00
39	3.26303263E-02	1.70753364E-01	1.35889297E-02	0.	1.04443676E-02	2.94584727E-03	0.	2.1444212E+00
40	3.75000000E-02	2.30030303E-01	1.56250000E-02	0.	1.94638625E-02	4.86596563E-03	0.	4.03003000E+00
41	4.33604336E-02	3.81023947E-01	1.83655172E-02	0.	3.84788162E-02	8.44656941E-03	0.	7.90774517E+00
42	5.05952381E-02	6.10251662E-01	2.21447444E-02	0.	8.18592393E-02	1.55922361E-02	0.	1.68228190E+01
43	5.98006645E-02	1.04123282E+00	2.75735144E-02	0.	1.91186717E-01	3.11234191E-02	0.	3.42506031E+01
44	7.19696970E-02	1.92940235E+00	3.58700643E-02	0.	5.04285529E-01	6.88363933E-02	0.	1.03737797E+02
45	8.88888889E-02	4.00000000E+00	4.93827160E-02	0.	1.57657786E+00	1.75174763E-01	0.	3.24000000E+02
46	1.14130435E-01	7.76533333E+00	7.38421550E-02	0.	4.2644136E+00	5.46470749E-01	0.	1.143991E+03
47	1.56028369E-01	1.04123282E+00	1.25748202E-01	0.	3.62616549E+01	1.33280661E+00	0.	7.03864502E+03
48	2.39583333E-01	1.56028369E+00	2.71267361E-01	0.	4.37936907E+02	1.02473711E+01	0.	9.00000000E+04
49	4.87012987E-01	2.50000000E+00	1.02019786E-01	0.	2.92079587E+04	1.02473711E+02	0.	8.00230000E+06





J	Y(J)	FUN(J)	FUN4(J)	FUN5(J)	FUN6(J)	FUN7(J)	FUN8(J)
1	-2.3585111E+00	0.	0.	0.	0.	0.	0.
2	-1.9388479E+00	0.	0.	0.	0.	0.	0.
3	-1.6907116E+00	0.	0.	0.	0.	0.	0.
4	-1.4239184E+00	0.	0.	0.	0.	0.	0.
5	-1.2099233E+00	0.	0.	0.	0.	0.	0.
6	-1.0316130E+00	0.	0.	0.	0.	0.	0.
7	-8.8303871E-01	0.	0.	0.	0.	0.	0.
8	-7.5917364E-01	0.	0.	0.	0.	0.	0.
9	-6.5597403E-01	0.	0.	0.	0.	0.	0.
10	-5.6993189E-01	0.	0.	0.	0.	0.	0.
11	-4.9831860E-01	0.	0.	0.	0.	0.	0.
12	-4.3859400E-01	0.	0.	0.	0.	0.	0.
13	-3.8883200E-01	0.	0.	0.	0.	0.	0.
14	-3.4726000E-01	0.	0.	0.	0.	0.	0.
15	-3.1280000E-01	0.	0.	0.	0.	0.	0.
16	-2.8400000E-01	0.	0.	0.	0.	0.	0.
17	-2.6000000E-01	0.	0.	0.	0.	0.	0.
18	-2.4000000E-01	0.	0.	0.	0.	0.	0.
19	-2.2000000E-01	0.	0.	0.	0.	0.	0.
20	-2.0000000E-01	0.	0.	0.	0.	0.	0.
21	-1.8000000E-01	0.	0.	0.	0.	0.	0.
22	-1.6000000E-01	0.	0.	0.	0.	0.	0.
23	-1.4000000E-01	0.	0.	0.	0.	0.	0.
24	-1.2000000E-01	0.	0.	0.	0.	0.	0.
25	-1.0000000E-01	0.	0.	0.	0.	0.	0.
26	-8.0000000E-02	0.	0.	0.	0.	0.	0.
27	-6.0000000E-02	0.	0.	0.	0.	0.	0.
28	-4.0000000E-02	0.	0.	0.	0.	0.	0.
29	-2.0000000E-02	0.	0.	0.	0.	0.	0.
30	0.	0.	0.	0.	0.	0.	0.
31	2.0000000E-02	0.	0.	0.	0.	0.	0.
32	4.0000000E-02	0.	0.	0.	0.	0.	0.
33	6.0000000E-02	0.	0.	0.	0.	0.	0.
34	8.0000000E-02	0.	0.	0.	0.	0.	0.
35	1.0000000E-01	0.	0.	0.	0.	0.	0.
36	1.2000000E-01	0.	0.	0.	0.	0.	0.
37	1.4000000E-01	0.	0.	0.	0.	0.	0.
38	1.6000000E-01	0.	0.	0.	0.	0.	0.
39	1.8000000E-01	0.	0.	0.	0.	0.	0.
40	2.0000000E-01	0.	0.	0.	0.	0.	0.
41	2.2000000E-01	0.	0.	0.	0.	0.	0.
42	2.4000000E-01	0.	0.	0.	0.	0.	0.
43	2.6000000E-01	9.53939531E-07	2.73510622E-02	0.	0.	0.	0.
44	2.8000000E-01	1.87405934E-06	2.70125273E-02	0.	0.	0.	0.
45	3.0000000E-01	2.7499430E-06	2.67173511E-02	0.	0.	0.	0.
46	3.2000000E-01	5.63504123E-06	2.64052491E-02	0.	0.	0.	0.
47	3.4000000E-01	1.56172075E-06	2.61957176E-02	0.	0.	0.	0.
48	3.6000000E-01	2.62370642E-06	2.60038047E-02	0.	0.	0.	0.
49	3.8000000E-01	7.44376386E-06	2.58314536E-02	0.	0.	0.	0.
50	4.0000000E-01	1.10170091E-05	2.56641811E-02	0.	0.	0.	0.
51	4.2000000E-01	2.28340664E-05	2.54848774E-02	0.	0.	0.	0.
52	4.4000000E-01	5.13316618E-05	2.53185020E-02	0.	0.	0.	0.
53	4.6000000E-01	1.17302008E-04	2.5166657531E-02	0.	0.	0.	0.
54	4.8000000E-01	3.78713413E-04	2.50262184E-02	0.	0.	0.	0.
55	5.0000000E-01	6.21415138E-04	2.488382073E-02	0.	0.	0.	0.
56	5.2000000E-01	9.88097385E-04	2.47592393E-02	0.	0.	0.	0.
57	5.4000000E-01	1.647369774E-04	2.464194610E-02	0.	0.	0.	0.
58	5.6000000E-01	5.96350758E-04	2.45263296E-02	0.	0.	0.	0.
59	5.8000000E-01	5.46040400E-04	2.441176190E-02	0.	0.	0.	0.
60	6.0000000E-01	4.70930224E-04	2.429855419E-02	0.	0.	0.	0.
61	6.2000000E-01	3.46330234E-04	2.41870098E-02	0.	0.	0.	0.
62	6.4000000E-01	1.81178247E-04	2.407972444E-02	0.	0.	0.	0.
63	6.6000000E-01	7.39360310E-05	2.397618829E-02	0.	0.	0.	0.
64	6.8000000E-01	3.28740962E-04	2.38761618E-02	0.	0.	0.	0.
65	7.0000000E-01	9.53142637E-04	2.37805984E-02	0.	0.	0.	0.
66	7.2000000E-01	6.97142457E-04	2.369707244E-02	0.	0.	0.	0.
67	7.4000000E-01	7.33522784E-04	2.36158829E-02	0.	0.	0.	0.
68	7.6000000E-01	6.71112719E-04	2.35369994E-02	0.	0.	0.	0.
69	7.8000000E-01	5.47428137E-04	2.34608994E-02	0.	0.	0.	0.
70	8.0000000E-01	4.06968817E-04	2.33877473E-03	0.	0.	0.	0.
71	8.2000000E-01	2.99360304E-04	2.33179974E-03	0.	0.	0.	0.
72	8.4000000E-01	1.46981405E-04	2.32511714E-03	0.	0.	0.	0.
73	8.6000000E-01	7.98991095E-05	2.31874583E-03	0.	0.	0.	0.
74	8.8000000E-01	4.44308361E-05	2.31263341E-03	0.	0.	0.	0.
75	9.0000000E-01	2.57206279E-05	2.30677674E-03	0.	0.	0.	0.
76	9.2000000E-01	1.66612483E-05	2.30113677E-03	0.	0.	0.	0.
77	9.4000000E-01	1.13347699E-05	2.29572572E-03	0.	0.	0.	0.
78	9.6000000E-01	3.88703409E-06	2.29059257E-03	0.	0.	0.	0.
79	9.8000000E-01	0.	0.	0.	0.	0.	0.
80	1.0000000E+00	0.	0.	0.	0.	0.	0.
81	1.0200000E+00	0.	0.	0.	0.	0.	0.
82	1.0400000E+00	0.	0.	0.	0.	0.	0.
83	1.0600000E+00	0.	0.	0.	0.	0.	0.
84	1.0800000E+00	0.	0.	0.	0.	0.	0.
85	1.1000000E+00	0.	0.	0.	0.	0.	0.
86	1.1200000E+00	0.	0.	0.	0.	0.	0.
87	1.1400000E+00	0.	0.	0.	0.	0.	0.
88	1.1600000E+00	0.	0.	0.	0.	0.	0.
89	1.1800000E+00	0.	0.	0.	0.	0.	0.
90	1.2000000E+00	0.	0.	0.	0.	0.	0.
91	1.2200000E+00	0.	0.	0.	0.	0.	0.
92	1.2400000E+00	0.	0.	0.	0.	0.	0.
93	1.2600000E+00	0.	0.	0.	0.	0.	0.
94	1.2800000E+00	0.	0.	0.	0.	0.	0.
95	1.3000000E+00	0.	0.	0.	0.	0.	0.
96	1.3200000E+00	0.	0.	0.	0.	0.	0.
97	1.3400000E+00	0.	0.	0.	0.	0.	0.
98	1.3600000E+00	0.	0.	0.	0.	0.	0.
99	1.3800000E+00	0.	0.	0.	0.	0.	0.
100	1.4000000E+00	0.	0.	0.	0.	0.	0.
101	1.4200000E+00	0.	0.	0.	0.	0.	0.
102	1.4400000E+00	0.	0.	0.	0.	0.	0.
103	1.4600000E+00	0.	0.	0.	0.	0.	0.
104	1.4800000E+00	0.	0.	0.	0.	0.	0.
105	1.5000000E+00	0.	0.	0.	0.	0.	0.
106	1.5200000E+00	0.	0.	0.	0.	0.	0.
107	1.5400000E+00	0.	0.	0.	0.	0.	0.
108	1.5600000E+00	0.	0.	0.	0.	0.	0.
109	1.5800000E+00	0.	0.	0.	0.	0.	0.

ORIGINAL PAGE IS  
OF POOR QUALITY

J	X4(J)	FOR(J)	FOR(J)	FOR(J)	FOR(J)	FOR(J)	FOR(J)	FOR(J)	FOR(J)
1	-2.35001111E+00	0.	1.00000000E+00	0.	0	4	50	R	
2	-1.90000000E+00	0.	1.00000000E+00	0.	0	4	50	R	
3	-1.00000000E+00	0.	1.00000000E+00	0.	0	4	50	R	
4	-1.42341046E+00	0.	1.00000000E+00	0.	0	4	50	R	
5	-1.20000000E+00	0.	1.00000000E+00	0.	0	4	50	R	
6	-1.03101000E+00	0.	1.00000000E+00	0.	0	4	50	R	
7	-8.80000000E-01	0.	1.00000000E+00	0.	0	4	50	R	
8	-7.59173342E-01	0.	1.00000000E+00	0.	0	4	50	R	
9	-6.55978035E-01	0.	1.00000000E+00	0.	0	4	50	R	
10	-5.69481695E-01	0.	1.00000000E+00	0.	0	4	50	R	
11	-4.98318080E-01	0.	1.00000000E+00	0.	0	4	50	R	
12	-4.85948400E-01	0.	1.00000000E+00	0.	0	4	50	R	
13	-3.88822000E-01	0.	1.00000000E+00	0.	0	4	50	R	
14	-3.47300000E-01	0.	1.00000000E+00	0.	0	4	50	R	
15	-3.12800000E-01	0.	1.00000000E+00	0.	0	4	50	R	
16	-2.84000000E-01	0.	1.00000000E+00	0.	0	4	50	R	
17	-2.60000000E-01	0.	1.00000000E+00	0.	0	4	50	R	
18	-2.40000000E-01	0.	1.00000000E+00	0.	0	4	50	R	
19	-2.20000000E-01	0.	1.00000000E+00	0.	0	4	50	R	
20	-2.00000000E-01	0.	1.00000000E+00	0.	0	4	50	R	
21	-1.80000000E-01	0.	1.00000000E+00	0.	0	4	50	R	
22	-1.60000000E-01	0.	1.00000000E+00	0.	0	4	50	R	
23	-1.40000000E-01	0.	1.00000000E+00	0.	0	4	50	R	
24	-1.20000000E-01	0.	1.00000000E+00	0.	0	4	50	R	
25	-1.00000000E-01	0.	1.00000000E+00	0.	0	4	50	R	
26	-8.00000000E-02	0.	1.00000000E+00	0.	0	4	50	R	
27	-6.00000000E-02	0.	1.00000000E+00	0.	0	4	50	R	
28	-4.00000000E-02	0.	1.00000000E+00	0.	0	4	50	R	
29	-2.00000000E-02	0.	1.00000000E+00	0.	0	4	50	R	
30	0.	0.	1.00000000E+00	0.	0	4	50	R	
31	2.00000000E-02	0.	1.00000000E+00	0.	0	4	50	R	
32	4.00000000E-02	0.	1.00000000E+00	0.	0	4	50	R	
33	6.00000000E-02	0.	1.00000000E+00	0.	0	4	50	R	
34	8.00000000E-02	0.	1.00000000E+00	0.	0	4	50	R	
35	1.00000000E-01	0.	1.00000000E+00	0.	0	4	50	R	
36	1.20000000E-01	0.	1.00000000E+00	0.	0	4	50	R	
37	1.40000000E-01	0.	1.00000000E+00	0.	0	4	50	R	
38	1.60000000E-01	0.	1.00000000E+00	0.	0	4	50	R	
39	1.80000000E-01	0.	1.00000000E+00	0.	0	4	50	R	
40	2.00000000E-01	0.	1.00000000E+00	0.	0	4	50	R	
41	2.20000000E-01	0.	1.00000000E+00	0.	0	4	50	R	
42	2.40000000E-01	0.	1.00000000E+00	0.	1	5	50	R	1
43	2.60000000E-01	2.38484883E-07	1.00000000E+00	0.	1	6	50	R	1
44	2.80000000E-01	4.02514834E-07	1.00000000E+00	0.	2	6	50	R	1
45	3.00000000E-01	6.87471263E-07	1.00000000E+00	0.	2	6	50	R	1
46	3.20000000E-01	9.08760000E-07	1.00000000E+00	0.	2	6	50	R	1
47	3.40000000E-01	1.14743019E-06	1.00000000E+00	0.	2	6	50	R	1
48	3.60000000E-01	1.40782433E-06	1.00000000E+00	0.	3	7	50	R	1
49	3.80000000E-01	1.81024096E-06	1.00000000E+00	0.	3	7	50	R	1
50	4.00000000E-01	2.71922277E-06	1.00000000E+00	0.	3	7	50	R	1
51	4.20000000E-01	3.70851650E-06	1.00000000E+00	0.	3	7	50	R	1
52	4.40000000E-01	5.3453654E-06	1.00000000E+00	0.	4	7	50	R	1
53	4.60000000E-01	4.32827169E-05	1.00000000E+00	0.	4	8	50	R	1
54	4.80000000E-01	9.91190332E-05	1.00000000E+00	0.	4	8	50	R	1
55	5.00000000E-01	1.55353777E-04	1.00000000E+00	0.	5	9	50	R	1
56	5.20000000E-01	1.72024343E-04	1.00000000E+00	0.	5	9	50	R	1
57	5.40000000E-01	1.61842493E-04	1.00000000E+00	0.	6	10	50	R	1
58	5.60000000E-01	1.49012742E-04	1.00000000E+00	0.	7	11	50	R	1
59	5.80000000E-01	1.36512215E-04	1.00000000E+00	0.	7	11	50	R	1
60	6.00000000E-01	1.17732556E-04	1.00000000E+00	0.	8	12	50	R	1
61	6.20000000E-01	8.65750335E-05	1.00000000E+00	0.	8	12	50	R	1
62	6.40000000E-01	4.04195619E-05	1.00000000E+00	0.	9	13	50	R	1
63	6.60000000E-01	-1.84840073E-05	1.00000000E+00	0.	9	13	50	R	1
64	6.80000000E-01	-3.21852403E-05	1.00000000E+00	0.	9	14	50	R	1
65	7.00000000E-01	-1.30285657E-04	1.00000000E+00	0.	10	14	50	R	1
66	7.20000000E-01	-1.74285614E-04	1.00000000E+00	0.	10	14	50	R	1
67	7.40000000E-01	-1.83280646E-04	1.00000000E+00	0.	10	14	50	R	1
68	7.60000000E-01	-1.67778183E-04	1.00000000E+00	0.	11	15	50	R	1
69	7.80000000E-01	-1.36351034E-04	1.00000000E+00	0.	11	15	50	R	1
70	8.00000000E-01	-1.01742204E-04	1.00000000E+00	0.	11	15	50	R	2
71	8.20000000E-01	-7.48400010E-05	1.00000000E+00	0.	11	15	50	R	4
72	8.40000000E-01	-3.67451054E-05	1.00000000E+00	0.	11	15	50	R	6
73	8.60000000E-01	-1.99747174E-05	1.00000000E+00	0.	11	15	50	R	7
74	8.80000000E-01	-1.11077315E-05	1.00000000E+00	0.	11	15	50	R	8
75	9.00000000E-01	-6.43015598E-06	1.00000000E+00	0.	11	15	50	R	10
76	9.20000000E-01	-4.01536707E-06	1.00000000E+00	0.	11	15	50	R	10
77	9.40000000E-01	-2.83369249E-06	1.00000000E+00	0.	11	15	50	R	11
78	9.60000000E-01	-9.71758523E-07	1.00000000E+00	0.	11	15	50	R	12
79	9.80000000E-01	0.	1.00000000E+00	0.	11	15	50	R	
80	1.00000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
81	1.02000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
82	1.04000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
83	1.06000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
84	1.08000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
85	1.10000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
86	1.12000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
87	1.14000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
88	1.16000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
89	1.18000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
90	1.20000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
91	1.22000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
92	1.24000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
93	1.26000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
94	1.28000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
95	1.30000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
96	1.32000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
97	1.34000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
98	1.36000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
99	1.38000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
100	1.40000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
101	1.42000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
102	1.44000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
103	1.46000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
104	1.48000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
105	1.50000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
106	1.52000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
107	1.54000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
108	1.56000000E+00	0.	1.00000000E+00	0.	11	15	50	R	
109	1.58000000E+00	0.	1.00000000E+00	0.	11	15	50	R	



J	XX(J)	VLAM(J)	VTAL(J)	VLAMP(J)	VTAMP(J)	GAM	GAMX	YV(J)	ZP(J)	R(J)	YF(J)
43	2.000E-01	1.871E-02	2.422E-02	8.426E-01	1.747E+00	3.422E+03	1.764E+01	4.017E-02	6.334E-04	3.848E-02	4.048E-02
44	2.400E-01	3.472E-02	6.952E-02	7.186E-01	1.560E+00	7.042E-03	1.856E-01	4.378E-02	1.293E-03	4.032E-02	4.448E-02
45	3.000E-01	4.333E-02	9.977E-02	6.252E-01	1.446E+00	1.079E-02	1.908E-01	4.735E-02	1.916E-03	4.200E-02	4.868E-02
46	3.200E-01	6.320E-02	1.270E-01	5.503E-01	1.336E+00	1.404E-02	1.957E-01	5.087E-02	2.436E-03	4.352E-02	5.248E-02
47	3.400E-01	7.066E-02	1.531E-01	4.884E-01	1.241E+00	1.859E-02	2.001E-01	5.436E-02	3.004E-03	4.488E-02	5.448E-02
48	3.600E-01	7.995E-02	1.771E-01	4.350E-01	1.160E+00	2.252E-02	2.049E-01	5.783E-02	3.734E-03	4.608E-02	6.048E-02
49	3.800E-01	8.816E-02	1.993E-01	3.837E-01	1.091E+00	2.677E-02	2.105E-01	6.128E-02	4.301E-03	4.712E-02	6.450E-02
50	4.000E-01	9.517E-02	2.212E-01	3.191E-01	1.037E+00	3.112E-02	2.242E-01	6.470E-02	4.836E-03	4.800E-02	6.857E-02
51	4.200E-01	1.003E-01	2.417E-01	2.042E-01	1.317E+00	3.601E-02	2.633E-01	6.826E-02	5.289E-03	4.872E-02	7.284E-02
52	4.400E-01	1.017E-01	2.524E-01	-1.817E-02	1.039E+00	4.242E-02	3.717E-01	7.215E-02	5.552E-03	4.928E-02	7.767E-02
53	4.600E-01	9.735E-02	2.837E-01	-3.196E-01	1.074E+00	5.226E-02	6.075E-01	7.759E-02	5.482E-03	4.968E-02	8.386E-02
54	4.800E-01	8.861E-02	3.046E-01	-4.527E-01	5.863E-01	6.783E-02	9.085E-01	8.515E-02	5.124E-03	4.992E-02	9.250E-02
55	5.000E-01	8.105E-02	3.219E-01	-3.183E-01	7.019E-01	8.698E-02	1.001E+00	9.588E-02	4.821E-03	5.000E-02	1.042E-01
56	5.200E-01	7.730E-02	3.320E-01	-1.400E-01	3.624E-01	1.043E-01	8.488E-01	1.093E-01	4.775E-03	4.992E-02	1.184E-01
57	5.400E-01	7.629E-02	3.365E-01	-3.203E-02	1.113E-01	1.190E-01	6.482E-01	1.243E-01	4.925E-03	4.968E-02	1.340E-01
58	5.600E-01	7.542E-02	3.372E-01	1.532E-02	-3.043E-02	1.300E-01	5.052E-01	1.398E-01	5.117E-03	4.928E-02	1.501E-01
59	5.800E-01	7.707E-02	3.358E-01	3.403E-02	-9.833E-02	1.390E-01	4.167E-01	1.554E-01	5.470E-03	4.872E-02	1.662E-01
60	6.000E-01	7.795E-02	3.335E-01	4.597E-02	-1.228E-01	1.465E-01	3.339E-01	1.708E-01	5.808E-03	4.800E-02	1.821E-01
61	6.200E-01	7.709E-02	3.310E-01	6.136E-02	-1.223E-01	1.529E-01	2.957E-01	1.859E-01	6.167E-03	4.712E-02	1.976E-01
62	6.400E-01	8.063E-02	3.287E-01	8.440E-02	-1.067E-01	1.580E-01	2.313E-01	2.005E-01	6.564E-03	4.608E-02	2.124E-01
63	6.600E-01	8.272E-02	3.263E-01	1.167E-01	-8.172E-02	1.618E-01	1.562E-01	2.141E-01	7.014E-03	4.488E-02	2.265E-01
64	6.800E-01	8.556E-02	3.255E-01	1.594E-01	-5.033E-02	1.639E-01	7.019E-02	2.268E-01	7.536E-03	4.352E-02	2.397E-01
65	7.000E-01	8.935E-02	3.248E-01	2.128E-01	-1.692E-02	1.642E-01	-2.249E-02	2.384E-01	8.148E-03	4.200E-02	2.516E-01
66	7.200E-01	9.429E-02	3.248E-01	2.740E-01	1.728E-02	1.627E-01	-1.140E-01	2.486E-01	8.872E-03	4.032E-02	2.620E-01
67	7.400E-01	1.005E-01	3.255E-01	3.466E-01	4.909E-02	1.596E-01	-1.944E-01	2.573E-01	9.722E-03	3.848E-02	2.710E-01
68	7.600E-01	1.082E-01	3.263E-01	4.207E-01	7.622E-02	1.551E-01	-2.546E-01	2.646E-01	1.072E-02	3.648E-02	2.784E-01
69	7.800E-01	1.173E-01	3.285E-01	4.925E-01	9.713E-02	1.497E-01	-2.888E-01	2.705E-01	1.186E-02	3.432E-02	2.844E-01
70	8.000E-01	1.277E-01	3.306E-01	5.559E-01	1.115E-01	1.439E-01	-2.957E-01	2.751E-01	1.312E-02	3.200E-02	2.889E-01
71	8.200E-01	1.392E-01	3.330E-01	6.055E-01	1.200E-01	1.382E-01	-2.825E-01	2.787E-01	1.450E-02	2.952E-02	2.923E-01
72	8.400E-01	1.515E-01	3.354E-01	6.378E-01	1.242E-01	1.329E-01	-2.533E-01	2.815E-01	1.595E-02	2.688E-02	2.948E-01
73	8.600E-01	1.643E-01	3.379E-01	6.521E-01	1.260E-01	1.282E-01	-2.163E-01	2.837E-01	1.745E-02	2.408E-02	3.965E-01
74	8.800E-01	1.772E-01	3.405E-01	6.503E-01	1.265E-01	1.243E-01	-1.776E-01	2.854E-01	1.894E-02	2.112E-02	2.977E-01
75	9.000E-01	1.901E-01	3.433E-01	6.360E-01	1.267E-01	1.212E-01	-1.411E-01	2.867E-01	2.042E-02	1.800E-02	2.985E-01
76	9.200E-01	2.026E-01	3.456E-01	6.134E-01	1.268E-01	1.187E-01	-1.091E-01	2.879E-01	2.185E-02	1.472E-02	2.991E-01
77	9.400E-01	2.145E-01	3.481E-01	5.865E-01	1.260E-01	1.168E-01	-8.211E-02	2.888E-01	2.324E-02	1.128E-02	2.994E-01
78	9.600E-01	2.250E-01	3.505E-01	5.585E-01	1.245E-01	1.154E-01	-6.021E-02	2.897E-01	2.458E-02	7.680E-03	2.996E-01

SIGMA = 4.86596563E-03  
 DELTA = 5.00000000E-02  
 BETASQ = 3.96000000E-02  
 DXR = 5.00000000E+01  
 DXSOR = 2.50000000E+03  
 GAMPI = 2.30496000E+00  
 CPIDXR = 1.15248000E+02  
 KMM1 = 49  
 KFM1 = 48  
 KF = 49  
 DELFTA = 2.00000000E-02  
 PIR = 3.18309886E-01  
 CON4 = 2.18792935E-01  
 CONS = 11111  
 H = 11111  
 JT = 123  
 JI = 2  
 JF = 108  
 DX = 2.00000000E-02  
 JXN = 7  
 SNO = 0.  
 CS20 = 1.00000000E+00  
 SNALP = 6.97564737E-02  
 IJW = 71  
 JW10 = 43  
 JW20 = 71  
 JW1X = R  
 JW3X = R  
 BETA = 11111  
 JW3M1 = 77  
 DLTPH = 2.63895147E-04  
 JCHCK = 78  
 IW = 1  
 JW10M2 = 41  
 JW3P1 = 79  
 JW10M1 = 42  
 H = 78  
 XWM = 11111  
 XWMSQR = 11111

LOCATION AND VALUE OF GREATEST CHANGE IN VELOCITY  
POTENTIAL (NEGATIVE LOCATION INDICES ARE FOR  
POINTS UNDER WING)

1	JMARK=	69	KMARK=	1	DPHIMX=	1.11764467E-02
2	JMARK=	-71	KMARK=	-2	DPHIMX=	4.02985866E-03
3	JMARK=	-70	KMARK=	-2	DPHIMX=	1.94666761E-03
4	JMARK=	-71	KMARK=	-2	DPHIMX=	1.25219995E-03
5	JMARK=	-66	KMARK=	-1	DPHIMX=	9.61927189E-04
6	JMARK=	78	KMARK=	1	DPHIMX=	1.05586409E-04
7	JMARK=	78	KMARK=	1	DPHIMX=	9.59222312E-05
8	JMARK=	78	KMARK=	1	DPHIMX=	9.05485458E-05
9	JMARK=	78	KMARK=	1	DPHIMX=	8.41379556E-05
10	JMARK=	78	KMARK=	1	DPHIMX=	7.85150904E-05
11	JMARK=	78	KMARK=	1	DPHIMX=	7.32160674E-05
12	JMARK=	78	KMARK=	1	DPHIMX=	6.86013757E-05
13	JMARK=	78	KMARK=	1	DPHIMX=	6.46195897E-05
14	JMARK=	78	KMARK=	1	DPHIMX=	6.09401991E-05
15	JMARK=	78	KMARK=	1	DPHIMX=	5.78092335E-05
16	JMARK=	78	KMARK=	1	DPHIMX=	5.49343102E-05
17	JMARK=	78	KMARK=	1	DPHIMX=	5.23569608E-05
18	JMARK=	78	KMARK=	1	DPHIMX=	5.00228118E-05
19	JMARK=	78	KMARK=	1	DPHIMX=	4.78872228E-05
20	JMARK=	78	KMARK=	1	DPHIMX=	4.59242397E-05
21	JMARK=	78	KMARK=	1	DPHIMX=	4.41000621E-05
22	JMARK=	78	KMARK=	1	DPHIMX=	4.23921712E-05
23	JMARK=	78	KMARK=	1	DPHIMX=	4.07812310E-05
24	JMARK=	78	KMARK=	1	DPHIMX=	3.92548354E-05
25	JMARK=	78	KMARK=	1	DPHIMX=	3.77834008E-05
26	JMARK=	78	KMARK=	1	DPHIMX=	3.63859394E-05
27	JMARK=	78	KMARK=	1	DPHIMX=	3.50700923E-05
28	JMARK=	78	KMARK=	1	DPHIMX=	3.38324635E-05
29	JMARK=	78	KMARK=	1	DPHIMX=	3.26407952E-05
30	JMARK=	78	KMARK=	1	DPHIMX=	3.15109701E-05
31	JMARK=	78	KMARK=	1	DPHIMX=	3.04537760E-05
32	JMARK=	78	KMARK=	1	DPHIMX=	2.94574684E-05
33	JMARK=	78	KMARK=	1	DPHIMX=	2.85014043E-05
34	JMARK=	78	KMARK=	1	DPHIMX=	2.75948242E-05
35	JMARK=	78	KMARK=	1	DPHIMX=	2.67419258E-05
36	JMARK=	78	KMARK=	1	DPHIMX=	2.59215478E-05
37	JMARK=	78	KMARK=	1	DPHIMX=	2.51413685E-05
38	JMARK=	78	KMARK=	1	DPHIMX=	2.44077040E-05
39	JMARK=	78	KMARK=	1	DPHIMX=	2.37116166E-05
40	JMARK=	78	KMARK=	1	DPHIMX=	2.30501701E-05
41	JMARK=	78	KMARK=	1	DPHIMX=	2.24211303E-05
42	JMARK=	78	KMARK=	1	DPHIMX=	2.18211957E-05
43	JMARK=	78	KMARK=	1	DPHIMX=	2.12407669E-05
44	JMARK=	78	KMARK=	1	DPHIMX=	2.06780912E-05
45	JMARK=	78	KMARK=	1	DPHIMX=	2.01333361E-05
46	JMARK=	78	KMARK=	1	DPHIMX=	1.96261279E-05
47	JMARK=	78	KMARK=	1	DPHIMX=	1.90991009E-05
48	JMARK=	78	KMARK=	1	DPHIMX=	1.85717100E-05
49	JMARK=	78	KMARK=	1	DPHIMX=	1.80507701E-05
50	JMARK=	78	KMARK=	1	DPHIMX=	1.76173064E-05
51	JMARK=	78	KMARK=	1	DPHIMX=	1.71924750E-05
52	JMARK=	78	KMARK=	1	DPHIMX=	1.67386667E-05
53	JMARK=	78	KMARK=	1	DPHIMX=	1.63460425E-05
54	JMARK=	78	KMARK=	1	DPHIMX=	1.59068116E-05
55	JMARK=	78	KMARK=	1	DPHIMX=	1.55241438E-05
56	JMARK=	78	KMARK=	1	DPHIMX=	1.51856047E-05
57	JMARK=	78	KMARK=	1	DPHIMX=	1.48695835E-05
58	JMARK=	78	KMARK=	1	DPHIMX=	1.44715651E-05
59	JMARK=	78	KMARK=	1	DPHIMX=	1.41162364E-05
60	JMARK=	78	KMARK=	1	DPHIMX=	1.38055950E-05
61	JMARK=	78	KMARK=	1	DPHIMX=	1.35194646E-05
62	JMARK=	78	KMARK=	1	DPHIMX=	1.32034500E-05
63	JMARK=	78	KMARK=	1	DPHIMX=	1.27697944E-05
64	JMARK=	78	KMARK=	1	DPHIMX=	1.23761727E-05
65	JMARK=	78	KMARK=	1	DPHIMX=	1.20487144E-05
66	JMARK=	78	KMARK=	1	DPHIMX=	1.17637029E-05
67	JMARK=	78	KMARK=	1	DPHIMX=	1.15131939E-05
68	JMARK=	78	KMARK=	1	DPHIMX=	1.12889837E-05
69	JMARK=	78	KMARK=	1	DPHIMX=	1.10834788E-05
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72	JMARK=	78	KMARK=	1	DPHIMX=	1.06182149E-05
73	JMARK=	78	KMARK=	1	DPHIMX=	9.88326295E-06
74	JMARK=	78	KMARK=	1	DPHIMX=	9.63552008E-06
75	JMARK=	78	KMARK=	1	DPHIMX=	9.43041947E-06
76	JMARK=	78	KMARK=	1	DPHIMX=	9.25811576E-06
77	JMARK=	78	KMARK=	1	DPHIMX=	9.10904824E-06
78	JMARK=	78	KMARK=	1	DPHIMX=	8.95251458E-06
79	JMARK=	78	KMARK=	1	DPHIMX=	8.79976959E-06
80	JMARK=	78	KMARK=	1	DPHIMX=	8.64092454E-06
81	JMARK=	78	KMARK=	1	DPHIMX=	8.23611180E-06
82	JMARK=	78	KMARK=	1	DPHIMX=	7.92768657E-06
83	JMARK=	78	KMARK=	1	DPHIMX=	7.82648919E-06
84	JMARK=	78	KMARK=	1	DPHIMX=	7.50696311E-06
85	JMARK=	78	KMARK=	1	DPHIMX=	7.25281521E-06
86	JMARK=	78	KMARK=	1	DPHIMX=	6.96404202E-06
87	JMARK=	78	KMARK=	19	DPHIMX=	6.74928582E-06
88	JMARK=	78	KMARK=	19	DPHIMX=	6.60152848E-06
89	JMARK=	78	KMARK=	19	DPHIMX=	6.46435850E-06
90	JMARK=	78	KMARK=	19	DPHIMX=	6.33740691E-06
91	JMARK=	78	KMARK=	19	DPHIMX=	6.21973408E-06
92	JMARK=	78	KMARK=	19	DPHIMX=	6.12662176E-06
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96	JMARK=	78	KMARK=	19	DPHIMX=	5.92899124E-06
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98	JMARK=	78	KMARK=	19	DPHIMX=	5.84361441E-06
99	JMARK=	78	KMARK=	19	DPHIMX=	5.80034490E-06
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103	JMARK=	78	KMARK=	19	DPHIMX=	5.57534019E-06
104	JMARK=	78	KMARK=	19	DPHIMX=	5.51475460E-06
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109	JMARK=	78	KMARK=	19	DPHIMX=	5.23170611E-06
110	JMARK=	78	KMARK=	19	DPHIMX=	5.17800967E-06
111	JMARK=	78	KMARK=	19	DPHIMX=	5.12484024E-06
112	JMARK=	78	KMARK=	19	DPHIMX=	5.07213074E-06
113	JMARK=	78	KMARK=	19	DPHIMX=	5.01920210E-06
114	JMARK=	78	KMARK=	19	DPHIMX=	4.96578884E-06

ORIGINAL PAGE IS  
OF POOR QUALITY

## SUBROUTINE RESULT

## SHOCK WAVE AND SONIC LINE LOCATIONS

J	XW(J)	SLAS(J,1)	SLAS(J,2)	SLAS(J,3)	SLAS(J,4)	SLAS(J,5)	SLAS(J,6)
18	-2.40000000E-01	0.	0.	0.	0.	0.	0.
19	-2.20000000E-01	0.	0.	0.	0.	0.	0.
20	-2.00000000E-01	0.	0.	0.	0.	0.	0.
21	-1.80000000E-01	0.	0.	0.	0.	0.	0.
22	-1.60000000E-01	0.	0.	0.	0.	0.	0.
23	-1.40000000E-01	0.	0.	0.	0.	0.	0.
24	-1.20000000E-01	0.	0.	0.	0.	0.	0.
25	-1.00000000E-01	0.	0.	0.	0.	0.	0.
26	-8.00000000E-02	0.	0.	0.	0.	0.	0.
27	-6.00000000E-02	0.	0.	0.	0.	0.	0.
28	-4.00000000E-02	0.	0.	0.	0.	0.	0.
29	-2.00000000E-02	0.	0.	0.	0.	0.	0.
30	0.	0.	0.	0.	0.	0.	0.
31	2.00000000E-02	0.	0.	0.	0.	0.	0.
32	4.00000000E-02	0.	0.	0.	0.	0.	0.
33	6.00000000E-02	0.	0.	0.	0.	0.	0.
34	8.00000000E-02	0.	0.	0.	0.	0.	0.
35	1.00000000E-01	0.	0.	0.	0.	0.	0.
36	1.20000000E-01	0.	0.	0.	0.	0.	0.
37	1.40000000E-01	0.	0.	0.	0.	0.	0.
38	1.60000000E-01	0.	0.	0.	0.	0.	0.
39	1.80000000E-01	0.	0.	0.	0.	0.	0.
40	2.00000000E-01	0.	0.	0.	0.	0.	0.
41	2.20000000E-01	0.	0.	0.	0.	0.	0.
42	2.40000000E-01	0.	0.	0.	0.	0.	0.
43	2.60000000E-01	0.	0.	0.	0.	0.	0.
44	2.80000000E-01	6.30180747E-02	0.	0.	0.	0.	0.
45	3.00000000E-01	9.20387956E-02	0.	0.	0.	0.	0.
46	3.20000000E-01	1.37695434E-01	0.	0.	0.	0.	0.
47	3.40000000E-01	1.91638680E-01	0.	0.	0.	0.	0.
48	3.60000000E-01	2.49887577E-01	0.	0.	0.	0.	0.
49	3.80000000E-01	3.08834648E-01	0.	0.	0.	0.	0.
50	4.00000000E-01	3.62253205E-01	0.	0.	0.	0.	0.
51	4.20000000E-01	3.99284579E-01	0.	0.	0.	0.	0.
52	4.40000000E-01	4.38382358E-01	0.	0.	0.	0.	0.
53	4.60000000E-01	4.6776444E-01	0.	0.	0.	0.	0.
54	4.80000000E-01	4.82193335E-01	0.	0.	0.	0.	0.
55	5.00000000E-01	4.93710771E-01	0.	0.	0.	0.	0.
56	5.20000000E-01	5.05799432E-01	0.	0.	0.	0.	0.
57	5.40000000E-01	5.17716024E-01	0.	0.	0.	0.	0.
58	5.60000000E-01	5.29297606E-01	0.	0.	0.	0.	0.
59	5.80000000E-01	5.40818417E-01	0.	0.	0.	0.	0.
60	6.00000000E-01	5.52180299E-01	0.	0.	0.	0.	0.
61	6.20000000E-01	5.63499657E-01	0.	0.	0.	0.	0.
62	6.40000000E-01	5.74822233E-01	0.	0.	0.	0.	0.
63	6.60000000E-01	5.86303544E-01	0.	0.	0.	0.	0.
64	6.80000000E-01	5.97822357E-01	0.	0.	0.	0.	0.
65	7.00000000E-01	6.09353530E-01	0.	0.	0.	0.	0.
66	7.20000000E-01	6.20935414E-01	0.	0.	0.	0.	0.
67	7.40000000E-01	6.32114730E-01	0.	0.	0.	0.	0.
68	7.60000000E-01	6.43141463E-01	2.58216644E-01	0.	0.	0.	0.
69	7.80000000E-01	0.	0.	0.	0.	0.	0.
70	8.00000000E-01	0.	0.	0.	0.	0.	0.
71	8.20000000E-01	0.	0.	0.	0.	0.	0.
72	8.40000000E-01	0.	0.	0.	0.	0.	0.
73	8.60000000E-01	0.	0.	0.	0.	0.	0.
74	8.80000000E-01	0.	0.	0.	0.	0.	0.
75	9.00000000E-01	0.	0.	0.	0.	0.	0.
76	9.20000000E-01	0.	0.	0.	0.	0.	0.
77	9.40000000E-01	0.	0.	0.	0.	0.	0.
78	9.60000000E-01	0.	0.	0.	0.	0.	0.
79	9.80000000E-01	0.	0.	0.	0.	0.	0.
80	1.00000000E+00	0.	0.	0.	0.	0.	0.
81	1.02000000E+00	0.	0.	0.	0.	0.	0.
82	1.04000000E+00	0.	0.	0.	0.	0.	0.
83	1.06000000E+00	0.	0.	0.	0.	0.	0.
84	1.08000000E+00	0.	0.	0.	0.	0.	0.
85	1.10000000E+00	0.	0.	0.	0.	0.	0.
86	1.12000000E+00	0.	0.	0.	0.	0.	0.
87	1.14000000E+00	0.	0.	0.	0.	0.	0.
88	1.16000000E+00	0.	0.	0.	0.	0.	0.
89	1.18000000E+00	0.	0.	0.	0.	0.	0.
90	1.20000000E+00	0.	0.	0.	0.	0.	0.
91	1.22000000E+00	0.	0.	0.	0.	0.	0.
92	1.24000000E+00	0.	0.	0.	0.	0.	0.



1 GENERAL POINTS ( COMPUTATIONAL APPROXIMATION )  
2 POINTS UNDER WING ( COMPUTATIONAL APPROXIMATION )  
3 POINTS ABOVE WING  
4 POINTS UNDER WING

[illegible]

ORIGINAL PAGE IS  
OF POOR QUALITY



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5.652904E-03 6.6009932E-03 7.82368238E-03 9.24426994E-03 1.0967916E-02 1.30740071E-02 1.57798827E-02 1.92589018E-02  
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7.7522837E-02 7.0267632E-02 6.2143730E-02 5.25707523E-02 4.22568696E-02 3.16020207E-02 2.03713809E-02 9.12204887E-03  
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3.17185074E-02	6.36923261E-02	8.02906564E-02	8.7285879E-02	6.50205808E-02	6.57443321E-02	6.46497747E-02	6.20169975E-02	6.20169975E-02
5.53138203E-02	7.47663702E-02	8.09803460E-02	5.63485436E-02					

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-6.84766243E-06	-7.16309462E-06	-7.47257448E-06	-7.77431298E-06	-8.06654753E-06	-8.34755983E-06	-8.61569339E-06	-8.86937026E-06
-9.10710571E-06	-9.32751711E-06	-9.52931559E-06	-9.71124649E-06	-9.87192249E-06	-1.00096832E-05	-1.01230292E-05	-1.02112381E-05
-1.02741740E-05	-1.03119171E-05	-1.03247179E-05	-1.03130956E-05	-1.02779283E-05	-1.02204864E-05	-1.01423911E-05	-1.00454827E-05
-9.93161934E-06	-9.80247410E-06	-9.65941751E-06	-9.50353882E-06	-9.33577686E-06	-9.15707751E-06	-8.96857058E-06	-8.77125784E-06
-8.56649878E-06	-8.35579067E-06	-8.14069779E-06	-7.92280857E-06	-7.70370583E-06	-7.48493005E-06	-7.26798179E-06	-7.05432187E-06
-6.84534102E-06	-6.64235135E-06	-6.44657746E-06	-6.25914850E-06	-6.08109092E-06	-5.91332217E-06	-5.75664522E-06	-5.61174386E-06
-5.47917898E-06	-5.35938561E-06	-5.25267085E-06					

48 18 92

-5.16076059E-07	-5.56413558E-07	-6.03098039E-07	-6.56219243E-07	-7.15847741E-07	-7.82029790E-07	-8.54782256E-07	-9.34087703E-07
-1.01983977E-06	-1.11208891E-06	-1.21053861E-06	-1.31504225E-06	-1.42535046E-06	-1.54115943E-06	-1.66210983E-06	-1.78778668E-06
-1.91772006E-06	-2.05138674E-06	-2.18821267E-06	-2.32757641E-06	-2.46881331E-06	-2.61122058E-06	-2.75406301E-06	-2.89657939E-06
-3.03798942E-06	-3.17750114E-06	-3.31431793E-06	-3.44764716E-06	-3.57670823E-06	-3.70074072E-06	-3.81901178E-06	-3.93082414E-06
-4.03552272E-06	-4.13250026E-06	-4.22119917E-06	-4.30110324E-06	-4.37170826E-06	-4.43249737E-06	-4.48302607E-06	-4.52304167E-06
-4.55244749E-06	-4.57123223E-06	-4.57946086E-06	-4.57729306E-06	-4.56495931E-06	-4.54296600E-06	-4.51168550E-06	-4.47172877E-06
-4.42370437E-06	-4.36821663E-06	-4.30584028E-06	-4.23712121E-06	-4.16259828E-06	-4.08283000E-06	-3.99842493E-06	-3.90997822E-06
-3.81816132E-06	-3.72367620E-06	-3.62723845E-06	-3.52956573E-06	-3.43136911E-06	-3.3334206E-06	-3.23615999E-06	-3.14047569E-06
-3.04691208E-06	-2.95605803E-06	-2.86846472E-06	-2.78464222E-06	-2.70505652E-06	-2.63012693E-06	-2.56022591E-06	-2.49566715E-06
-2.43672419E-06	-2.38360935E-06	-2.33648296E-06					

49 18 92

-1.26316928E-07	-1.36234705E-07	-1.47801765E-07	-1.60890859E-07	-1.75569896E-07	-1.91850691E-07	-2.09737737E-07	-2.29227004E-07
-2.50304818E-07	-2.72946828E-07	-2.97117088E-07	-3.22767283E-07	-3.49836117E-07	-3.78248881E-07	-4.07917213E-07	-4.38739070E-07
-4.70593916E-07	-5.03368123E-07	-5.36905398E-07	-5.71058626E-07	-6.05663911E-07	-6.40548819E-07	-6.75532799E-07	-7.10428951E-07
-7.45045740E-07	-7.79188810E-07	-8.12662848E-07	-8.45273569E-07	-8.76329696E-07	-9.07144920E-07	-9.36039827E-07	-9.63343755E-07
-9.83895541E-07	-1.01255010E-06	-1.03416968E-06	-1.05363437E-06	-1.07083625E-06	-1.08567968E-06	-1.09808689E-06	-1.10800554E-06
-1.11540683E-06	-1.12028142E-06	-1.12263885E-06	-1.12250339E-06	-1.11993967E-06	-1.11500248E-06	-1.10778559E-06	-1.09839434E-06
-1.08694743E-06	-1.07357347E-06	-1.05840850E-06	-1.04159494E-06	-1.02328182E-06	-1.00362521E-06	-9.82788622E-07	-9.60939152E-07
-9.38249570E-07	-9.14896491E-07	-8.91057227E-07	-8.66903222E-07	-8.42623481E-07	-8.18372923E-07	-7.94321406E-07	-7.70627577E-07
-7.47442615E-07	-7.24909239E-07	-7.03160804E-07	-6.82320487E-07	-6.62500580E-07	-6.43801867E-07	-6.26313103E-07	-6.10110596E-07
-5.95257870E-07	-5.81805443E-07	-5.69790683E-07					

# AIRLIFT LIFT DISTRIBUTION

CP(J) = LIFT MINUS VORTEX EFFECT  
 CPO(J) = LIFT  
 CPI(J) = LIFT MINUS THICKNESS AND VORTEX EFFECTS  
 CP2(J) = LIFT MINUS THICKNESS EFFECT  
 AINT = THICKNESS EFFECT  
 DCP = VORTEX EFFECT

J	CP(J)	CPO(J)	CPI(J)	CP2(J)	AINT	DCP
43	1.59075127E-02	2.02903330E-02	1.64586993E-02	2.38415185E-02	-5.51185559E-03	4.38281927E-04
44	1.66216973E-03	2.52146043E-03	1.71226571E-03	2.57155640E-03	-5.00959700E-03	8.59290698E-04
45	1.85044597E-03	3.13462525E-03	1.85855261E-03	1.13273190E-03	1.89335472E-06	1.27417928E-02
46	2.08522324E-03	3.76580582E-03	2.08182789E-03	3.76241047E-03	3.39535429E-06	1.60058258E-03
47	2.36321853E-03	4.46054401E-03	2.38003337E-03	4.45735665E-03	3.18516686E-06	2.07752548E-03
48	2.68545377E-03	5.14868276E-03	2.75452721E-03	5.21775620E-03	-6.90734347E-03	2.46322899E-03
49	3.11334700E-03	5.95316505E-03	3.22086844E-03	6.06068649E-03	-1.07521425E-04	2.83981805E-03
50	3.81175824E-03	7.03064482E-03	3.84667711E-03	7.06555969E-03	-3.49148698E-05	3.21686058E-03
51	4.75612254E-03	8.40042314E-03	4.86212750E-03	8.50692770E-03	-1.06034564E-04	3.64483020E-03
52	6.73351424E-03	1.09866219E-02	6.89505543E-03	1.11431631E-02	-1.56541189E-04	4.25310766E-03
53	1.11331674E-02	1.64793417E-02	1.11074835E-02	1.64536380E-02	2.57038601E-05	5.34617446E-03
54	1.84289966E-02	2.55800855E-02	1.85465365E-02	2.56895975E-02	-1.09511959E-04	7.14308889E-03
55	2.73699157E-02	3.65005085E-02	2.84229909E-02	3.75532437E-02	-1.05267525E-03	9.13065281E-03
56	3.65218752E-02	4.71224305E-02	3.83478225E-02	4.89384277E-02	-1.81554733E-03	1.05906052E-02
57	4.50059503E-02	5.64808913E-02	4.64229023E-02	5.83008438E-02	-1.81995201E-03	1.14749415E-02
58	5.20181364E-02	6.40749104E-02	5.38377024E-02	6.58944764E-02	-1.81956003E-03	1.20567740E-02
59	5.90140459E-02	7.15426945E-02	5.97327429E-02	7.22613954E-02	-7.13698449E-04	1.2526526E-02
60	6.52024262E-02	7.81627777E-02	6.46245117E-02	7.75850604E-02	5.77914497E-04	1.29605487E-02
61	6.99703925E-02	8.3329584E-02	6.83687106E-02	8.17252765E-02	1.63168190E-03	1.33555658E-02
62	7.35651288E-02	8.72606767E-02	7.06741500E-02	8.43696580E-02	2.89097874E-03	1.36955079E-02
63	7.53160813E-02	8.92667029E-02	7.12388792E-02	8.51595551E-02	4.10720703E-03	1.39506759E-02
64	7.59250418E-02	9.00258093E-02	6.97060888E-02	8.38063565E-02	6.21895301E-03	1.41077676E-02
65	7.83493979E-02	9.29318362E-02	6.60742243E-02	8.02120926E-02	1.22697135E-02	1.41378683E-02
66	8.2183911E-02	9.60912591E-02	6.04849744E-02	7.45578424E-02	2.21334167E-02	1.40728880E-02
67	8.29429440E-02	9.67789029E-02	5.33953470E-02	6.73313059E-02	2.94475970E-02	1.39559589E-02
68	5.9691129E-02	6.77392253E-02	4.94736630E-02	5.92458760E-02	8.49344986E-03	1.27702129E-02
69	1.86055167E-02	3.22251203E-02	3.74607627E-02	5.10799679E-02	-1.88564860E-02	1.36192053E-02
70	1.3039003E-02	2.65224202E-02	2.99953706E-02	4.34947855E-02	-1.49761053E-02	1.35134149E-02
71	9.79156541E-03	2.32533795E-02	1.75359970E-02	3.09978111E-02	-7.74463162E-03	1.34618141E-02
72	0.01824958E-03	2.15710194E-02	1.18583240E-02	2.33110954E-02	-5.84307599E-03	1.34527694E-02
73	6.11794319E-03	1.95811043E-02	7.88866401E-03	2.13519278E-02	-1.77072383E-03	1.34631638E-02
74	4.29968382E-03	1.77599123E-02	5.14685755E-03	1.86171275E-02	-8.57213735E-04	1.34732300E-02
75	3.27645013E-03	1.67366233E-02	3.25250065E-03	1.67126747E-02	2.39495434E-05	1.34601741E-02
76	6.56295037E-03	1.99743624E-02	1.92374173E-03	1.52546537E-02	4.62020863E-03	1.34309120E-02
77	4.95242703E-03	1.83524043E-02	9.58895499E-04	1.4348E719E-02	4.00353243E-03	1.33699764E-02
78	-1.47868519E-04	1.32048821E-02	0.	1.33503517E-02	-1.47868519E-04	1.33503517E-02

## LIFT AND MOMENT

AL = LIFT, AM = MOMENT, XBAR = MOMENT ARM ABOUT NOSE  
 A = ATTACHED FLOW, S = SEPARATED FLOW  
 NS = NEGLECT SHOCK  
 AINTO = SHOCK LIFT, SMA = VORTEX LIFT  
 AREA = EXPOSED WING AREA  
 OR MAXIMUM CROSS-SECTIONAL AREA

ALA	=	2.01012025E-02
ALS	=	2.69564257E-02
AMA	=	1.31611109E-02
AMS	=	1.79579237E-02
XBARA	=	6.54742466E-01
XBARs	=	6.66183315E-01
ALANS	=	1.93366004E-02
ALSNS	=	2.61918276E-02
AMANS	=	1.26295870E-02
AMSNS	=	1.74263998E-02
XBARAN	=	6.52144129E-01
XBARSN	=	6.65337258E-01
AINTO	=	7.64602085E-04
SMA	=	6.85522716E-03
CLA	=	2.67213459E-01
CLS	=	3.58345463E-01
CLANS	=	2.57051216E-01
CLSNS	=	3.48181221E-01
CAINTO	=	1.01642425E-02
CSMA	=	9.11300045E-02
CMA	=	1.74957309E-01
CMS	=	2.38723769E-01
CMANS	=	1.67891493E-01
CMSNS	=	2.31657553E-01
ARFA	=	1.50449358E-01



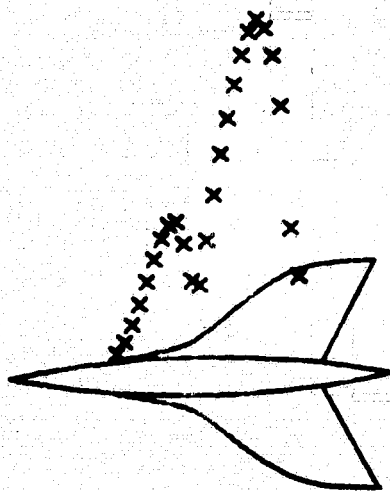
BCDY SURFACE PRESSURE COEFFICIENTS

CP(J) - OMEGA = +J DEGREES ( LEEWARD SIDE )  
 CP(J) - OMEGA = -J DEGREES ( WINDWARD SIDE )  
 CP1(J) - OMEGA = +90 DEGREES  
 CP2(J) - OMEGA = -90 DEGREES  
 CPX, CP0X, CP1X AND CP2X - VORTEX EFFECTS NEGLECTED

J	CP(J)	CP0(J)	CP1(J)	CP2(J)	CPX	CP0X	CP1X	CP2X
31	2.26606185E-01	2.26606185E-01	1.92497076E-01	2.99643020E-01				
32	1.73244456E-01	1.73244456E-01	1.43367554E-01	2.46049083E-01				
33	1.40261819E-01	1.40261819E-01	1.10617124E-01	2.08834239E-01				
34	1.12297246E-01	1.12297246E-01	8.47972359E-02	1.78549537E-01				
35	8.81945923E-02	8.81945923E-02	6.30143115E-02	1.52302598E-01				
36	6.66998721E-02	6.66998721E-02	4.39518186E-02	1.28775691E-01				
37	4.76013062E-02	4.76013062E-02	2.68854398E-02	1.07244898E-01				
38	2.98527703E-02	2.98527703E-02	1.13691111E-02	8.72641546E-02				
39	1.35577364E-02	1.35577364E-02	2.89371569E-03	6.85369134E-02				
40	-2.09523192E-03	-2.09523192E-03	-1.61144768E-02	5.08517380E-02				
41	-1.66849798E-02	-1.66849798E-02	-2.84720176E-02	3.40297829E-02				
42	-3.04970674E-02	-3.04970674E-02	-4.30518980E-02	1.79854882E-02				
43	-9.63728477E-02	-9.63728477E-02	-5.40659462E-02	1.32736441E-02	-5.17006006E-02	9.67617788E-03	-5.72028499E-02	1.03784272E-02
44	-1.07108508E-01	-1.07108508E-01	-6.76927130E-02	-1.11065583E-02	-6.54548857E-02	-9.31712815E-03	-6.41202828E-02	-1.06517290E-02
45	-1.17533361E-01	-1.17533361E-01	-8.09314196E-02	-2.29774441E-02	-1.85942238E-02	-1.87925792E-02	-7.53931605E-02	-2.21936425E-02
46	-1.26534076E-01	-1.26534076E-01	-9.19370195E-02	-3.51963466E-02	-9.02326461E-02	-2.65628260E-02	-8.51812974E-02	-3.40141747E-02
47	-1.34949150E-01	-1.34949150E-01	-1.02696884E-01	-4.73221264E-02	-1.01300330E-01	-3.83899296E-02	-9.44400099E-02	-4.57522201E-02
48	-1.42707767E-01	-1.42707767E-01	-1.12773871E-01	-5.73081799E-02	-1.11724123E-01	-4.66541253E-02	-1.03081814E-01	-5.53404343E-02
49	-1.51244415E-01	-1.51244415E-01	-1.23674664E-01	-7.36103048E-02	-1.23055235E-01	-5.170061330E-02	-1.12580771E-01	-7.11806874E-02
50	-1.58190335E-01	-1.58190335E-01	-1.33131460E-01	-7.82786216E-02	-1.33267432E-01	-5.29478644E-02	-1.20627534E-01	-7.50570339E-02
51	-1.62336949E-01	-1.62336949E-01	-1.40351273E-01	-8.57110500E-02	-1.42159475E-01	-5.44029203E-02	-1.26291109E-01	-8.07722862E-02
52	-1.64437535E-01	-1.64437535E-01	-1.45990333E-01	-9.04038635E-02	-1.51285178E-01	-5.64528994E-02	-1.29813632E-01	-8.11244457E-02
53	-1.65124150E-01	-1.65124150E-01	-1.50726495E-01	-9.64042997E-02	-1.61458403E-01	-5.87925827E-02	-1.31303533E-01	-8.30341280E-02
54	-1.60954019E-01	-1.60954019E-01	-1.56411106E-01	-9.59568822E-02	-1.72010679E-01	-6.10021118E-02	-1.33098884E-01	-8.31291792E-02
55	-1.73011250E-01	-1.73011250E-01	-1.68933847E-01	-1.23082215E-02	-1.86202704E-01	-6.36131900E-02	-1.34995671E-01	-1.85088430E-02
56	-1.49276376E-01	-1.49276376E-01	-1.48636887E-01	-2.5124485E-02	-2.04885585E-01	-2.14362124E-02	-1.65583567E-01	-1.78757060E-02
57	-2.20546953E-01	-2.20546953E-01	-2.11718374E-01	-3.48801621E-02	-2.25854645E-01	-1.62641336E-02	-1.91969687E-01	-2.36209049E-02
58	-2.44186679E-01	-2.44186679E-01	-2.34126156E-01	-4.34935667E-02	-2.45980451E-01	-7.23527105E-02	-2.17307710E-01	-3.59079625E-02
59	-2.63434397E-01	-2.63434397E-01	-2.52944401E-01	-4.83075205E-02	-2.62643780E-01	-1.03249287E-02	-2.38208875E-01	-4.27548336E-02
60	-2.77722067E-01	-2.77722067E-01	-2.67238547E-01	-5.44011441E-02	-2.74929838E-01	-2.25051693E-02	-2.53929621E-01	-4.46657342E-02
61	-2.87546582E-01	-2.87546582E-01	-2.77329947E-01	-5.93317748E-02	-2.83123384E-01	-3.72033295E-02	-2.64364900E-01	-5.5274735E-02
62	-2.93506632E-01	-2.93506632E-01	-2.85688847E-01	-6.00472774E-02	-2.87699534E-01	-4.44414426E-02	-2.71334605E-01	-5.7566754E-02
63	-2.95919411E-01	-2.95919411E-01	-2.86555155E-01	-6.04733435E-02	-2.88730537E-01	-5.62211370E-02	-2.74185362E-01	-7.01603616E-02
64	-2.94677331E-01	-2.94677331E-01	-2.84004672E-01	-7.15407735E-02	-2.86391642E-01	-6.40358295E-02	-2.73327927E-01	-7.58615453E-02
65	-2.90241231E-01	-2.90241231E-01	-2.81869477E-01	-7.99184934E-02	-2.83413071E-01	-6.54933613E-02	-2.68651251E-01	-7.73070818E-02
66	-2.81540401E-01	-2.81540401E-01	-2.73645550E-01	-8.29933881E-02	-2.70469930E-01	-6.37454355E-02	-2.59633168E-01	-6.45261973E-02
67	-2.67137744E-01	-2.67137744E-01	-2.59363760E-01	-8.85959533E-02	-2.54941065E-01	-6.24000333E-02	-2.50294448E-01	-1.26973855E-02
68	-2.53946895E-01	-2.53946895E-01	-2.32327551E-01	-9.91423343E-02	-2.25913077E-01	-6.43071338E-02	-2.16717702E-01	-3.91347597E-02
69	-6.04638877E-02	-6.04638877E-02	1.22661253E-02	5.80377333E-02	2.00781119E-02	7.44522663E-02	2.96813811E-02	6.98492972E-02
70	1.05672522E-01	1.05672522E-01	1.11907047E-01	1.28254449E-01	1.21614701E-01	1.12129922E-01	1.25712416E-01	1.04037207E-01
71	1.19292797E-01	1.19292797E-01	1.26605577E-01	1.19392777E-01				
72	1.11896259E-01	1.11896259E-01	1.18776151E-01	1.25951016E-01				
73	1.12250659E-01	1.12250659E-01	1.18784005E-01	1.12256659E-01				
74	1.19747913E-01	1.19747913E-01	1.25264949E-01	1.19247913E-01				
75	1.31483676E-01	1.31483676E-01	1.36857490E-01	1.31483676E-01				
76	1.44313758E-01	1.44313758E-01	1.52927432E-01	1.44313758E-01				
77	1.70231627E-01	1.70231627E-01	1.73948311E-01	1.70231627E-01				
78	2.00254514E-01	2.00254514E-01	2.02956421E-01	2.00254514E-01				
79	2.49939707E-01	2.49939707E-01	2.51397494E-01	2.49939707E-01				

CPSTAR = -3.40704836E-02

DRAG = -1.1917534E-05

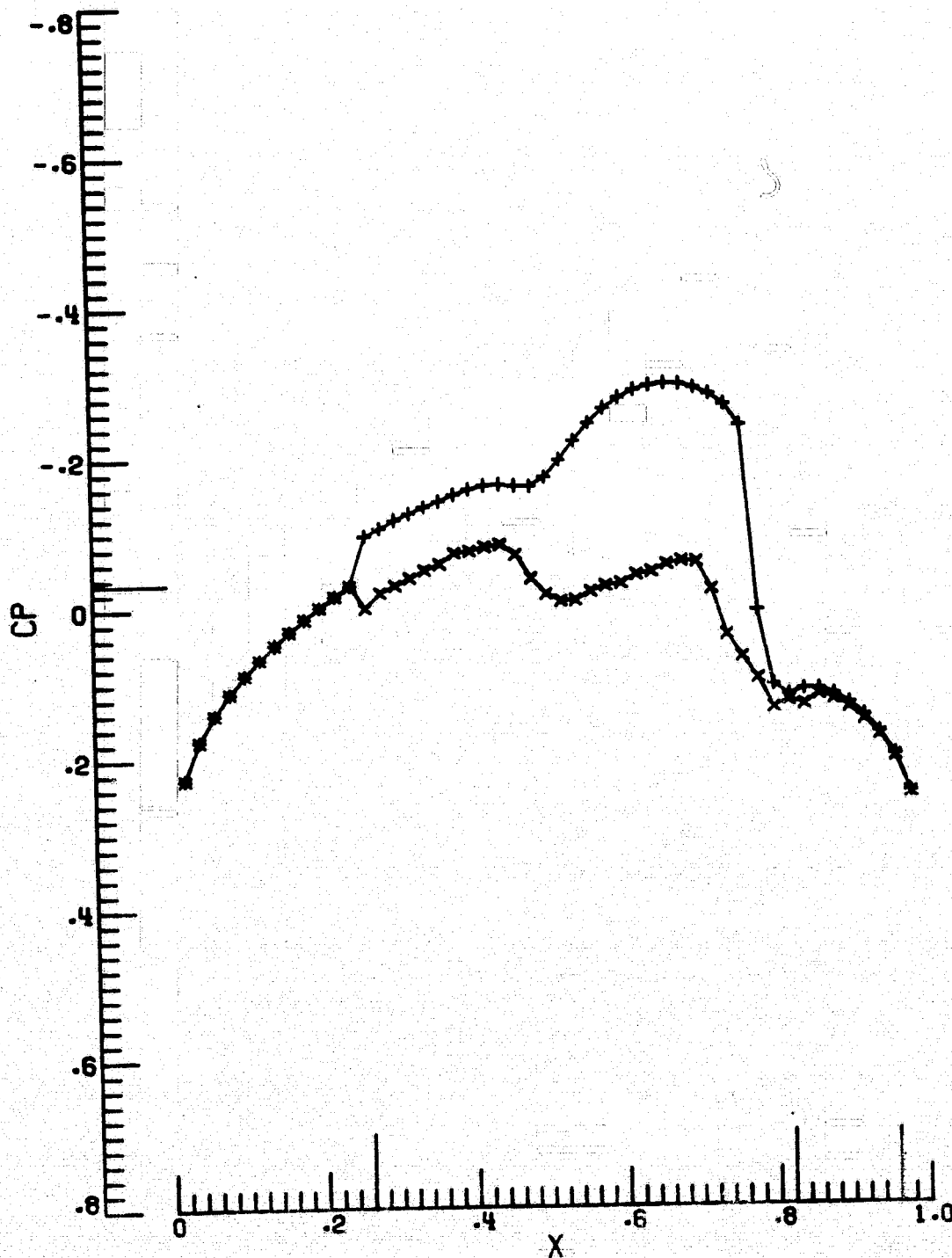


SONIC LINE AND SHOCK WAVE.

$M = .980$   $F = 10.000$   $H = .300$

$\text{ALPHA} = 4.00 \text{ DEG.}$   $\text{OMEGA} = 0.00 \text{ DEG.}$

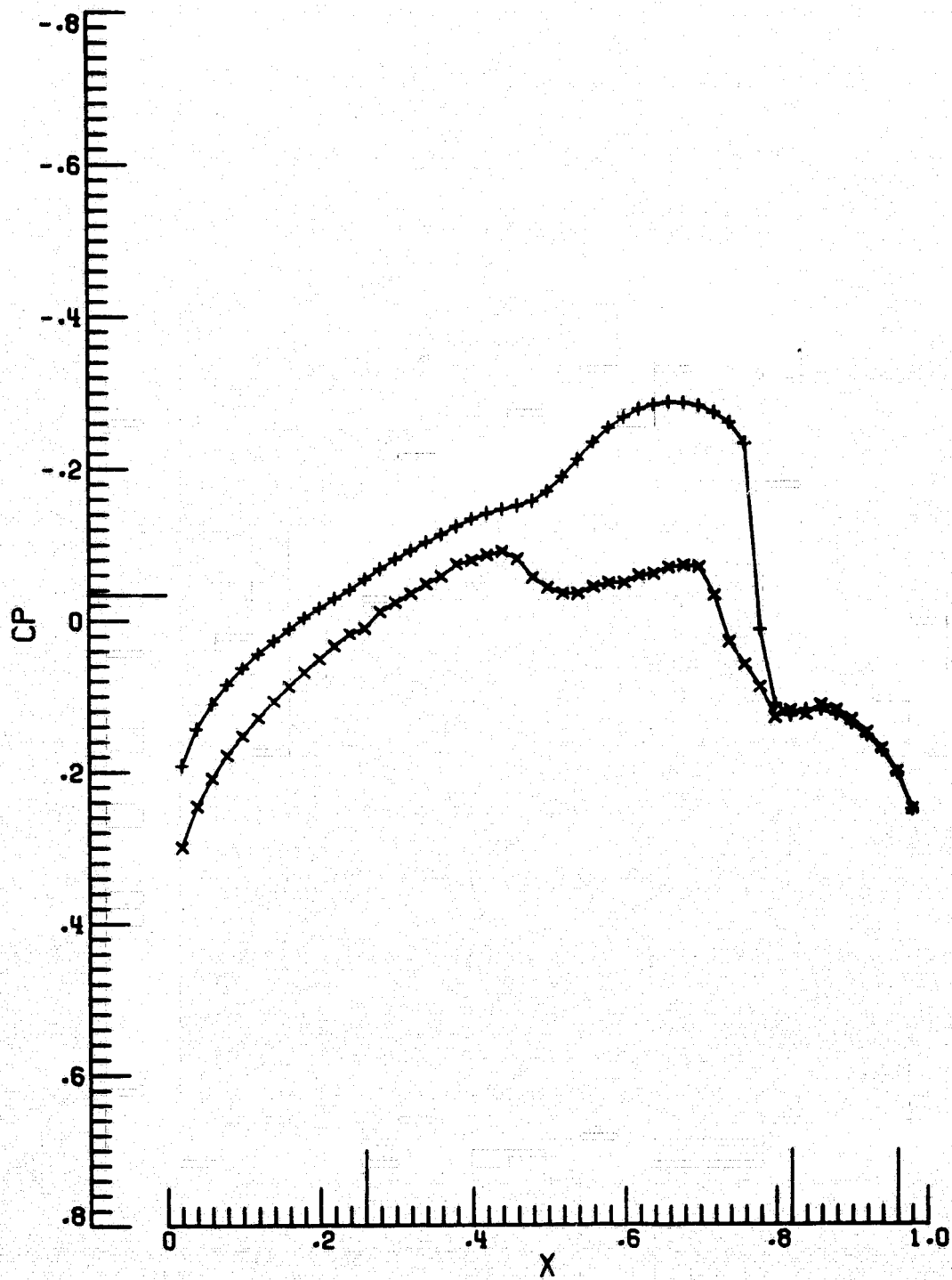
Figure 7. - Outline of configuration and shock-wave and sonic-line locations in computational plane.



BODY PRESSURE DISTRIBUTION  
IN WING PLANE

$M = .980$   $F = 10.000$   $H = .300$   
 $\text{ALPHA} = 4.00 \text{ DEG.}$   $\text{OMEGA} = 0.00 \text{ DEG.}$

Figure 8.- Body pressure distribution in wing plane.



BODY PRESSURE DISTRIBUTION  
IN SYMMETRY PLANE

$M = .980$   $F = 10.000$   $H = .300$

$\text{ALPHA} = 4.00 \text{ DEG.}$   $\text{OMEGA} = 0.00 \text{ DEG.}$

Figure 9. - Body pressure distribution in symmetry plane.

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